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# NW La Center Road/I-5 Interchange Improvement Project (MP 16.80) 

La Center, Washington

## Final

# NW La Center Road/I-5 Interchange Improvement Project (MP 16.80) 

La Center, Washington

## Prepared For:

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Project No. 12393.0

September 2013


## STAKEHOLDER ACCEPTANCE

The undersigned parties, including all members of the team from the Washington Department of Transportation (WSDOT) and the Federal Highway Administration (FHWA) concur with the Interchange Justification Report Methods and Assumptions for the NW La Center Road/I-5 Interchange Project as presented in this document.

## WSDOT Region:



## WSDOT Headquarter Design:



Development Services and Access Manager
$\frac{\text { (itite }}{\text { Tite~ }}$ Daten)


## FHWA:


(1) Participation on the Stakeholders Committee and/or signing of this document does not constitute approval of the NW La Center Road/I-5 Interchange Improvement Project Interchange Justification Report.
(2) All members of the Stakeholder Committee will accept this document as a guide and reference as the study progresses through the various stages of project development. If there are any agreed upon changes to the assumptions in this document a revision will be created, endorsed and signed by all the stakeholders.

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## EXECUTIVE SUMMARY

The Exit 16 interchange (at NW La Center Road and NW 319 ${ }^{\text {th }}$ Street, milepost 16.80) along Interstate 5 currently serves the City of La Center and surrounding rural areas. The interchange is a diamond interchange with a two-lane structure over the freeway and stop-controlled access at the ramp terminals. Closely spaced frontage road intersections exist just outside each of the l-5 ramp terminals, posing access management challenges to the operations of the interchange. From a pure capacity standpoint, the existing interchange form is adequate to support existing development within the City of La Center and surrounding rural areas. However, the interchange has been the subject of recent planning studies that examined the impacts of enhancing development opportunities along NW La Center Road on the east and west sides of I-5. One nearterm development opportunity involves 152 acres of land owned by Salishan Mohegan, LLC along the west side of I-5. This property spans the north and south sides of NW $319^{\text {th }}$ Street and is proposed to be developed as a major casino center associated with the Cowlitz Tribe (Cowlitz Reservation Development).

Given the anticipated traffic impacts associated with the Cowlitz Reservation Development, it is recognized that the existing NW La Center Road/I-5 interchange will need to be reconstructed/modified along with the supporting local circulation network in order to provide safe and efficient access to/from l-5.

To support the interchange reconstruction/modification project, the Washington State Department of Transportation (WSDOT) and the Federal Highway Administration (FHWA) requires an Interchange Justification Report (IJR). The IJR documents the interchange planning process, the evaluation of improvement alternatives, the design of the preferred alternative, the impacts to the Interstate system and local street network, and the coordination that supports and justifies the request for an access revision. As a component of the IJR process, the WSDOT Design Manual requires a 'Methods and Assumptions Document' be developed to record assumptions, criteria, and support team decisions used in the IJR. The remainder of this document outlines the Methods and Assumptions that will be used in the NW La Center Road/I-5 Interchange IJR.

## INTRODUCTION AND PROJECT DESCRIPTION

The existing NW La Center Road/I-5 Interchange is a simple diamond interchange form that was constructed to provide access between I-5, the City of La Center, and surrounding rural residential areas. Based on a limited interchange form and the findings of several recent planning studies ${ }^{12}$, the interchange and supporting local circulation system are not capable of safely and efficiently supporting extensive new development. One such development, the Cowlitz Reservation Development involves 152 acres of land owned by the Salishan Mohegan, LLC. This property, which is located on the west side of I-5 and spans the north and south sides of NW $319^{\text {th }}$ Street, is proposed to be developed as a cultural center, housing for tribal elders, a gaming facility, and a potential hotel.

To support the Cowlitz Reservation Development, the existing interchange and supporting local street network will need to be reconfigured to better accommodate intensified traffic patterns at the interchange. An IJR will be completed to document the planning, evaluation, and selection of the necessary interchange replacement. The IJR will be completed with the following focus areas:

- Accommodating multi-modal traffic circulation in a safe and efficient manner,
- Addressing and satisfying regulatory agency approval criteria,
- Minimizing negative impacts to adjacent property owners (right-of-way and access),
- Addressing the existing closely spaced frontage road intersections at NW $319^{\text {th }}$ Street and NW Paradise Park Road.
- Advancing the transportation system in a manner consistent with long-term community aspirations (e.g, La Center Transportation Plan), and
- Ensuring that the selected interchange form supports future expansion to meet the surrounding communities' growth needs through 2036.
- Interchange improvement(s) will not inhibit WSDOT’s ability to improve or expand mainline I-5.

The IJR will focus on the existing NW La Center Road/I-5 Interchange and its functional area along the NW $319^{\text {th }}$ Street/NW La Center Road corridors. This will include the two adjacent frontage roads on either side of the interchange. As illustrated in Figure 1, the project study area will also include the two upstream/downstream (SR 501 Exit 14 at milepost 14.17 and SR 503 Exit 21 at milepost 21.08 ) interchanges along the I-5 corridor. Analysis included in the IJR will formally document these minimal impacts. The following sections describe the existing conditions of the interstate system and the non-interstate highway/local transportation system within the project study area.

[^0]||kittelson.com|fs|H_Portland|projfile|12393 - Cowlitz Reservation Development|dwgs|figs|FreewayAnalysis_figures.dwg Dec 18, 2012-11:51am - klaustsen $\quad$ Layout Tab: 1_Site Vicinity_TG


## I-5 Mainline

Within the interchange improvement study area, l-5 is a 6-lane, median-separated, interstate highway. The WSDOT State Highway Log classifies this section of I-5 as Rural. Existing average annual daily traffic (AADT) for this section of I-5 is approximately 65,350 vehicles per day based on the most recent 2011 data at nearby R045 permanent traffic recorder station located at milepost 20.14. The posted speed limit along this segment of $\mathrm{I}-5$ is 70 mph .

## NW La Center Road/I-5 Interchange

The NW La Center Road interchange is a diamond interchange located at milepost 16.80. The interchange is located within the City of La Center. The interchange consists of single-lane on- and off-ramps with unsignalized ramp terminals at NW La Center Road. Traffic volumes on I-5 at the NW La Center Road interchange are approximately 62,000 vehicles per day.

The ramp terminals are located approximately 535 feet (centerline-to-centerline) apart and are separated by a relatively narrow two-lane overpass structure with no formal pedestrian accommodations. The I-5/NW La Center Road interchange is served by several local roadways that provide connectivity between I-5, La Center, and the surrounding rural areas. These facilities are documented below.

## NW La Center Road

NW La Center Road is an east-west, two-lane roadway that connects I-5 and the City of La Center. Clark County classifies NW La Center Road as a Major Collector. Within the vicinity of the interchange, there are no sidewalks or bicycle lanes along either side of the roadway. Based on recent traffic count information, the existing ADT east of the I-5 interchange is approximately 11,000 vehicles per day.

## NW 319 ${ }^{\text {th }}$ Street

West of I-5, NW La Center Road becomes NW 319 ${ }^{\text {th }}$ Street. This east-west roadway is classified as a Rural Minor Collector by Clark County and primarily serves the rural residential development located between I-5 and the Columbia River to the west. Existing ADT along this roadway is approximately 1,500 vehicles per day.

## NW 31 ${ }^{\text {st }}$ Avenue

NW $31^{\text {st }}$ Avenue is a north-south roadway located on the west side of I-5 south of NW $319^{\text {th }}$ Street. Clark County classifies NW $31^{\text {st }}$ Avenue as a Rural Major Collector. Oriented parallel to I-5, this roadway acts as a rural frontage road to $1-5$ providing a continuous connection between NW $319^{\text {th }}$ Street and the City of Ridgefield to the south. The intersection of NW $31^{\text {st }}$ Avenue with NW $319^{\text {th }}$ Street is located approximately 100 feet (centerline-to-centerline) from the l-5 southbound ramp terminal.

## NW Paradise Park Road

NW Paradise Park Road is a north-south roadway located on the east side of I-5. Clark County classifies NW Paradise Park Road as a Local roadway. As with NW 31 ${ }^{\text {st }}$ Avenue, NW Paradise Park Road acts as a rural
frontage road to I-5 and connects to NW La Center Road approximately 125 feet (centerline-to-centerline) east of the northbound ramp terminal. NW Paradise Park Road provides access to Paradise Point State Park.

## SR 503/I-5 Interchange

The SR 503/I-5 interchange is a split diamond interchange located in Woodland, WA. This interchange is located approximately 4.28 miles north of the NW La Center Road/I-5 interchange at milepost 21.08 in Woodland, WA.

## SR 501/I-5 Interchange

The SR 501/I-5 Interchange is diamond interchange located approximately 2.63 miles south of the NW La Center Road/l-5 interchange at milepost 14.17. Recently reconstructed to include a six-lane overpass and signalized ramp terminals, this interchange primarily serves the City of Ridgefield and the surrounding rural residential areas.

## I-5 Weigh Station

An existing weigh station for northbound I-5 traffic is located south of the La Center/l-5 interchange at milepost 15.5.

## PROJECT DESCRIPTION

The NW La Center Road interchange improvement project is expected to mitigate the impacts of the proposed Cowlitz Reservation Development at full-buildout in year 2016. For the purposes of the analysis, the proposed Cowlitz Reservation Development is anticipated to include the following uses:

- 2,440 gaming positions (the IJR will study 3,500 gaming positions for a conservative analysis)
- Up to 3,450 parking spaces
- 4 restaurants
- 5,000-6,000 square feet of retail space
- Casino bars
- Event Center with seating for up to 1,500 guests
- Valet parking services
- 250-room hotel

The traffic impacts of such a development are expected to necessitate the reconstruction of the existing NW La Center Road/I-5 interchange and realignment of NW 31 ${ }^{\text {st }}$ Avenue and NW Paradise Park Road. As previously stated, the IJR will formally document the planning, alternatives development, alternatives evaluation, and selection of the preferred interchange form to address the anticipated project traffic as well as the background traffic growth in the study area. To support this effort, the following sections highlight the study parameters and assumptions that will be incorporated into the IJR analysis.

## ANALYSIS YEARS/PERIODS

Based on preliminary scoping efforts with the City of La Center, Clark County, WSDOT and FHWA, three analysis years, 2012, 2016 and 2036, will be required. The 2016 study year is assumed to represent the build out year of the Cowlitz Reservation Development and will be used for identifying mitigations that will be needed for and funded exclusively (no federal, state, or local dollars will be used to plan, design, and/or construct the project) by Salishan Mohegan, LLC. The 2036 study year scenario is informational for WSDOT to ensure that near-term interchange improvements don't preclude the ability to provide future long-term improvements.

In order to assess the impact of the Cowlitz Reservation Development, conditions will be analyzed for the following time periods based daily profile counts of the surrounding roadways and the anticipated trip generation profile of the casino:

- Weekday morning peak period (7:00-9:00 a.m.)
- Weekday evening roadway peak period (4:00-6:00 p.m.)
- Friday peak period (4:00-6:00 p.m.) [This time period represents when traffic volumes in the site vicinity would peak in the future with trips associated from the proposed Cowlitz Reservation Development]


## PROJECT AND STUDY AREAS

The project study area will focus on the NW La Center Road/I-5 Interchange and immediately adjacent frontage road network. A transportation impact analysis of intersections impacted by the Cowlitz Reservation Development will be prepared to address the transportation system impacts beyond the NW LaCenter Road/I-5 Interchange on the local LaCenter and Clark County roadway network. The following NW La Center Road/l-5 interchange intersections have been identified for detailed operations analyses within the IJR:

- NW 31 ${ }^{\text {st }}$ Avenue/NW 319 ${ }^{\text {th }}$ Street;
- I-5 Southbound Ramp/NW La Center Road;
- I-5 Northbound Ramp/NW La Center Road; and
- Paradise Road/NW La Center Road

In addition to the intersection operations, the IJR will include I-5 mainline and merge/diverge analyses for the following locations:

- I-5 at the NW La Center Road interchange ramps; and
- I-5 at the weigh station located approximately 1.25 miles south of the NW La Center Road interchange.

