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July 26, 2017

City of La Center Attn: Tony Cooper 305 NW Pacific Hwy La Center, WA 98629

**RE: Existing Sewer Conveyance Capacity Analysis** 

Dear Tony,

The Riverside Estates Subdivision and the Sunrise Terrace Subdivision have both been proposed to be constructed along Old Pacific Highway in the northwest corner of the City of La Center. Unfortunately, there is no existing sanitary service to this portion of the city. As a result, a sanitary pump station has been proposed in the southeast corner of the Riverside Estates Subdivision to provide the necessary service for both developments. Due to the size of both projects, it was prudent to verify the capacity of the impacted portion of the City of La Center's existing sanitary sewer conveyance system to ensure it is sized sufficiently to accommodate the increased flows. The following analysis and documentation is intended to confirm that the existing sanitary sewer conveyance system is sufficient to safely convey the additional sewer generated from both developments.

As part of this analysis, Romtec Utilities was contracted to complete a preliminary pump station design and size the proposed sanitary force main which will convey the effluent from the proposed pump station to the City of La Center's existing sanitary conveyance system. A basin analysis was previously completed to establish peak flow rates generated from the total buildout of the Riverside Estates Subdivision and the Sunrise Terrace Subdivision. These flows were provided to Romtec Utilities who used them to complete the preliminary pump station design. The preliminary design resulted in a 6' I.D. wet well structure and a 687 valve vault structure with 4" discharge piping, valves, and fittings. The pump station will use a 6" force main and will generate a total flow rate of 305 gpm. A spreadsheet depicting the design assumptions and friction losses, along with the conceptual plan and profile, has been included with this analysis.

As directed by city staff, the analysis of the sanitary sewer conveyance system was limited to the portion of the system that will be impacted by the increased flows generated from the proposed developments to the beginning of the new 18" gravity main recently installed by the City of La Center. As can be seen in the provided plan and profile, the force main will discharge into the existing sanitary manhole located at the north end of W E Avenue. This manhole is labeled as Manhole E18 on the City of La Center's Appendix B Collection System Map. After discharging into Manhole E18 the effluent will gravity flow south down W E Avenue through Manhole E17

into Manhole E16 located in the intersection of W E Avenue and W 7<sup>th</sup> Street. At this manhole flows are diverted east to Manholes E15 and E14. Manhole E14 is located in the intersection of W 7<sup>th</sup> Street and Pacific Highway. At Manhole E14 there is a considerable increase in flow which is generated from the majority of Basin E as delineated on the City's Collection System Map. The flow at Manhole E14 is then directed south down Pacific Highway through Manhole E12 into Manhole E7 which is the start of the new 18" gravity main. It should be noted that all of the conveyance pipes from Manhole E18 to E7 are 8".

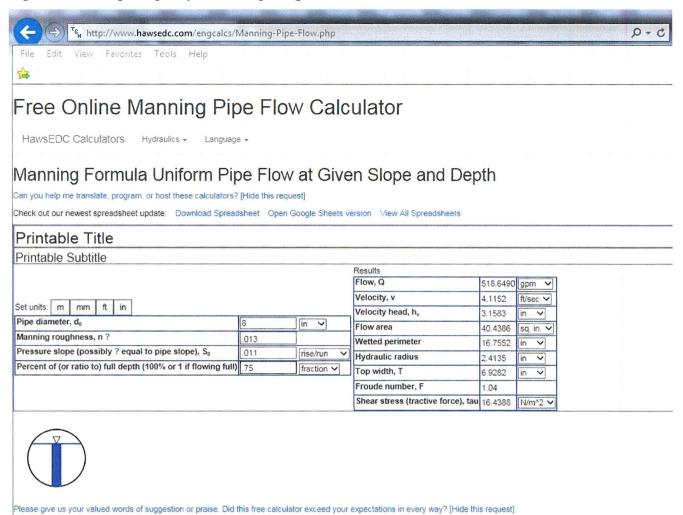
After determining which pipe sections would be impacted, anticipated flow rates were calculated for each section of pipe. These rates were established by utilizing the contributing flow spreadsheet provided by city staff to calculate the existing flows in the pipe and then adding the 305 gpm flows generated from the proposed pump station. The relevant portion of the spreadsheet used to calculate the existing flows has been included with this letter. After calculating the anticipated flows, it was determined, based on existing pipe slopes and contributing flows, that the pipes from Manholes E16 to E15 and Manholes E12 to E7 would be the confining sections of the conveyance system. Pipe slopes were calculated by having a surveyor establish locations and rim elevations of each manhole and obtain measurements from the rim to the inverts of the pipes. The rim elevations and the measure downs were then used to calculate the relative invert elevations. These elevations were then used to calculate the pipe slopes which were used to determine the flow capacity of the pipe.