The project study area extends to the northern interchange (I-5/SR 503 in Woodland) and southern interchange (I-5/SR 501 in Ridgefield).

## TRAFFIC OPERATIONS ANALYSIS

In total, the traffic operations analyses will be performed for the following scenarios:

- Existing 2012 Weekday AM Peak Hour
- Existing 2012 Weekday PM Peak Hour
- Existing 2012 Weekday Friday PM Peak Hour
- 2016 Background Weekday AM Peak Hour
- 2016 Background Weekday PM Peak Hour
- 2016 Background Weekday Friday PM Peak Hour
- 2016 w/Cowlitz Reservation Development (No-Build), Weekday AM Peak Hour
- 2016 w/Cowlitz Reservation Development (No-Build), Weekday PM Peak Hour
- 2016 w/Cowlitz Reservation Development (No-Build), Weekday Friday PM Peak Hour
- 2016 w/Cowlitz Reservation Development and interchange improvements (Build), Weekday AM Peak Hour
- 2016 w/Cowlitz Reservation Development and interchange improvements (Build), Weekday PM Peak Hour
- 2016 w/Cowlitz Reservation Development and interchange improvements (Build), Weekday Friday PM Peak Hour
- 2036 Background (No-Build) Weekday AM Peak Hour
- 2036 Background (No-Build) Weekday PM Peak Hour
- 2036 Background (No-Build) Weekday Friday PM Peak Hour
- 2036 w/Cowlitz Reservation Development and 2016 identified interchange improvements (Build), Weekday AM Peak Hour
- 2036 w/Cowlitz Reservation Development and 2016 interchange improvements (Build), Weekday PM Peak Hour
- 2036 w/Cowlitz Reservation Development and 2016 interchange improvements (Build), Weekday Friday PM Peak Hour


## EXISTING CONDITIONS ANALYSIS

The existing operations and level of service will be assessed at the identified study intersections/l-5 mainline/merge-diverge areas during the three peak hour analysis periods using 2012 traffic volumes. These volumes were developed using data collected in mid-September 2012 and data provided by WSDOT for the permanent traffic recorder (PTR) station R045 located on I-5 north of the NW La Center Road/I-5 Interchange in the study area. The process used to develop traffic volumes for the l-5 mainline and interchange ramps that are representative of typical traffic volumes was developed based on conversation with WSDOT staff. The existing traffic volumes development is described in detail in Appendix $A$.

Synchro/SimTraffic and HCS 2010 will be used for the traffic operation analysis. Synchro and SimTraffic (Version 7) will be used to analyze signalized and stop-controlled intersections. HCS 2010 will be used to analyze the $\mathrm{l}-5$ mainline performance and the interchange merge/diverge areas.

## 2016 BACKGROUND ANALYSIS

This analysis will determine traffic operations at the study intersections/l-5 mainline/merge-diverge areas during all three study periods in the year 2016 without any improvements or changes to the interchange/local roadway network. Traffic volumes for the year 2016 will be derived based on the 2011 Clark County Metropolitan Transportation Plan (MTP) model. Where feasible, the projected volumes will be calculated by first using a straight-line interpolation between the base 2010 and future year 2036 traffic volume projections from the model and then post-processing (using the NCHRP 255 methodology) the results. In-process development data has been requested ${ }^{3}$ from the City of La Center, City of Ridgefield, City of Woodland, and Clark County and included as part of year 2016 forecast traffic volumes.

City of La Center, City of Ridgefield, and Clark County transportation improvement plans will be reviewed for the surrounding area to determine how any planned improvements may impact access to the site and operations at the study intersections.

Synchro/SimTraffic, and HCS 2010 will be used for the traffic operation analysis. Synchro and SimTraffic (Version 7) will be used to analyze signalized and stop-controlled intersections. HCS 2010 will be used to analyze the l-5 Mainline performance and the interchange merge/diverge areas.

## 2016 WITH COWLITZ RESERVATION DEVELOPMENT ANALYSIS

Traffic operations at the study intersections/l-5 mainline/merge-diverge areas for all three study periods will be estimated in the year 2016 with the additional traffic volumes generated by the Cowlitz Reservation Development. The expected trip generation form the Cowlitz Reservation Development will then be added to the 2016 background volumes to create this analysis scenario. The assumption is that no improvements are made to the roadway network or intersections. In addition, no capacity improvements to l-5 will be assumed in the study area by 2016.

Synchro/SimTraffic, and HCS 2010 will be used for the traffic operation analysis. Synchro and SimTraffic (Version 7) will be used to analyze signalized and stop-controlled intersections. HCS 2010 will be used to analyze the $\mathrm{I}-5$ Mainline performance and the interchange merge/diverge areas.

It is anticipated that roundabouts will be a design consideration in the development and analysis of interchange improvement alternatives. In these instances, the traffic analysis software SIDRA will be used to conduct the analysis. In recognition of WSDOT standards, Appendix B outlines several SIDRA variables that will be changed from the default parameters.

[^1]
## TRIP GENERATION AND ASSIGNMENT

Trip generation estimates for the proposed Cowlitz Reservation Development will be based on data from other similar casino developments (a separate Trip Generation memorandum will be prepared for review and consent by all stakeholders prior to the publication of the Draft IJR). Based on past experience and a preliminary assessment of the data, we recommend calculating trips per gaming position ${ }^{4}$. Data indicates that the number of trips generated at a casino is more highly correlated to the number of gaming positions than the square footage of gaming space or the size of the entire development. We will assign the sitegenerated traffic to the study intersections using the estimated trip distribution patterns within the site vicinity for each of the three analysis periods. The proposed peak hour trip assignments for the Cowlitz Reservation Development are shown in Appendix $C$.

## 2016 WITH COWLITZ RESERVATION DEVELOPMENT AND INTERCHANGE IMPROVEMENTS ANALYSIS

This scenario will present the proposed mitigation to address the impacts of the proposed Cowlitz Reservation Development. The operations at the study intersections/l-5 mainline/merge-diverge areas for the three analysis periods based on projected 2016 traffic volumes and the Cowlitz Reservation Development. An initial level of analysis will involve using forecasted volumes and potentially Synchro and HCS 2010 to determine the two critical time periods of this 2016 scenario. Based on our understanding of the proposed development, it is expected that the two critical time periods will be the Weekday p.m. peak hour and the Friday Evening/Weekend peak hour period.

If necessary, a VISSIM model of the study area will be created if a preferred interchange alternative scenario does not meet the operational performances specified in the body of this report. Additional details of the VISSIM modeling is outlined in Appendix D.

## 2036 BACKGROUND ANALYSIS

This analysis will determine traffic operations at the study intersections/l-5 mainline/merge-diverge areas during all three study periods in the year 2036 without any improvements or changes to the interchange/local roadway network. Traffic volumes for the year 2036 will be derived based on the 2011 Clark County Metropolitan Transportation Plan (MTP) model.

## 2036 WITH COWLITZ RESERVATION DEVELOPMENT AND 2016 INTERCHANGE IMPROVEMENTS ANALYSIS

A long-term 2036 scenario will be analyzed to demonstrate the long-term impacts of the Cowlitz Reservation Development. Future traffic volumes for the 2036 scenario will be projected based on the same methodology previous described above. The analysis will be used to ensure that the proposed interchange project does not preclude the development of future capacity needs and is designed in such a way that it can be readily expanded to meet the year 2036 needs.

[^2]
## SELECTION OF MEASURES OF EFFECTIVENESS

Multiple Measures of Effectiveness (MOE) will be used for the operational analysis of the different scenarios. Level of Service (LOS) is the critical measure to determine whether the project can meet the minimum operation requirements.

WSDOT

The WSDOT Design Manual, Chapter 320 describes the measure of effectiveness (MOE) used for determining a highway facilities' level of service (LOS) as follows:

- The level of service (LOS) for operating state highway facilities is based upon measures of effectiveness (MOEs), in accordance with the latest version of the Highway Capacity Manual.
- These MOEs (see Table 1 below) describe the measures best suited for analyzing state highway facilities, such as freeway segments, signalized intersections, and on- or off-ramps. Depending on the facility, WSDOT LOS thresholds are LOS C and LOS D on state highway facilities.

Table 1 WSOT Measures of Effectiveness by Facility Type

| Type of Facility | Measure of Effectiveness (MOE) |
| :--- | :--- |
| Basic Freeway Segments | Density (pc/mi/ln) |
| Ramps | Density (pc/mi/ln) |
| Ramp Terminals | Delay (sec/veh) |
| Multilane Highways | Density (pc/mi/ln) |
| Two-Lane Highways | Percent Time Spent Following <br> Average Travel Speed (mi/hr) |
| Signalized Intersections | Control Delay Per Vehicle (sec/veh) |
| Unsignalized Intersections | Average Control Delay Per Vehicle (sec/veh) |
| Urban Streets | Average Travel Speed (mi/hr) |

## Intersection Analysis - Level of Service (LOS), Delay, Volume/Capacity (V/C) Ratio, Queues

For intersection analysis, LOS is determined by the average delay (seconds). The 2010 Highway Capacity Manual (HCM) provides LOS criteria for intersections, illustrated in Table 2. As shown in the table, the same LOS criteria will be used for both signalized intersections and roundabouts.

Table 2 LOS Criteria for Intersection with Traffic Control (HCM 2010)

| LOS | Traffic Signals and Roundabouts | Stop Signs and Yield Signs |
| :---: | :---: | :---: |
|  | Total Delay per Vehicle (sec) | Control Delay per Vehicle (sec) |
|  | $\leq 10$ | $0-10$ |
| B | $>10$ and 20 | $>10$ and 15 |
| C | $>20$ and 35 | $>15$ and 25 |
| D | $>35$ and 55 | $>25$ and 35 |
| E | $>55$ and 80 | $>35$ and 50 |
| F | $>80$ | $>50$ |

Per discussions with WSDOT staff, it has been noted that the existing interchange is in a predominately rural area. However, it is anticipated that the proposed Cowlitz Reservation Development will change the character of the area to a more urban setting. Therefore, the LOS C standard will be used at the interchange ramp terminals for the existing conditions analysis and the 2016 analysis, while the LOS D standard will be used for the 2036 analysis.

## Mainline LOS, Density, Speed, Travel Time

For freeway analysis (including mainline analysis of I-5, merge, and diverge), LOS is determined by the density of traffic. The HCM provides LOS criteria for freeway merge, diverge, and weave, shown in Table 3.

Table 3 LOS Criteria for Freeway Merge/Diverge/Weave (HCM 2010)

|  | Maximum Density (pc/mi/ln) |  |
| :---: | :---: | :---: |
|  | Merge/Diverge | Weave |
| A | $\leq 10$ | $0-10$ |
| B | $>10-20$ | $>10-20$ |
| C | $>20-28$ | $>20-28$ |
| D | $>28-35$ | $>28-35$ |
| E | $>35$ | $>35$ |
| F | Demand Exceeds Capacity | Demand Exceeds Capacity |

Speed (mph) and travel time (minutes) are also indictors of the performance of an individual segment and the overall freeway facility. HCS 2010 will be the primary software for freeway facility analysis.

The base saturation flow rate for all signalized intersection analyses will be 1,900.