Pipe capacities were calculated using Manning's Equation. These calculations were made assuming the pipes were flowing 75% full with a Manning's roughness coefficient of 0.013. Using an 8" diameter pipe with a slope of 1.1%, the 75% capacity of the pipe run from Manhole E16 to E15 is 518.65 gpm. This is greater than the 318.4 gpm anticipated flows through this pipe segment. The 75% capacity for the pipe run from Manhole E12 to E7 was calculated at 1,211 gpm using a 6.0% pipe slope. This is substantially greater than the 618.1 gpm anticipated for this pipe segment. Printouts verifying these calculations have been included as Figures 1 and 2 below. Table 1 below shows the comparison of the anticipated flows and the 75% capacity flows for the two relevant pipes.

Table 1: Total Flows and 75% Pipe Capacity Comparison

PIPE SEGMENT ID	UP MH	DOWN MH	EXISTING FLOW	PEAK FLOW	PUMP STATION FLOW	TOTAL FLOW	75% PIPE CAPACITY
			(GPD)	(GPM)	(GPM)	(GPM)	(GPM)
la-75	E-12	E-7	82.9	313.1	305	618.1	1211.3
la-2	E-16	E-15	3.1	13.4	305	318.4	623.4

Figure 1: 75% Pipe Capacity for the Pipe Segment from Manhole E16 to E15



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Figure 2: 75% Pipe Capacity for the Pipe Segment from Manhole E12 to E7

						MARKET CONTRACTOR
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	***************************************					
Printable Title	ACOUNTY OF THE PROPERTY OF THE					
Printable Subtitle						
			Results	1,0,1,0,00		
			Flow, Q	1211.3030		
Set units: m mm ft in			Velocity, v	9.6109	ft/sec V	
Pipe diameter, d <sub>0</sub>	8	in V	Velocity head, h <sub>v</sub>	17.2273	in 🗸	
Manning roughness, n ?	.013		Flow area	40.4386	sq. in. 🗸	
Pressure slope (possibly ? equal to pipe slope), S <sub>0</sub>	.06	rise/run V	Wetted perimeter	16.7552	in V	
Percent of (or ratio to) full depth (100% or 1 if flowing full)		fraction V	Hydraulic radius Top width, T	2.4135	in 🗸	
				6.9282	in 💙	
			Froude number, F	2.43	[Mimon A	
			Shear stress (tractive force), tau	08.0002	N/m^2 ✓	
Please give us your valued words of suggestion or praise. Did	this free calcula	ator exceed your	expectations in every way? [Hide th	is request]		
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After completing the downstream sanitary sewer conveyance analysis we feel that the existing system has more than sufficient capacity to safely convey the additional sanitary effluent from the proposed pump station for the Riverside Estates and Highland Terrace Subdivisions. If you have any questions please feel free to call me at (360) 431-9988.

Sincerely,

Precision Land Services, Inc.