## INTERCHANGE JUSTIFICATION REPORT REQUIREMENTS

As outlined by the WSDOT Design Manual, there are eight policy point requirements that need to be addressed as part of an IJR. These eight policy points are outlined below:

- Policy Point 1 - Need for Access Point Revision
- The IJR will describe the need for the interchange improvement and why the existing interchange is not sufficient to meet the design year needs.
- Data analysis will be provided to support the needs findings.
- Policy Point 2 - Reasonable Alternatives
- This policy point will be one of the main focal points for the NW La Center Road/l-5 Interchange Improvement Project.
- All reasonable alternatives will be described and considered in the interchange form alternatives analysis. These will include the design options, locations, and transportation system management-type improvements to meet the proposal design year needs.
- All reasonable design alternatives will be evaluated and documented in the evaluation process.
- Policy Point 3 - Operational and Safety Analyses
- This policy point will be one of the main focal points for the NW La Center Road/I-5 Interchange Improvement Project.
- An operational and safety analysis will be conducted per WSDOT IJR guidelines.
- Policy Point 4 - Access Connections and Design
- Access within the vicinity of the interchange will be critical component of the NW La Center Road/I-5 Interchange Improvement Project given the presence of the two existing frontage roads on both sides of the interchange.
- The analysis will include documentation on how the interchange improvements relate to the WSDOT Design Manual spacing criteria. Any design deviations needed to support the preferred interchange design will be fully addressed in this section.
- Policy Point 5 - Land Use and Transportation Plans
- Future land use and transportation considerations will be accounted for the in the nearand long-term operations analyses.
- The interchange improvement proposal will address consistency with local and regional land use and transportation plans.
- Policy Point 6 - Future Interchanges
- The proposed interchange improvement will demonstrate compliance with other planned access points and revisions along the l-5 study corridor.
- Policy Point 7 - Coordination
- In parallel with the IJR, a separate transportation impact analysis will be prepared for the Cowlitz Development Project. The applicable traffic volume increases from this separate study effort will be included at the IJR study intersections and appropriate references will be made as necessary to ensure coordination and consistency.
- Policy Point 8 - Environmental Processes
- A separate NEPA process is being developed in parallel with the IJR.

To meet these requirements, all eight policy points will be addressed in the NW La Center Road/I-5 Interchange Improvement Project IJR.

Appendix A

## Existing Traffic Volumes Development

## EXISTING TRAFFIC VOLUMES DEVELOPMENT

A variety of traffic volume data were utilized as part of this transportation analysis, including:

- Twenty-four hour tube counts collected at all four ramps of the l-5/La Center Road Interchange from September 2012;
- Basic Axle Classification Report data for permanent traffic recorder (PTR) R045, located on I-5 at milepost 20.14 for portions of 2010, 2011, and 2012;
- Diamond Traffic Counter sixty minute counts for ramps of the l-5/La Center interchange from March 2011.


## NW La Center Road/I-5

KAI collected twenty-four hour tube counts at the ramps of the l-5/La Center Road interchange for Friday, September 14, 2012 through Sunday, September 23, 2012. These automated tube counts collected hourly traffic volumes and vehicle classification by direction. The average of the Tuesday through Thursday data was used to develop the weekday AM peak (7:00 AM - 9:00 AM) and weekday PM peak (4:00 PM - 6:00 PM) volumes and truck percentages. The data from Friday, September 14 and Friday, September 21, 2012 was used to develop the Friday peak (4:00 PM - 6:00 PM) volumes and truck percentages. The data was not seasonally adjusted, as traffic reports from station R045 suggest that September traffic volumes are higher than average. This is further shown in Attachment A, which includes the monthly conversion factors for station R045. The factor to convert September average weekday traffic (AWDT) to annual average daily traffic (AADT) is 0.96, indicating that September traffic is higher than average traffic. Therefore, using the September counts is conservative. Attachment A also includes an analysis of PTR data provided by Ray Shank that justifies the use of September count data.

## I-5 Mainline

WSDOT provided a basic axle classification report for ATR station R045, which is located on I-5 at milepost 20.14, just north of the I-5/La Center Road interchange, from September 2012. Traffic volumes at the station from Wednesday, September 19, 2012 through Monday, September 24, 2012 were available. Therefore, an average of the weekday AM peak period (7:00 AM - 9:00 AM) and weekday PM peak period (4:00 PM - 6:00 PM) traffic volumes from Wednesday and Thursday were used to estimate the weekday peak periods. In order to confirm the appropriateness of this data, it was compared to additional data at the ATR station, which suggested the September 2012 data is fairly typical for the freeway. This comparison is provided in Attachment 2, which includes peak volume data at station R045 from September 2010 and June 2012. Also, historical WSDOT data from R045 indicates that September is one of the higher months in terms of traffic volumes (as explained above and demonstrated in Attachment A). Therefore, using September data is conservative.

The volumes at the ATR station were used in conjunction with the ramp volumes to extrapolate the volumes on I-5 south of the NW La Center Road/I-5 interchange. The truck percentages recorded at the station were used for all of I-5.

STATE OF WASHINGTON - DEPARTMENT OF TRANSPORTATION
R I P S S Y S T E M

CONVERSION FACTORS: AVERAGE WEEKDAY TRAFFIC (AWDT) TO ANNUAL AVERAGE DAILY TRAFFIC (AADT) RURAL STATIONS

| MONTH | AWDT FACTOR |  | AWDT FACTOR |  | AWDT FACTOR |  | AWDT FACTOR |  | AWDT FACTOR |  | AWDT FACTOR |  | AWDT FACTOR |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | R014 |  | R020 |  | R023 |  | R037 |  | R038 |  | R039 |  | R040W |  |
| JANUARY | 10379 | 1.64 | 5374 | 1.13 | 8573 | 1.29 | 899 | 1.85 | 2446 | 2.04 | 21331 | 1.57 | 737 | 2.34 |
| FEBRUARY | 11520 | 1.48 | 5597 | 1.09 | 8379 | 1.32 | 988 | 1.69 | 3111 | 1.60 | 23374 | 1.43 | 939 | 1.84 |
| MARCH | 13542 | 1.26 | 5968 | 1.02 | 9519 | 1.16 | 730 | 2.28 | 2476 | 2.01 | 23650 | 1.42 | 895 | 1.93 |
| APRIL | 14694 | 1.16 | 6287 | . 97 | 10090 | 1.09 | 756 | 2.20 | 2488 | 2.00 | 24596 | 1.36 | 875 | 1.97 |
| MAY | 16080 | 1.06 | 6225 | . 98 | 10603 | 1.04 | 1178 | 1.41 | 2973 | 1.68 | 27405 | 1.22 | 1131 | 1.53 |
| JUNE | 18375 | . 93 | 6431 | . 95 | 11624 | . 95 | 1946 | . 86 | 3435 | 1.45 | 30724 | 1.09 | 1514 | 1.14 |
| JULY | 20766 | . 82 | 6830 | . 89 | 13173 | . 84 | 2751 | . 61 | 4736 | 1.05 | 34678 | . 97 | 2058 | . 84 |
| AUGUST | 19917 | . 86 | 7491 | . 81 | 13389 | . 82 | 2598 | . 64 | 4594 | 1.08 | 34974 | . 96 | 1980 | . 87 |
| SEPTEMBER | 16819 | 1.01 | 7509 | . 81 | 11733 | . 94 | 2115 | . 79 | 3588 | 1.39 | 30199 | 1.11 | 1833 | . 94 |
| OCTOBER | 14669 | 1.16 | 6739 | . 90 | 10267 | 1.07 | 1693 | . 98 | 2966 | 1.68 | 26444 | 1.27 | 1345 | 1.28 |
| NOVEMBER | 14439 | 1.18 | 5988 | 1.02 | 9709 | 1.14 | 968 | 1.72 | 2517 | 1.98 | 24541 | 1.37 | 980 | 1.76 |
| DECEMBER | 12652 | 1.35 | 5565 | 1.09 | 9852 | 1.12 | 1090 | 1.53 | 3798 | 1.31 | 26149 | 1.28 | 1052 | 1.64 |
| AADT | 17032 |  | 6091 |  | 11031 |  | 1666 |  | 4982 |  | 33518 |  | 1726 |  |
|  | R041 |  | R042 |  | R043 |  | R045 |  | R047E |  | R047S |  | R047W |  |
| JANUARY | 3385 | 1.39 | 8086 | 1.78 | 4535 | 1.13 | 55528 | 1.18 | 10682 | 1.40 | 2795 | 1.85 | 9168 | 1.34 |
| FEBRUARY | 3652 | 1.28 | 8993 | 1.60 | 4566 | 1.12 | 55963 | 1.17 | 11081 | 1.35 | 2978 | 1.74 | 9445 | 1.30 |
| MARCH | 3923 | 1.20 | 10410 | 1.38 | 4610 | 1.11 | 60528 | 1.08 | 11399 | 1.31 | 3257 | 1.59 | 9581 | 1.28 |
| APRIL | 4155 | 1.13 | 12065 | 1.19 | 5079 | 1.01 | 62155 | 1.05 | 13025 | 1.15 | 3760 | 1.38 | 10048 | 1.22 |
| MAY | 4492 | 1.04 | 12552 | 1.15 | 5248 | . 97 | 63336 | 1.03 | 14443 | 1.03 | 4287 | 1.21 | 11966 | 1.03 |
| JUNE | 4852 | . 97 | 14410 | 1.00 | 5328 | . 96 | 68173 | . 96 | 15687 | . 95 | 5030 | 1.03 | 12926 | . 95 |
| JULY | 5236 | . 90 | 16740 | . 86 | 5890 | . 87 | 72012 | . 91 | 18019 | . 83 | 6275 | . 83 | 14568 | . 84 |
| AUGUST | 5327 | . 88 | 17019 | . 85 | 6294 | . 81 | 72811 | . 90 | 17679 | . 84 | 6071 | . 85 | 14492 | . 85 |
| SEPTEMBER | 5140 | . 91 | 13466 | 1.07 | 5637 | . 91 | 67949 | . 96 | 16049 | . 93 | 5020 | 1.03 | 13581 | . 91 |
| OCTOBER | 4629 | 1.01 | 12238 | 1.18 | 5035 | 1.01 | 63914 | 1.02 | 15127 | . 99 | 4535 | 1.14 | 12805 | . 96 |
| NOVEMBER | 4215 | 1.11 | 11291 | 1.27 | 4518 | 1.13 | 63466 | 1.03 | 12281 | 1.22 | 3564 | 1.45 | 10327 | 1.19 |
| DECEMBER | 4043 | 1.16 | 10480 | 1.37 | 4475 | 1.14 | 62679 | 1.04 | 12635 | 1.18 | 3799 | 1.36 | 10908 | 1.13 |
| AADT | 4689 |  | 14396 |  | 5106 |  | 65349 |  | 14932 |  | 5180 |  | 12293 |  |
|  | R048 |  | R054 |  | R055 |  | R057 |  | R058 |  | R061 |  | R063 |  |
| JANUARY | 11870 | 1.35 | 1791 | 1.16 | 6359 | 1.67 | 2053 | 2.04 | 1636 | 2.56 | 10422 | 1.33 | 6622 | 1.23 |
| FEBRUARY | 12730 | 1.25 | 1756 | 1.19 | 7117 | 1.49 | 2143 | 1.95 | 2045 | 2.05 | 11574 | 1.20 | 6934 | 1.17 |
| MARCH | 13781 | 1.16 | 1984 | 1.05 | 8223 | 1.29 | 2352 | 1.78 | 1771 | 2.37 | 12856 | 1.08 | 7338 | 1.11 |
| APRIL | 14972 | 1.07 | 2070 | 1.01 | 9133 | 1.16 | 2775 | 1.51 | 2165 | 1.94 | 12918 | 1.07 | 7711 | 1.06 |
| MAY | 15747 | 1.01 | 1940 | 1.07 | 9767 | 1.09 | 3252 | 1.29 | 2862 | 1.46 | 13203 | 1.05 | 8294 | . 98 |
| JUNE | 16815 | . 95 | 2183 | . 95 | 11256 | . 94 | 3816 | 1.10 | 3345 | 1.25 | 14358 | . 96 | 8718 | . 93 |
| JULY | 17658 | . 90 | 2494 | . 84 | 12958 | . 82 | 4865 | . 86 | 4628 | . 91 | 15584 | . 89 | 9467 | . 86 |
| AUGUST | 17380 | . 92 | 2703 | . 77 | 12814 | . 83 | 4776 | . 88 | 4451 | . 94 | 15920 | . 87 | 9419 | . 86 |
| SEPTEMBER | 16619 | . 96 | 2438 | . 85 | 10960 | . 97 | 3751 | 1.12 | 3496 | 1.20 | 14059 | . 99 | 8564 | . 95 |
| OCTOBER | 15947 | 1.00 | 2255 | . 92 | 9463 | 1.12 | 3390 | 1.23 | 2857 | 1.47 | 13364 | 1.04 | 8101 | 1.01 |
| NOVEMBER | 14191 | 1.13 | 1848 | 1.13 | 8799 | 1.21 | 2789 | 1.50 | 2166 | 1.93 | 12634 | 1.10 | 7658 | 1.06 |
| DECEMBER | 13372 | 1.19 | 1820 | 1.14 | 8213 | 1.29 | 3038 | 1.38 | 2866 | 1.46 | 12027 | 1.15 | 7412 | 1.10 |
| AADT | 159 |  |  |  | 106 |  |  |  |  |  | 138 |  |  |  |

* OREGON-OWNED RECORDERS AND FERRY TERMINALS EXCLUDED


## Kelly Laustsen

| From: | Shank, Ray [ShankR@wsdot.wa.gov](mailto:ShankR@wsdot.wa.gov) |
| :--- | :--- |
| Sent: | Thursday, November 29, 2012 3:00 PM |
| To: | Matt Hughart |
| Cc: | Keniston, Rick; Bellinger, Dave; Nova, Robert; Clark, Mike; Kelly Laustsen; Jeff Whitman |
| Subject: | Cowlitz Reservation Development - Volume Methodology Discussion |

Matt,

The following comments/guidance has been provided by our headquarters staff regarding the development of traffic volumes to be used in the analysis of the 5/LaCenter Interchange.

## Justification Discussion for using September 2012 Count Data

The Permanent Traffic Recorder (PTR) R045 is used for factoring mainline I-5 from the LaCenter Interchange northward. We use PTR R109 for factoring the mainline I-5 through the SR 501 (Ridgefield) Interchange.

Looking into this data, the seasonality we ascribe to both the end of SR 501 and the end of 503 (and therefore should reflect the ramps as well) comes from an average of urban sites we label GR-02. This is a much flatter seasonal curve than R045 or R109. The figures below reflect 2011 total monthly volume divided by total annual volume for GR-02, R045 and R109. What they show (somewhat cryptically) is that the 7-day average from your short count is likely only going to be a few percent off from the annual average. Since this is well within the margin of error for factoring, we would just consider the September count average as equivalent to the annual average.

| Factor | Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| GR-02 | 7.9\% | 7.4\% | 8.5\% | 8.3\% | 8.6\% | 8.7\% | 8.8\% | 9.0\% | 8.5\% | 8.4\% | 7.9\% | 8.2\% |
| R045 | 7.2\% | 6.8\% | 8.1\% | 8.0\% | 8.4\% | 8.8\% | 9.7\% | 10.0\% | 8.8\% | 8.4\% | 7.9\% | 8.0\% |
| R109 | 7.4\% | 7.0\% | 8.2\% | 8.1\% | 8.5\% | 8.8\% | 9.5\% | 9.7\% | 8.7\% | 8.3\% | 7.9\% | 8.1\% |

The peak hour volumes from the short count are anticipated to be appreciably lower than a $30^{\text {th }}$ highest hour. The fact that R045 has significantly different temporal trends than the ramps means it is not appropriate as a factor source.

Therefore to justify using the available September data, we suggest multiplying the short count peak hour volume by 1.3 and determine if the higher volume would have any practical implication for design over the un-factored peak. If the answer is no, just use the short count peak as is. If the answer is yes, we will have to discuss further to determine an appropriate methodology.

Comparing Counts at Adjacent Interchanges

Weekday counts are available for all ramps of the Ridgefield, LaCenter, and Woodland Interchanges in March 2011. We can utilize these short counts along with the data you collected at the LaCenter Interchange in September 2012 to create a factor to derive estimated September 2012 volume data for the adjacent interchanges. In order to create this factor, we're assuming similar temporal trends between these three interchanges.

After looking at the September 2012 data, it appears that the peak hour on Friday is slightly lower than that of the weekday peak hour. To be conservative in our evaluation, the weekday peak volume data for the ramps will be applied as the Friday peak hour volume.

Additional Data Effort

- PTR R045 Validation - I have requested a status update for this effort and will let you know when the validation has been completed.
- SR 503/Woodland Interchange Study - After reviewing the study, the forecast year was 2025 and likely won't help with your volume projection for the Woodland interchange. However, if you think it might help I can forward you a CD containing a copy.
- Weigh Station Data - I should receive some information tomorrow regarding the number of commercial vehicles that use the weigh station. I will forward this information onto you when it becomes available.

Please review and let me know if you have any questions.

## Ray Shank

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## I-5 Data Comparison

PTR Station R045

| Wed/Thurs Avg | Northbound |  |  |  | Southbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 9/19-20/2012 | 1 | 2 | 3 | Total | 4 | 5 | 6 | Total |
| 6:00 AM | 517 | 638.5 | 414 | 1569.5 | 442 | 714 | 503 | 1659 |
| 7:00 AM | 571.5 | 840.5 | 567.5 | 1979.5 | 490 | 815.5 | 564.5 | 1870 |
| 8:00 AM | 557 | 722.5 | 453.5 | 1733 | 479.5 | 759 | 477 | 1715.5 |
| 4:00 PM | 792 | 912.5 | 677.5 | 2382 | 620 | 1080.5 | 992 | 2692.5 |
| 5:00 PM | 779.5 | 895 | 638.5 | 2313 | 585 | 1021.5 | 890.5 | 2497 |
| 6:00 PM | 648 | 773.5 | 529 | 1950.5 | 462.5 | 742 | 502 | 1706.5 |


|  | Northbound |  |  |  |  | Southbound |  |  |  |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $9 / 21 / 2012$ | 1 | 2 | 3 | Total | 4 | 5 | 6 | Total |  |
| $4: 00 ~ P M$ | 898 | 1130 | 1097 | $\mathbf{3 1 2 5}$ | 660 | 1177 | 1144 | $\mathbf{2 9 8 1}$ |  |
| $5: 00 ~ P M$ | 897 | 1084 | 1071 | $\mathbf{3 0 5 2}$ | 607 | 1117 | 1065 | $\mathbf{2 7 8 9}$ |  |
| $6: 00 ~ P M$ | 761 | 1030 | 939 | $\mathbf{2 7 3 0}$ | 542 | 963 | 781 | $\mathbf{2 2 8 6}$ |  |


| Wed | Northbound |  |  |  | Southbound |  |  |  |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $9 / 22 / 2010$ | 1 | 2 | 3 | Total | 4 | 5 | 6 | Total |
| $6: 00 \mathrm{AM}$ | 480 | 663 | 440 | $\mathbf{1 5 8 3}$ | 470 | 718 | 452 | $\mathbf{1 6 4 0}$ |
| $7: 00 \mathrm{AM}$ | 612 | 784 | 549 | 1945 | 506 | 833 | 616 | 1955 |
| $8: 00 \mathrm{AM}$ | 574 | 737 | 459 | $\mathbf{1 7 7 0}$ | 480 | 771 | 448 | $\mathbf{1 6 9 9}$ |
| 4:00 PM | 757 | 877 | 646 | $\mathbf{2 2 8 0}$ | 593 | 993 | 858 | $\mathbf{2 4 4 4}$ |
| 5:00 PM | 760 | 847 | 610 | $\mathbf{2 2 1 7}$ | 547 | 1,006 | 849 | $\mathbf{2 4 0 2}$ |
| $6: 00 \mathrm{PM}$ | 676 | 779 | 520 | $\mathbf{1 9 7 5}$ | 452 | 781 | 479 | $\mathbf{1 7 1 2}$ |


| Fri 9/24/2010 | Northbound |  |  |  | Southbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | Total | 4 | 5 | 6 | Total |
| 4:00 PM | 902 | 1,074 | 958 | 2934 | 680 | 1,195 | 1,345 | 3220 |
| 5:00 PM | 895 | 1,072 | 967 | 2934 | 593 | 1,113 | 1,001 | 2707 |
| 6:00 PM | 753 | 926 | 767 | 2446 | 536 | 960 | 838 | 2334 |


| Wed | Northbound |  |  |  |  | Southbound |  |  |  |
| ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $6 / 13 / 2012$ | 1 | 2 | 3 | Total | 4 | 5 | 6 | Total |  |
| $6: 00 \mathrm{AM}$ | 508 | 667 | 387 | $\mathbf{1 5 6 2}$ | 441 | 665 | 592 | $\mathbf{1 6 9 8}$ |  |
| $7: 00 \mathrm{AM}$ | 597 | 800 | 578 | 1975 | 495 | 721 | 599 | 1815 |  |
| $8: 00 \mathrm{AM}$ | 574 | 693 | 467 | $\mathbf{1 7 3 4}$ | 454 | 754 | 595 | $\mathbf{1 8 0 3}$ |  |
| 4:00 PM | 781 | 874 | 633 | $\mathbf{2 2 8 8}$ | 569 | 959 | 1,087 | $\mathbf{2 6 1 5}$ |  |
| 5:00 PM | 776 | 841 | 599 | $\mathbf{2 2 1 6}$ | 519 | 884 | 889 | $\mathbf{2 2 9 2}$ |  |
| $6: 00 \mathrm{PM}$ | 609 | 692 | 447 | $\mathbf{1 7 4 8}$ | 408 | 665 | 494 | $\mathbf{1 5 6 7}$ |  |


| Fri $6 / 15 / 20$ | Northbound |  |  |  | Southbound |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | Total | 4 | 5 | 6 | Total |
| 4:00 PM | 868 | 1,094 | 1,155 | 3117 | 583 | 1,054 | 1,348 | 2985 |
| 5:00 PM | 856 | 1,042 | 1,034 | 2932 | 504 | 1,038 | 1,191 | 2733 |
| 6:00 PM | 760 | 917 | 840 | 2517 | 106 | 953 | 1,342 | 2401 |

Appendix B
SIDRA Assumptions and Methods

## WSDOT Roundabout Standard Operations Analysis

It is recognized that WSDOT uses different methodologies than what is accepted in NCHRP 572 Roundabouts: An informational guide. The following parameters will be used in the roundabout analysis for the NW La Center Road/I-5 Interchange Improvement Project.

1) Change the Level of Service Method to HCM 2000
2) Change Capacity Model to SIDRA Standard
3) Change Roundabout LOS Method to 'Same as signalized intersections'
4) Change Entry Lane Width to 14 ft
5) Environment Factor:

- La Center does not have any roundabouts. Therefore, a 1.2 environment factor (which is consistent with HCM 2010) will be used. For future 2036 scenarios, the environmental factor will be adjusted to 1.1 per WSDOT methodology.

6) Basic Saturation Rate

- Although the existing interchange is in a predominately rural area, it is anticipated that the proposed Cowlitz Reservation Development will change the character of the area to more of an urban setting. As such, it is proposed that 1,900 be used as the base saturation rate.


## Appendix C

## Trip Distribution and Assignment






VITMELSON \& ASSOCIATES, INC.

Appendix D

## VISSIM Modeling Assumptions and Methods

The purpose of this appendix is to outline the processes and standards associated with developing any needed microsimulation (VISSIM) models for the NW La Center Road/I-5 Interchange improvement project. These microsimulation models will be developed using VISSIM to determine the impacts associated with the following issues:

- Development of the Cowlitz Reservation
- Modifications to NW La Center Road and the its interchange with I-5

The remainder of this appendix outlines the process Kittelson \& Associates, Inc. (KAI) will use to develop any applicable VISSIM models for this project.

## Modeling Study Area

As previously developed by regional stakeholders, the prepared VISSIM models will include the following intersections.

- NW 31 ${ }^{\text {st }}$ Avenue/NW 319 ${ }^{\text {th }}$ Street
- I-5 Southbound Ramp/NW La Center Road
- I-5 Northbound Ramp/NW La Center Road
- Paradise Road/NW La Center Road

In addition to the above intersections, I-5 ramps will be modeled, along with their interaction with I-5, for the ramps at the NW La Center Road Interchange, the SR 501 Interchange, the SR 503 interchange, and the $\mathrm{l}-5$ weigh station.

## Scenarios/Study Time Periods

Per the above methods and assumptions, VISSIM will only be used if a preferred alternative scenario does not meet the operational performances specified in the body of this report. For these scenarios, VISSIM will be used to review the alternative to determine feasibility of implementation. For each of these scenarios the following two time periods will be analyzed.