Tim Wines, PE

## APPENDIX A

Flow Calculations for Existing Sanitary Mainline

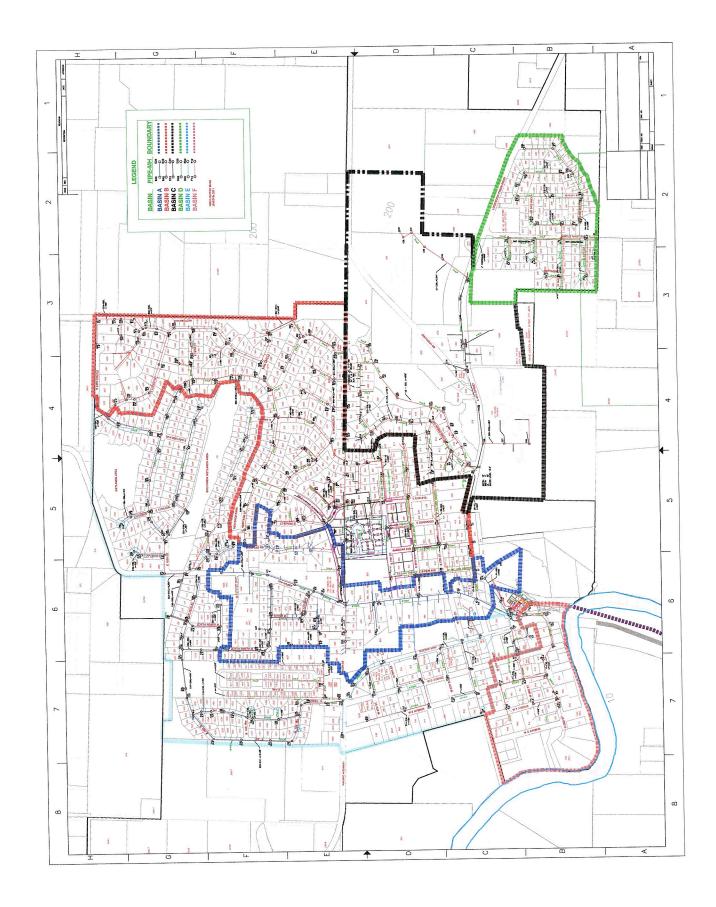
Table A-1 - Sanitary Sewer Collection System Flows

IT ID         MH         DOWN         CONTRIBUTING         TOTAL         TOTAL         PERSONS         FACTOR         FLOW         FLOW           IT ID         MH         MH         ERU         ERU         PERSONS         FACTOR         FLOW         FLOW           IT ID         E-12         E-7         9         402         1.085         3.8         82.9         313.1           ID         E-14         E-14         349         393         1.061         3.8         81.1         306.7           ID         E-14         E-14         6         21         0.019         4.2         9.1         38.3           ID         E-16         E-16         4         15         0.041         4.2         9.1         38.3           ID         E-16         E-16         4         15         0.041         4.2         9.1         13.4           ID         E-16         E-16         4         11         0.030         4.4         1.4         6.3         9.9           ID         E-17         E-16         4         1         1         0.019         4.4         1.4         1.4         6.3			MAINL	MAINLINE E with R	iversi	n Riverside Estates and Highland Terrace	s and	Highland	Terrac	);e	
E-12         E-7         9         402         1.085         3.8         82.9           E-20         E-14         349         393         1.061         3.8         81.1           E-14         E-12         23         44         0.119         4.2         9.1           E-15         E-14         6         21         0.057         4.3         4.3         3.1           E-16         E-15         4         15         0.041         4.3         3.1         7           E-18         E-17         7         0.019         4.4         1.4	PIPE SEGMENT ID	P E	DOWN	CONTRIBUTING		TOTAL	PEAK FACTOR	EXISTING FLOW	PEAK	PUMP STATION FLOW	TOTAL FLOW
E-12         E-14         349         393         1.061         3.8         82.9           E-14         E-14         349         393         1.061         3.8         81.1           E-14         E-12         23         44         0.119         4.2         9.1           E-15         E-14         6         21         0.057         4.3         4.3           E-16         E-15         4         15         0.041         4.3         3.1           E-17         E-16         4         11         0.030         4.4         2.3           E-18         E-17         7         0.019         4.4         1.4						PER 1000		(GPD)	(GPM)	(GPM)	(GPM)
E-12         E-7         9         402         1.085         3.8         82.9           E-20         E-14         349         393         1.061         3.8         81.1           E-14         E-12         23         44         0.119         4.2         9.1           E-15         E-14         6         21         0.057         4.3         4.3         4.3           E-16         E-15         4         11         0.030         4.4         2.3           E-18         E-17         7         0.019         4.4         1.4											
E-20         E-14         349         393         1.061         3.8         81.1           E-14         E-12         23         44         0.119         4.2         9.1           E-15         E-14         6         21         0.057         4.3         4.3         4.3           E-17         E-16         4         11         0.030         4.4         2.3           E-18         E-17         7         0.019         4.4         1.4		E-12	E-7	6	402	1.085	3.8	82.9	313.1	308	618.1
E-14         E-12         23         44         0.119         4.2         9.1           E-15         E-14         6         21         0.057         4.3         4.3         4.3           E-16         E-15         4         15         0.041         4.3         3.1         5           E-17         E-16         4         11         0.030         4.4         2.3         4           E-18         E-17         7         0.019         4.4         1.4         1.4	la-73	E-20	E-14	349	393	1.061	3.8	81.1	306.7	308	611.7
E-15         E-16         E-15         E-16         E-16         E-16         4         4         4.3         4.3         4.3         7         0.041         4.3         3.1         6           E-17         E-16         4         11         0.030         4.4         2.3         7           E-18         E-17         7         7         0.019         4.4         1.4		E-14		23	44	0.119	4.2	9.1	38.3	305	343.3
E-16         E-15         4         15         0.041         4.3         3.1           E-17         E-16         4         11         0.030         4.4         2.3           E-18         E-17         7         7         0.019         4.4         1.4	la-3	E-15	E-14	9	21	0.057	4.3	4.3	18.6	308	323.6
E-17         E-16         4         11         0.030         4.4         2.3           E-18         E-17         7         7         0.019         4.4         1.4	la-2	E-16		4	15	0.041	4.3	3.1	13.4	308	318.4
<b>E-18 E-17</b> 7 7 0.019 4.4 1.4	la-1	E-17	E-16	4	11	0.030	4.4	2.3	9.6	302	314.9
	la-4	E-18	E-17	2	7	0.019	4.4	1.4	6.3	305	311.3