- Weekday PM Peak Hour
- Weekday Friday PM Peak Hour (Due to Casino use)

Prior to the future alternative being modeled in VISSIM, an existing conditions model will be developed and calibrated for the same time periods. The procedures used for this calibration and delivery of models are discussed further in this appendix.

For each VISSIM model the peak period data will be entered in the model in 15 minute intervals along with a thirty minute "warm-up" period. For this model, the term peak period refers to the point in time where forecasted traffic along either NW La Center Road or at the interchange's ramps results in a failing level of service (congestion) to the point where the model recovers (uncongested). It is believed that this will be no greater than two hours. Peak period information will be documented in the final report. The warm-up
period of the model cannot be used to develop meaningful measures of effectiveness; however, it is used to "prime" the model for peak hour conditions. Data for the warm-up periods will be developed based on the same traffic data used to develop the peak hour data with the warm-up period being $90 \%$ as intense as the peak hour. The peak hour factor for the peak hour will be the same as in existing condition.

## Model Development

Development of the VISSIM models will follow the Federal Highway Administration's (FHWA) 7 step process as outlined in the FHWA's Traffic Analysis Toolbox Volume III: Guidelines for Applying Traffic Microsimulation Modeling Software. These steps are summarized below.

- Identification of Study Purpose, Scope, and Approach
- Data Collection and Preparation
- Base Model Development
- Error Checking
- Calibration
- Alternatives Analysis
- Final Report and Technical Documentation

Based on the above process, the project team has prepared a list of assumptions which will be used for the individual steps. These are summarized below.

## Identification of Study Purpose, Scope, and Approach

The purpose and scope for this project were previously developed and approved by the regional stakeholders. No alternation to the scope and purpose is being proposed at this time.

## Data Collection and Preparation

Data sources required for model construction have been identified and are documented below.

## Geometric Data

Geometric data for the future condition will be developed based on the functional layout and design phase of this project and will be entered into VISSIM.

## Traffic Control Data

Control data for the future year conditions will be based on the functional analysis and design phase of this project. Control data includes, but is not limited to, the following:

- Signal Timing
- Speed Limits
- Turn Restrictions
- Yield Signs/Stop Signs


## Traffic Demand Data

Future year data will be developed through a trip generation and traffic forecasting exercise to be carried out and documented during this project. Existing year traffic count information will also be used to determine the base background heavy vehicle percentage. Vehicle characteristics, aside from heavy vehicle percentage, and performance data has not been collected and the default values contained within VISSIM will be used. Heavy vehicle models within the VISSIM model will be split between AASHTO design vehicles WB $40,50,65$ and 67 as determined by the available data.

## Origin-Destination Data

O-D data will not be developed for this project due to the model area's limited extents. As such all potential legal O-D pairs will be allowed and volume distribution will be handled through VISSIM's routing decisions. When routing decisions need to cover multiple intersections, relative percentages will be applied to the routes based on the turning movement distributions the route travel's through. Precautions will be taken to prevent I-5 off-ramp traffic from entering the network and immediately entering the adjacent I-5 on-ramp, unless this is observed in the field.

## Travel Time Data

Travel time data will not be collected for this project due to the limited extents of the model. Average vehicle speed will be compared to the posted speed limits and field visit data to ensure drivers are travelling at reasonable speeds.

## Base Model Development

Using the data outlined above, the required scenarios and existing conditions will be developed using VISSIM and industry best practices. Base model development represents a model which still needs to be validated and is only the first preliminary step in model development. The following key information regarding the base model is summarized below.

## Basic Settings

- VISSIM version 5.40 will be used
- A modeling resolution of 10 steps per second will be used
- Aggregated data will be developed based on 10 individual model runs and checked against FHWA procedures to ensure that the model is statistically valid. For this effort, a confidence interval of $95 \%$ will be assumed.
- If the model is shown to require more runs, the model will be further ran and continuously checked for stabilization.
- Default vehicle lengths and distributions will be used for passenger vehicles.
- Heavy vehicles will use AASHTO design vehicles WB 40, 50, 62, 65 and 67 as determined by the available data.
- Wiedemann 74 driver behaviors will be used for NW La Center Road modeling
- Wiedemann 99 driver behaviors will be used for I-5 mainline and ramp modeling
- Any model specific settings will be documented in the final technical documentation
- Desired speed curves will be developed based on available l-5 mainline data


## Routing Decisions

Routing decisions will be coded in a manner that the beginning of the decision (red bar) is as far upstream of the first decision point as possible. The will enable a vehicle to make a decision at the first possible opportunity. In instances of short distances between intersections, routing decisions may need to combine multiple routes in order to minimize unrealistic lane changes. At this time it has not been determined if passenger vehicle and heavy vehicle traffic share similar routes. If it is determined that they do not, a specific set of routing decisions will be included to accommodate heavy vehicle routing through the model.

## Speed Decisions

Speed decisions will be placed at each entrance to the model. For instances where a speed change will occur, the decision point will be placed so the vehicle will change speeds as soon as they are on the link with the new anticipated speed. For off and on-ramps, speed decisions will be placed accordingly per the geometric and control data from the alternative development.

## Reduced Speed Areas

Reduced speed areas will be placed on any link or connector whose corresponding roadway geometry would cause vehicles to temporarily slow down to negotiate the area. The most common area for reduced speed zones are for left and right turn movements. As this data will not be collected, the following reduced speed area settings will be used for passenger vehicles.

- Right Turns - $10 \mathrm{mph}(7 \mathrm{mph}-13 \mathrm{mph})$
- Left Turns - 15 mph ( $12 \mathrm{mph}-18 \mathrm{mph}$ )

Heavy vehicles will use the following speeds.

- Right Turns - $8 \mathrm{mph}(5 \mathrm{mph}-10 \mathrm{mph})$
- Left Turns - 12 mph ( $10 \mathrm{mph}-15 \mathrm{mph}$ )


## Conflicts Areas/Priority Rules

Conflicts in VISSIM can be modeled using conflict areas and/or priority rules. Typically it is desired to use conflict areas; however, certain situations may require the use of priority rules. For this model, the project team will prioritize the use of conflict areas over priority rules.

## Error Checking

KAI's error checking process is summarized below. It is similar to the process outlined in FHWA Traffic Analysis Toolbox Volume III: Guidelines for Applying Traffic Microsimulation Modeling Software.

- Review Input
- Roadway network
- Traffic volumes and routing
- Traffic control
- Review Animation
- Driver behavior
- Location, extent and frequency of congestion
- Miscellaneous localized problems
- Review Errors
- Traffic unable to enter network
- Traffic removed from simulation

Error checking for this project will be conducted by a senior engineer with the project modeler performing a back check on the identified issues. Error checking will be completed prior to model calibration.

## Existing Condition Model Calibration

Calibration of the VISSIM model will occur for the "existing condition" models only. Any modified parameters will be carried forward to future conditions models. The existing conditions model is deemed calibrated when the volume, speed, and other operational observations are satisfactorily replicated to those in the field.

The calibration process we will follow is illustrated in Figure 1 below. This figure is from FHWA Traffic Analysis Toolbox Volume IV which discusses CORSIM modeling. However, the general principals of calibration do not change between VISSIM and other microsimulation tools.

Figure 1 - Calibration Approach Flowchart


Calibration for the existing conditions model will be based on reaching target thresholds of model reported results versus field measured data. Each of the thresholds for these areas is detailed below. For this effort, traffic volume will be the primary calibration metrics, while queue lengths and visual accuracy will be secondary efforts. Once the below outlined targets are met, the model will be considered calibrated and existing condition measures of effectiveness will be collected.

## Traffic Volume Calibration (Primary Calibration Indicator)

Traffic volume calibration involves measuring averaged modeled volumes against field measured data. To do this comparison the project team will use the GEH statistic formula. The GEH formula was empirically developed to review traffic models involving a wide variety of traffic volume intensities. Its primary benefit is that it accounts for the desire to have varying levels of agreement depending on how large or small traffic volumes are.

An example of this issue is that a turning movement of 50 vehicles per hour may experience a typical stochastic model fluctuation of between 10-20 vehicles or 20-40 percent and still be acceptable. While a mainline volume of 5000 vehicles per hour, should experience a fluctuation of no more then $5-10$ percent. In using the GEH formula, the same set of rules can be used for any volume as the desired deviation from the measured volume is built into the formula. In this manner, the formula is similar to a Chi-Squared test.

The GEH formula is:

$$
G E H=\sqrt{\frac{(M-C)^{2}}{(0.5(C+M))}}
$$

For this modeling effort, the following guidance will be used regarding the GEH score of calibrated movements.
i. GEH Less than 2 - Calibrated Value
ii. GEH Between 2 and 5 - Acceptable Value
iii. GEH Between 5 and 10 - Review model, provide comment if volume cannot be further calibrated
iv. GEH Greater than 10 - Revise model, provide explanation in report if volume cannot be further calibrated

Target goals for this model develop are:

- $85 \%$ of the modeled movements with a GEH score below a 5 , and
- The model aggregated with a GEH score below a 4.

Instances where it is not possible to meet these goals will be documented in the final technical documentation.

## I-5 Speed Data (Primary Calibration Indicator)

I-5 speed data will be used as the second primary calibration metric. Two values will be reviewed based on available data; the average mainline speed, by direction, across all through lanes and the $85^{\text {th }}$ percentile speed across all through lanes. The proposed calibration targets are documented for each below.

- Average speed across all lanes within $5 \%$ (approximately $+/-3.5 \mathrm{mph}$ )
- 85th percentile speed across all lanes within $5 \%$ (approximately $+/-4 \mathrm{mph}$ )

Instances where it is not possible to meet these goals will be documented in the final technical documentation.

## Queuing Calibration (Secondary Calibration Indicator)

Queuing will be collected visually during the project team's field visits. As such, the model will only be calibrated in a general sense to queuing. The visual information gathered will be documented in the final technical memorandum and the model will be visually inspected to ensure that queues are neither significantly shorter nor longer than what was observed in the field.

## Visual Calibration (Secondary Calibration Indicator)

VISSIM is capable of producing a visual output of the model which the analyst can then compare to their own experience in the field and others' field notes. This visual observation will be completed to ensure that the model overall is operating as expected and that the representation of driver behavior is reasonable. Any unique situations which occur in the model will be documented in the final technical documentation.

## Future Condition Analysis

Once a calibrated existing conditions model is created, the future conditions documented above will be analyzed using the base assumptions developed during calibration. Future year traffic volumes and geometric modifications have been developed outside of the VISSIM effort and will be incorporated in the future VISSIM model.

Similar to calibration a base level of volume validation will be completed to ensure that modeled volumes are in line with expected volumes. Once volume validation is complete, the future year model will undergo error checking and will be considered complete. Following these steps, the future year alternatives' measures of effectiveness will be produced.

Measures of effectiveness will be based on VISSIM's default data collection settings. Current settings are not HCM compliant in that the HCM and VISSIM measure delay slightly differently. However, per the ODOT VISSIM protocols (endorsed by WSDOT); it was determined that the difference in delay calculations is minimal and the appropriate course action is to refer to the delay values generated by VISSIM by the term delay instead of HCM delay. HCM level of service will continue to be applied using the VISSIM delay data.

## VISSIM Milestones

Due to the expedient nature of this effort the following project milestones are proposed for model review by project stakeholders.

- Calibrated Base Model and Calibration and Results Report
- Future Alternative Models with Corresponding Documentation
- Final Report with all Alternative Models

Further milestones included as part of the larger project will cover topics such as forecast volumes, alternative geometry, traffic control, project background and project justification. Results from these efforts will be forwarded onto technical reviewers based on their availability at the above milestones.

## Final Report and Technical Documentation

Technical documentation for a VISSIM modeling effort involves two parts. The first is a final technical report which will include the following items:

- Project Background
- Base Assumptions
- Areas of concern or special interest
- Future Year Conditions
- Supporting Appendices (traffic counts, model outputs, signal data.., etc)

The second deliverable is the VISSIM model themselves, including the existing condition model as well as any alternatives. The following VISSIM files will be provided to the reviewing agency(s) and allow for independent verification of the models.

- VISSIM (.inp) files
- Signal Timing (.rbc) Files
- Background Imagery (various formats) and background scaling files (.bgr)
- Random Seed Numbers


# Appendix B Transportation Impact Analysis (TIA) for the Cowlitz Reservation Development 

Due to the size of the Transportation Impact Analysis, it is provided as a separate file.

## Appendix C Engineering Assessment of NW La Center Road/I-5 Interchange Structure

# NW La Center Road/I-5 Interchange Existing Bridge Review 

Prepared For: Cowlitz Reservation Development Project Team

Prepared By: Don Wagner, CH2M HILL
Date: July 23, 2014
The existing NW La Center Road Bridge over I-5 is a four span structure constructed in 1969 with an overall length of 313 feet with span lengths of 105.5 feet over the northbound and southbound Interstate 5 Freeway (I-5) and 51 feet long end spans. The overall bridge width is 34 feet and the minimum vertical clearance is 16.5 feet. The bridge provides a 26 foot wide roadway with one 11 foot wide travel lane and 2 foot wide shoulder in each direction and 3 foot wide sidewalks on each side. The bridge superstructure includes prestressed concrete girders with a cast in place concrete deck. The bridge substructure includes cast in place concrete abutments and piers supported by timber piling.

Based upon the most recent inspection, the bridge is generally in fair to good condition with some hairline map cracking of the deck, columns and cap beams. Several girders located over I5 have high vehicle impact damage with spalls, delamination and exposed prestress strands and repairs. The bridge inventory load rating is 33 tons and operating load rating is 56 tons. The bridge is not posted.

The existing bridge will require widening to meet current roadway travel lane, shoulder, and sidewalk width design standards. In addition, future traffic demands result in the need for at least two travel lanes in each direction. Due to right of way constraints on the northeast side of the bridge, widening on the south side of the bridge is preferred. The roadway profile on I-5 raises to the south. Widening on the south side of the existing bridge and maintaining the existing cross slope will result in a reduction in the minimum vertical clearance to less than 16.5 feet without either reducing the structure depth, lowering the I-5 profile, raising the overcrossing roadway profile or some combination of these. In addition, traffic will need to be maintained during construction of the widening resulting in the need for staged construction of the widening.

The existing bridge does not meet current seismic design standards. The existing bridge structural seismic deficiencies include columns that do not have sufficient transverse reinforcing steel to provide confinement in the plastic hinge regions at the top and bottom, cap beams that do not have sufficient top and bottom reinforcing steel to accommodate the column plastic moment demands, footings that do not have top reinforcing steel, and timber piles that are embedded 6 inches and do not include any tension ties. In addition, the bridge
spans are all simple spans with no continuity at the intermediate piers and no longitudinal restrainers.

Chapter 4 of the WSDOT Bridge Design Manual requires for widening of an existing bridge that element seismic capacity/demand ratios be compared before and after widening. If the seismic capacity/demand ratio is not decreased, the widening can be designed and constructed without retrofitting existing seismically deficient bridge elements. If the widened bridge capacity/demand ratios are decreased, the seismically deficient existing elements must be retrofitted as part of the widening project.

Considering the existing bridge structural system and seismic deficiencies, it will be difficult to widen the existing bridge without increasing the existing seismic capacity/demand ratios. Thus, the existing structure will need to be retrofitted for the widening. Considering the age and condition of the existing bridge, replacement of the bridge deck and the outer girders with high load impact damage should be included with the widening and retrofit of the existing bridge. In addition, considering traffic must be maintained and construction must be staged, the cost of the widening, retrofitting, and deck and girder replacement will likely be about the same or more than a new wider bridge. The new bridge can be constructed south of the existing bridge while traffic is maintained on the existing bridge resulting in minimal traffic impacts except when the roadway tie-ins are constructed at each end of the bridge. As such, replacement of the existing bridge is recommended in lieu of widening and retrofitting the existing bridge.

## Appendix D March 14th, 2013 Alternatives Workshop Meeting Minutes

Kittelson \& Associates, inc.
TRANSTPORTATIONENGINEERING/PLANNING 610 SW Alder Street, Suite 700, Portland, OR 97205 P 503.228.5230 F 503.273.8169

## I-5/NW La Center Road Interchange Improvement -

## Alternatives Workshop

March 14, 2013 at 10:00 AM

| Date: | March 21, 2013 |
| :--- | :--- |
| To: | Wroject \#: 12393.0 |
|  | Project Team |
| From: | Kittelson and Associates, Inc. (KAI) |
| Project: | I-5/NW La Center Road Interchange Improvement |
| Subject: | Summary Meeting Notes |

## Summary of Action Items:

- Project Team to update Property and Right-of-Way (ROW) Map to adjust ROW lines on west side of interchange to accurately reflect County ROW.
- Project Team to develop additional interchange concept sketches to include designs developed as part of the La Center Sub Area Plan.
- Project Team to consider comments received during meeting related to interchange and corridor concepts that have been developed thus far.
- Project Team to distribute a matrix comparing the interchange concepts in the next couple of weeks.
- Project Team to evaluation NB Terminal dual left-turn utilization based on Casino entrance and circulation plan and conduct an event sensitivity analysis for evening events.
- WSDOT and City staff to provide any additional comments on the Operations Memorandum, Design Criteria Memorandums, and interchange and corridor concepts developed by the Project Team by Monday, March $25^{\text {th }}, 2013$.
- WSDOT and City staff to provide any additional interchange or corridor concepts for the Project Team's consideration by Monday, March $25^{\text {th }}, 2013$.

1. Introductions

- The focus of this meeting is on the interchange form (l-5/NW La Center Road), as well as the alignments of NW $319^{\text {th }}$ Street and NW $31^{\text {st }}$ Avenue on the west side of the interchange. The scheduled April $2^{\text {nd }}$ meeting will address the alignment of NW Paradise Park Road.
- The purpose of this meeting is to present the concepts that have been developed thus far, receive feedback, and gather input on any additional concepts the project team should consider.


## 2. Background

## a. Summary of available property and right-of-way for improvements

- The Property and Right-of Way Map (Figure A) displays existing ROW constraints, property ownership, and wetlands. The majority of challenges and constraints are on the east side of the interchange (narrow ROW, property negotiation discussions).
- Action Item: It was noted that NW 31 ${ }^{\text {st }}$ Avenue is in the County ROW (not the City). KAI will update the map to accurately reflect ROW on the west side of the interchange.


## b. Overview of future interchange operations

- Merge/diverge operations show that the northbound (NB) off-ramp and southbound (SB) on-ramp do not meet standards in 2016 or 2036 with the Cowlitz Reservation development. Therefore, double-lane ramps are necessary.
- Question: Did you explore just extending the ramps? Yes, we looked at a variety of options.
- With signals at the ramp terminal intersections, a 4-lane bridge structure will be required in 2016 and a 6-lane structure in 2036 to support future traffic volumes and the proposed Cowlitz Reservation development.
- Question: How do the intersections look with the proposed 2016 configuration and 2036 volumes? Unacceptable - intersections are operating over-capacity.
- Comment: It looks like the AM peak is very concentrated (one dominant movement), while the PM peak is more dispersed (several movements). Also, the AM peak is more concentrated because everyone leaves for work near the same time. True. However, the volume of vehicles making opposing movements (in conflict with the left-turn onto I-5 southbound) in the AM is low.
- Question: The NB off-ramp has 960 left turns. How does this intersection operate at a LOS D? The operations displayed in the memorandum are with the proposed geometry, not the existing geometry.
- Question: Is there a second access to the site? Yes, an additional access is planned farther west. We split the volumes 50/50 at the two accesses for this analysis. We also looked at a scenario where $85 \%$ of vehicles enter at the first access and exit at the second access based on the one-way operations currently anticipate on site. We will consider the distribution of vehicles in each access when refining the site plan layout. We will also look at weaving maneuvers along the NW 319 ${ }^{\text {th }}$ Street/NW La Canter Road corridor.
- Action Item: KAI will evaluate the NB Terminal dual left-turn utilization based on Casino entrance and circulation plan and conduct an event sensitivity analysis for evening events
- With roundabouts at the ramp terminals, there is more flexibility for staging the design, and a narrower bridge structure (4-lane) is required. The specifics of the signal and roundabout designs are further discussed later in the meeting.
- Comment: WSDOT will consider both roundabouts and signals. WSDOT does not like roundabouts on high-speed facilities (posted speed greater than 50 mph), but at ramp terminals they are typically acceptable.
- Question: Have you considered teardrop roundabouts instead of circular roundabouts? Yes. Circular roundabouts provide the opportunity for U-turns if accesses need to be limited in the vicinity of the ramp terminals, but we will also consider teardrop roundabouts.
- Action item: The project team requests any additional comments or questions on the Operations Memorandum as soon as possible so we can incorporate them before the process goes any farther.


## c. Overview of design criteria

- The goal is to maintain the existing gore points on the I-5 SB off-ramp and I-5 NB onramp; design new gore points on I-5 NB off-ramp and I-5 SB on-ramp (future operations require double-lane ramps).
- Question: Have you checked geometry of existing ramps? Not yet, but intend to. At a high-level assessment, we are concerned about the existing acceleration and deceleration distances, respectively.
- Question: Are there environmental impacts if the ramps are altered? Potentially not (based on how far the gore points are moved), but we haven't looked at this specifically.
- The design speed for the cross road (i.e., NW La Center Road and NW $319^{\text {th }}$ Street) is currently anticipated for 55 mph .
- Comment: It appears that a 35 -mph design speed would be more appropriate in the vicinity of the interchange. For a signalized corridor, the design speed dictates the horizontal alignment and the associate superelevation, while roundabouts provide more flexibility for the approaching geometry due to managing speeds. Project team will work with City and Clark County staff to establish the desired design speed for the NW La Center Road/NW 319 ${ }^{\text {th }}$ Street corridor.
- Action items:
- The project team requests any additional comments or questions on the design criteria assumptions as soon as possible.
- The project team requests an appropriate design speed for the NW La Center Road/NW 319th Street corridor.


## d. Existing structure assessment

- The existing structure has sufficient capacity to carry existing loads.
- The existing structure is substandard in terms of lane-widths, shoulders, and lack of sidewalk.
- The vertical clearance appears to be 16.5 feet. We do not have exact deck clearance information, as the original assumption was that we will not retain the existing structure. If there is an option to keep the structure, we will survey the bridge main deck and ensure vertical clearances.
- The grades approaching the bridge over the highway is approximately 2.5-2.8\%. The profile over the bridge is within a vertical curve.
- Our preliminary recommendation is to potentially reuse the existing substructure and replace the superstructure.
- There are seismic issues, so that any widening of the bridge structure will require the substructure to be upgraded. Therefore, it may be advisable to replace the full-bridge in terms of cost-effectiveness.
- Question: Is there room to add a lane in each direction along I-5 under the existing structure? This is likely possible, but we can't say with certainty yet. The median is approximately 64 feet.
e. Site constraints (environmental, topography)
- There are no wetlands in the northeast (NE) corner (Fudge property) or impacts to the stream.
- Question: You have taken in to account that the Cowlitz Reservation development may use the stream, correct (i.e. for clean wastewater)? Yes, we have had initial discussions about this but will continue to look at this possibility.
- In the southeast (SE) corner (Carlson property), there is compacted top soil, wetland areas (category 4), and a previous waste-site. This restricts how far NW La Center Road can be moved south and to the east. With the realignment of NW Paradise Park Road, it may be difficult to maintain the S-curve and have the road tie in at a 90degree intersection angle.
- On the west side of the interchange, the wetlands represented on the maps were surveyed as part of the environmental impact statement (EIS).