<sup>\*</sup> Highlighted rows indicate pipe segments analysed for conveyance capacity.

## APPENDIX B

City of La Center's Appendix B Collection System Map



## APPENDIX C

Romtec Utilities Preliminary Pump Station Design



## **SYSTEM PIPING**

JOB NAME:	Riverside Estate	es (4in Wet Well I	Piping)	DATE:	6/1	5/17
ELEVATIONS:				New Pipe	Old Pipe	1
FM Discharge:	178.54	]		Water @ Start	Water @ Stop	
Lead Start:	123.85	1	Pump Flow:	305.0	305.0	
Lead Stop:	121.33	1	Static Head:	54.69	57.21	ft
Total Flow:	305	gpm	TDH:	77.2	84.9	ft
Duty Pumps:	1	John .	Est. Efficiency:	50%		1
Total Pumps:	2		Est. HP:	11.9	13.1	]нР
L		J		L	<u> </u>	1
PIPE MATERIAL	AND SIZE			· · · · · · · · · · · · · · · · · · ·		HITTO CONTRACTOR OF THE REPORTED TO
	Wet Well	Valve Vault	Meter Vault	FM1	FM2	FM3
Length:	12	20		2600		
Material:	<b>Ductile Iron</b>	Ductile Iron		PVC		
Class:	Class 53	Class 53		C900 DR18		
Nom. ID:	4"	4"		6"		
True ID:	4.160	4.160	×	6.080		
New C:	130	130		150		
Old C:	110	110		130	a	
Section GPM:	305.0	305.0		305.0		
V (ft/s):[	7.20	7.20		3.37		
PIPE FITTINGS						
	Wet Well	Valve Vault	Meter Vault	FM1	FM2	FM3
Disch Ell:	1					
45 Ell:				5		
90 EII:	1	1		1		
Tee:		3				1
Valve:		2				
Check:		1				
Outlet:				1		
Other (K=.5):						
Total K	0.8	5.6	0.0	2.1	0.0	0.0
FRICTION LOSSES					me	<b>#4</b> ***
	Wet Well	Valve Vault	Meter Vault	FM1	FM2	FM3
Major Loss_New:	0.59	0.98		15.39		
Major Loss_Old:	0.80	1.33		20.06		
Minor Loss:	0.64	4.51	L	0.36	L	
Total Fr	iction Loss New	22.47	] Total	Friction Loss Old:	27.71	]