## 3. Interchange Concepts

a. Initial design concepts

- Part of the interchange justification report (IJR) process involves doing a thorough look at other potential alternatives.
- The operations analysis done thus far on the ramps and at the ramp terminals assumes the existing diamond interchange form, but we are also considering other interchange forms.
- We have developed 8 interchange concepts and created single-line sketches to get an idea of what the interchange form will look like. Once a form is selected, we will further develop the concept and identify impacts.
- Question: The analysis is based on where identified deficiencies are, correct? Yes, we are reacting to where we have identified deficiencies due to growth in the area.
- Question: Any there issues with weigh-station south of interchange? There are no merge/diverge issues there, but there are potentially mainline capacity issues.
- Question (on Concept 5): The NB off-ramp does not have to be aligned with the cloverleaf ramp, correct? Yes, the concepts show one option, typically the worst-case scenario.
- The parclo concepts will push the ramp gore points farther from the interchange and have significant impacts on properties at each quadrant of the interchange.
- The project team would like to get any additional thoughts or ideas to add to mix of options. We would like to ensure that we have a thorough and robust assessment to include in the IJR.


## b. Evaluation criteria

- The project team presented the preliminary evaluation criteria to compare the interchange concepts.
- Comment: We should also consider the potential for wrong-way movements (i.e. on the loop ramps).
- Comment: The evaluation assessment in the IJR should be in as concise a form as possible (i.e., a matrix). We don't need a long write-up or analysis.
c. Work session to sketch other potential concepts to consider
- No additional concepts were suggested during the meeting.
- Comment: The parclo designs where the ramps and frontage roads are next to each other may create complications and be hard to deal with from a driver expectation point of view. The parclo concepts also have significant right-of-way impacts. They can be problematic with wrong-way movements and driver confusion.
- Comment: The project team has done a thorough job of capturing the concepts WSDOT would typically look at.
- Question: Have you looked at sub-area concepts? Yes. We will look at these more thoroughly and include a sketch of any applicable concepts in the evaluation.
- Action Item: the project team will add sketches of any applicable concepts from the La Center sub-area concept plan.
- Action item: the project team requests any additional ideas or concepts in the next week.


## 4. Corridor Concepts

## a. Horizontal and vertical alignments

i. La Center Road

- Constraints for the alignment of NW La Center Road include:
- The existing bridge structure and how we construct/expand the bridge while maintaining traffic;
- Staying within the existing ROW on the east side of interchange; and
- Wetland constraints.
- There are less ROW constraints on the west side of the interchange, so most challenges for the alignment are on the east side.
- The goal is to leave 12 -foot lanes on the bridge structure and maintain 2 feet of clearance for workers during construction. If we maintain and expand the existing bridge structure, we will likely expand to one side.
- The initial alignment layouts are based on the design criteria and assumptions.
- To accommodate potential vertical alignments, the existing structure would either have to be raised or significantly modified (which may not be cost effective).
- The roundabout concept has the option of building a second separate bridge structure, with each structure providing for one direction of traffic. The structure could be built to accommodate long-term demand with striping used to size it for near-term demand.
- The ramp terminals will have to be raised 3-5 feet.
- Question: There is limited left-turn storage on the bridge between the ramp terminals. Could you pull the terminals closer together to create tight diamond? We have the design working with signal timing (in terms of providing sufficient left turn storage), but we can look at that convention.
- Action Item: Project team to consider design with more closely spaced ramp terminals, with left-turn vehicles stored outside the interchange.


## ii. NW 31 ${ }^{\text {st }}$ Avenue, and NW $319^{\text {th }}$ Street

- The horizontal alignment of NW $319^{\text {th }}$ Street will be developed to tie-in with NW La Center Road across the bridge and avoid wetland impacts. The alignment will be further refined based on the bridge structure and placement of ramp terminal intersections.
- The alignment of NW $319^{\text {th }}$ Street west of the interchange cannot be fully developed without discussions with the County.
- Comment: We can ask the County questions now, but they cannot provide engineering guidance. Once we define the layouts further we can sit down with the County to work out an appropriate alignment of NW 319 ${ }^{\text {th }}$ Street to match the existing facilities on the west of the project.
- Comment: WSDOT noted that another project was able to pay for the wetland impacts using Habitat Bank, LLC. This may be a possibility for this project as well if wetland impacts are unavoidable. Credits may be available in the next couple months.
- Question: Will the County road be on easement through tribal land? No, the County will own the land.
- Once the layouts are further defined, we will thoroughly look at on-site circulation, weaving, and how to move vehicles in out and of the site.
b. Ramp terminals and frontage road intersections


## i. Signals or roundabouts

- The project team presented a design with signals at the ramp terminal and frontage road intersections to accommodate projected 2016 traffic volumes (including the proposed Cowlitz Reservation development).
- Question: What assumptions were made about left-turn utilization from the northbound off-ramp to NW La Center Road? We will have to check this and do a sensitivity analysis.
- The project team presented a design with signals at the intersections that accommodates projected 2036 traffic volumes (including the proposed Cowlitz Reservation development).
- The 2036 design requires widening the bridge structure and expanding the intersections. We typically widen to the outside on both sides, although this creates complications with the bridge structure and alignment.
- The project team presented design options to accommodate the projected 2016 and 2036 traffic volumes with roundabouts instead of signals.
- A narrow (4-lane) bridge structure is required with roundabouts.
- From a constructability and design perspective, roundabouts provide more flexibility.
- The roundabout design can be expanded from 2016 to 2036 by widening to the inside (using the splitter islands). Additional turn lanes are also required on the ramps to accommodate 2036 traffic volumes.
c. Work session to sketch other potential concepts to consider
- No additional concepts were suggested during the meeting.
- Action Item: The project team requests any comments on the signal or roundabout layouts or any additional concepts in the next week.


## 5. Next Steps

- The project team will produce meeting minutes and distribute them with a copy of the PowerPoint in the next week.
- Action Item: The project team requests any additional interchange or corridor concepts in the next week.
- Action Item: The project team will distribute a matrix comparing the interchange concepts in the next couple of weeks.
- A second workshop is scheduled for April $2^{\text {nd }}$ (10 am - noon)
- Additional property negotiation discussions are necessary before this meeting can be held.
- The meeting will discuss the alignment of NW Paradise Park Road.
- Question: Will the frontage roads be moved farther from interchange? Yes, the question is how far. We will also maintain full access to the gas station in the NE quadrant of the interchange.
- The goal is to submit the TIA and IJR by May $2^{\text {nd }}$
- The project team would like to receive and incorporate all comments before the submittal.

Other Items:

- Property Update
- Carlson and Fudge property owners are cooperative
- The preferred alternative is to use a westernly NW Paradise Park Road alignment, which would help provide full access to the gas station. However, the Landon property is not yet available.
- Question: What is the timeline for conducting the bridge assessment? The assessment will only be done if we intend to maintain the existing structure, which is likely only plausible with the roundabout design.
- Comment: The City of La Center noted that they would like to see the potential frontage road alignments and impacts on City. They also noted that a diverging diamond interchange (DDI) design is likely to be unpopular, although left-turn movements on to l-5 have been a concern. As the City does not currently have someone to main traffic signals (and likely won't for a while), roundabouts work well.
- Comment: WSDOT noted that there would have to be a reason to use a DDI above other alternatives (i.e. roundabouts) and it would be less desirable. FHWA will have the final say on the interchange form.
- Question: Have you looked at operations for the SPUI? We have not done a detailed analysis, but will look at farther. The bridge structure to accommodate a SPUI would be large and expensive, and the form would also create pedestrian and bike concerns due to the size of the intersection.
- Question Can the design handle the flow in/out of the site during an event when traffic volumes in and out of the site are not balanced? The project team will look into this and consider operations during special events (e.g., flagging).
- Comment: From a guest perspective, roundabouts are likely more comfortable and attractive. The DDI form would have some negatives, and may lessen property values (as there may be concerns associated with the design).
- Steve Horenstein provided an updated on the federal case, and noted that it is moving along. Recent news articles related to the case have not represented the situation accurately. Steve noted that we have a strategy for addressing the situation, and will likely lose approximately 4 months in the project timeline.


## Appendix E July 14th, 2014 Alternatives Workshop Meeting Minutes

## ALTERNATIVES WORKSHOP \#2: JULY 14, 2014 at 1:30 PM

July 17, 2014
Project \#: 12393.0
To: WSDOT Staff, City of La Center Staff, and Project Team
From: Marc Butorac, P.E. PTOE and Matt Hughart, AICP
Project: Cowlitz Reservation Development
Subject: Workshop Meeting Summary

This memorandum provides a summary of the action items developed as part of the July 14, 2014 Alternatives Workshop \#2 held at WSDOT as well as high level meeting notes and a copy of the PowerPoint presentation. Please review these materials and let us know if we have inadvertently missed any of the requested action items or if you would like to see any additional points of clarification be provided in this meeting summary by Tuesday, July 22nd. We will be providing a written summary addressing the action items below by Friday, July $25^{\text {th }}$.

## Summary of Action Items:

A. Begin formal Coordination with Washington State Parks and Recreation: Project team to reach out to officials at Paradise Point State Park regarding interchange and frontage road realignments.
B. $\mathbf{3 2 4}{ }^{\text {th }}$ Avenue Connection to Paradise Park Road: Project team to look at alternatives for enhancing this connection.
C. 2037 Design Cost Estimates: Project team to prepare the cost estimates for the 2037 full buildout improvements under both the signal and roundabout options
D. $\mathbf{2 0 3 7}$ No-Build Operation Analysis: Project team to prepare operations without secondary improvements.
E. Refined Roundabout Design Plan and discuss Bicycle \& Pedestrian Accommodations: Project team to prepare narrative and additional plans that illustrate pedestrian and bicycle accommodations for the roundabout designs.
F. Preliminary List of Design Deviations: Project team to prepare a preliminary list of design deviations and provide a brief narrative on the preliminary justifications to WSDOT for review prior to initial IJR submittal.
G. Weekday PM Peak Analysis: Project team to prepare a brief discussion and comparison of the weekday p.m. peak hour to the Friday p.m. peak hour in the IJR and TIA.
H. $31^{\text {st }}$ Documentation for City Ownership: Project team to prepare documentation of $31^{\text {st }}$ ROW
I. Work Session Response Packet: Project team to prepare a response packet addressing these action items and submit to WSDOT and City of La Center.

## Meeting Notes

1.) Introductions

- See attached attendance list and copy of the presentation.
- Clark County staff were invited, but chose not to attend this Workshop.
- Comment: IJR Policy Point requires coordination with all impacted agencies. Clark County coordination issue will need to be addressed in IJR.
2.) Project Update
- Project Schedule
- DRAFT IJR and TIA on-going - targeting September submittal
- Re-Evaluation Report on-going - targeting October submittal
- SEPA/NEPA review - targeting January 2015 completion
- Final Interchange Design (pending review and approval) - Jan 2015 to Jan 2016
- Construction - ~Spring 2016 to ~Fall 2017
- Property Acquisition
- Property acquisition and options are being acquired to accommodate frontage road realignments
3.) Interchange Form Alternatives Analysis
- Diamond form based on March 2013 Work Shop.
- Developing a new overpass alignment south of existing structure for construction phasing and maintenance of traffic.
- New overpass profile approximately 5 feet higher than existing.
- Ramp Modifications
- NB Dual Lane Exit (similar to Ridgefield)
- SB Dual Lane Entrance at Terminal with merge prior to Mainline merge
- Comment: Need to produce a list of design deviations. WSDOT staff would like to review them prior to being included in IJR.
- Dual NB off-ramp will have impacts to existing Paradise Park Road alignment and likely require some mitigation.
- Comment: Analysis needs to show 2017 and 2037 no-build operations.
4.) Frontage Road Alternatives Analysis
- Private acquisition of property for roadway realignment - no eminent domain
- 8 frontage road alignment concepts were developed
- Preferred frontage road alignment - Option E2
- Comment: More analysis and discussion is needed regarding $324^{\text {th }}$ connection to Paradise Park Road.
- Comment: Project team should begin discussions with Paradise Park State Park officials regarding proposed Paradise Park Road realignment.
5.) Ramp Terminal Control Analysis
- Signalized and Roundabout scenarios being analyzed
- 2017 and 2037 layouts were presented
- Comment: Are alternatives being driven solely by projected volumes? No, staging, maintaining adjacent parcel sizes, and construction issues are also being considered.
- 2017 Signalization - Preliminary Cost of $\$ 24.2 \mathrm{M}( \pm 20 \%)$
- 2017 Roundabout - Preliminary Cost of $\$ 25.6 \mathrm{M}( \pm 20 \%)$
- Comment: Cost estimates should be developed for 2037 build scenarios to determine how long-term costs compare. Long-term signalization may be higher than long-term roundabout.
- Preliminary Preferred Ramp Terminal Control - Roundabouts
- Better Near- and Long-term Operations
- Overpass width set in the near-term
- Safety benefits
- Aesthetics / Gateway Treatment
- Comment: Need to assess pedestrian and bicycle accommodation for roundabout designs
- Comment: Need to assess La Center Road/Realigned Paradise Park intersection as a signal with roundabouts at the ramp terminals.
6.) $319^{\text {th }}$ Alignment Alternatives
- Existing $319^{\text {th }}$ is an easement
- Comment: Send WSDOT documentation of La Center boundary along $31^{\text {st }}$.
- Preferred new southerly alignment to accommodate more efficient east-west through travel.
- New alignment avoids wetlands
7.) Next Steps
- WSDOT staff to review memos submitted as part of the Workshop and provide project team comments by end of July.
- Project team will prepare a response memo addressing Workshop comments.
- Submittal of Draft IJR and TIA - September $1^{\text {st }}$
- Tentative date for next meeting is August $6^{\text {th }}$ at 1:30 p.m.


# Appendix F Technical Memorandum: Interchange Evaluation Intersection Traffic Control 

Kittelson \& Associates, inc.<br>TRANSPORTATIONENGINEERING/PLANNING 610 SW Alder Street, Suite 700, Portland, OR 97205 P 503.228.5230 F 503.273.8169

## TECHNICAL MEMORANDUM <br> NW La Center Road/I-5 Interchange Improvement Project Signalized Interchange Evaluation

| Date: | February $23^{\text {rd }}, 2015$ | Project \#: 12393 |
| :--- | :--- | :--- |
| To: |  |  |
|  | Peter Schultz and Paul Tresnan |  |
|  | Mohegan Gaming Advisors, LLC |  |
| From: | Jeff Whitman, PE; Kelly Laustsen |  |
| Copy: | Project Team (i.e., CH2MHILL, Olson Engineering, and BergerABAM) |  |

This memorandum presents the intersection analysis findings and design alternatives for intersection control at the NW La Center Road/Interstate 5 (I-5) interchange. Specifically, the memorandum assesses the lane configurations and storage lengths needed to support projected future traffic conditions with traffic signals at the interchange ramp terminals and frontage road intersections. The results of this assessment were used to inform the interchange improvement recommendations included in the NW La Center Road/I-5 Interchange Justification Report (IJR).

## METHODOLOGY AND ASSUMPTIONS

The operational analysis results presented in this memorandum assess intersection geometric needs for signalized intersection control at the following intersections:

- NW 319 ${ }^{\text {th }}$ Street/NW $31^{\text {st }}$ Avenue
- NW La Center Road/I-5 Southbound Ramp Terminal
- NW La Center Road/I-5 Northbound Ramp Terminal
- NW La Center Road/NW Paradise Park Road

These intersections were analyzed for two horizon years during two peak hour conditions ${ }^{1}$ :

- Opening Year 2017 Weekday AM and Weekend Peak ${ }^{2}$ Hours
- Future Year 2037 Weekday AM and Weekend Peak ${ }^{2}$ Hours

[^3]
## Analysis Assumptions

The following key assumptions were made in preparing the analysis:

- The need to mitigate the four intersections is identified in the NW La Center Road/l-5 Interchange Improvement Project Interchange Justification Report (IJR). The IJR highlights the intersection and interchange improvement needs for accommodating trips traveling to the Cowlitz Reservation Development during the critical weekend peak hour and accommodating eastbound trips from the City of La Center to l-5 during the AM peak hour.
- The IJR provides the methodology for developing 2017 and 2037 traffic volumes.
- All four analysis scenarios include site-generated traffic from full build-out of the proposed Cowlitz Reservation Development. The site-generated traffic was added to 2017 and 2037 background traffic volumes to arrive at the total traffic volumes.
- With the project, NW $31^{\text {st }}$ Avenue will be realigned and the intersection with NW $319^{\text {th }}$ Street moved approximately 600 feet (centerline-to-centerline) west of the southbound ramp terminal.
- With the project, NW $319^{\text {th }}$ Street will be relocated approximately 350 feet south of its current alignment.
- With the project, Paradise Park Road will be realigned and the intersection with NW La Center Road moved approximately 450 feet (centerline-to-centerline) east of the northbound ramp terminal.
- This analysis assumes the existing gas station driveway near the Paradise Park Road/La Center Road intersection will operate as a right-in/right-out driveway. Therefore, all left turning traffic into and out of the gas station would use the Paradise Park Road /La Center Road intersection.
- The IJR identifies traffic volumes at this intersection do not meet signal warrants under 2017 traffic conditions, but do meet signal warrants under 2037 traffic conditions. This evaluation assumes a stop controlled (northbound and southbound approaches) intersection in 2017, and a signalized intersection in 2037.
- A detailed site plan for the Cowlitz Reservation Development was not available at the time this evaluation was prepared; therefore, the analysis presented in this technical memorandum is predicated on the assumption that the two site accesses on NW 319 ${ }^{\text {th }}$ Street results in a roughly even distribution of site traffic with $50 \%$ entering and exiting the site at the NW $319^{\text {th }}$ Street/NW $31^{\text {st }}$ Avenue (east access) intersection, and $50 \%$ entering and exiting the site at the west access along $319^{\text {th }}$ Street. The $50 / 50$ trip distribution split also translates to a 50/50 lane utilization for the northbound left-turn lanes at the NW La Center Road/NB Ramp Terminal.


## Analysis Methodology

The traffic signal intersection operational analyses presented in this technical memorandum were prepared following Highway Capacity Manual 2010 (HCM 2010) analysis procedures using Synchro 8 software. Synchro 8 analyzes individual signalized intersections as well as coordinated traffic signal timings along a corridor. Queuing analyses reflects the average $95^{\text {th }}$ percentile queues obtained from five simulation runs using SimTraffic software. Queue lengths are rounded up to the nearest 25 feet.

## SIGNALIZED CORRIDOR ASSESSMENT

The following sections assess intersection operations and queueing on the corridor with signal control at the ramp terminals and frontage road intersections. The analysis was utilized to determine the lane configurations and storage necessary to accommodate future traffic projections.

## Opening Year 2017 Build (Signalized) Total Traffic Conditions

The build total traffic conditions analysis forecasts how the study intersections will operate with the traffic generated by the Cowlitz Reservation Development assuming traffic signals and associated lane widenings are installed at the intersection of NW $31^{\text {st }}$ Avenue/NW $319^{\text {th }}$ Street/East Site Access and the I-5 ramp terminals. The traffic volumes at the intersection of NW La Center Road/NW Paradise Park Road are not sufficient to warrant signalization, so the intersection was modeled with two-way stop control.

Figure 1 illustrates the assumed potential 2017 build lane configurations. Figure 2 illustrates the 2017 signalized design concept at the study intersections. Table 1 provides level of service (LOS) results for the signalized intersections during the weekday AM and weekend peak hours (also shown in Figure 1).

Appendix " $A$ " includes the 2017 build total intersection operations analysis worksheets.
Table 12017 Signalized Intersection Operations (Build)

| Intersection | Operating <br> Standard | Weekday AM <br> Peak Hour | Weekend <br> Peak Hour |
| :--- | :---: | :---: | :---: |
| NW 319 ${ }^{\text {th }}$ Street/NW 31 ${ }^{\text {st }}$ Avenue | D | A | B |
| NW La Center Road/I-5 SB Ramp Terminal | C | A | A |
| NW La Center Road/I-5 NB Ramp Terminal | C | B | B |
| NW La Center Road/NW Paradise Park Road | E | E | E |

As shown in Table 1, all intersections satisfy the LOS criteria.




Table 2 provides the associated projected $95^{\text {th }}$ percentile queue lengths. Available storage lengths are provided based on the conceptual design illustrated in Figure 2.

Table 22017 Signalized Intersection $95^{\text {th }}$ Percentile Queue Lengths (feet) (Build)

| Intersection | Approach Lane | Weekday AM Peak Hour | Weekend <br> Peak Hour | Available Storage | Adequate Storage? |
| :---: | :---: | :---: | :---: | :---: | :---: |
| NW 319 ${ }^{\text {th }}$ Street/ NW 31 ${ }^{\text {st }}$ Avenue (Traffic Signal) | SB Left | 75 | 200 | 225 | Yes |
|  | SB Through/Right | 25 | 25 | 300 | Yes |
|  | EB Left | 25 | 25 | 150 | Yes |
|  | EB Through/Right | 75 | 175 | 500+ | Yes |
|  | NB Left | 25 | 25 | 100 | Yes |
|  | NB Through/Right | 75 | 75 | 500+ | Yes |
|  | WB Left | 75 | 125 | 325 | Yes |
|  | WB Through | 100 | 300 | $550{ }^{1}$ | Yes |
|  | WB Right | 75 | 150 | $550{ }^{1}$ | Yes |
| NW La Center Road/ I-5 SB Ramp Terminal (Traffic Signal) | SB Through/Left | 150 | 150 | 500+ | Yes |
|  | SB Right | 25 | 100 | 425 | Yes |
|  | EB Through | 175 | 125 | $550{ }^{1}$ | Yes |
|  | WB Through (right lane) | 125 | 150 | $450{ }^{1}$ | Yes |
|  | WB Through (middle lane) | 150 | 125 | $450{ }^{1}$ | Yes |
|  | WB Left | 150 | 50 | 225 | Yes |
| NW La Center Road/ I-5 NB Ramp Terminal (Traffic Signal) | NB Left (left lane) | 150 | 200 | 300 | Yes |
|  | NB Left (middle lane) | 125 | 250 | 500+ | Yes |
|  | NB Through/Right | 150 | 200 | 500+ | Yes |
|  | WB Through | 200 | 200 | $425^{1}$ | Yes |
|  | WB Through/Right | 100 | 125 | 200 | Yes |
|  | EB Left | 125 | 100 | 175 | Yes |
|  | EB Through | 75 | 100 | $450{ }^{1}$ | Yes |
| NW La Center Road/ Paradise Park Road (Two-Way StopControl) | SB | 125 | 75 | 125 | Yes |
|  | EB Left | 100 | 75 | 125 | Yes |
|  | NB | 50 | 75 | 15 | Yes |
|  | WB Left | 25 | 25 | 125 | Yes |
| ${ }^{1}$ Distance to adjacent intersection $E B=$ Eastbound, $N B=$ Northbound, $S B=$ Southbound, $W B=W e s t b o u n d$ |  |  |  |  |  |

Table 2 shows the projected $95^{\text {th }}$ percentile queues can be accommodated within the available storage areas.

## Future Year 2037 Total Traffic Conditions

An operational analysis was conducted for the horizon year 2037 to ensure the proposed interchange area improvements identified under the year 2017 do not preclude future improvement needs.

## 2037 No-Build Analysis

A 2037 "No-Build" analysis was conducted to determine what infrastructure improvements may be needed beyond those identified in the 2017 total signalized build analysis. The operations at the study intersections in 2037 with the proposed Cowlitz Reservation Development and 2017 signalized infrastructure improvements are provided in Table 3 and Figure 3.

Appendix " $B$ " includes the 2037 no-build total intersection operations analysis worksheets.

Table 32037 Signalized Intersection Operations (No-Build)

| Intersection | Operating <br> Standard | Weekday AM <br> Peak Hour | Weekend <br> Peak Hour |
| :--- | :---: | :---: | :---: |
| NW $319^{\text {th }}$ Street/NW 31 ${ }^{\text {st }}$ Avenue | D | A | C |
| NW La Center Road/I-5 SB Ramp Terminal | D | B | B |
| NW La Center Road/I-5 NB Ramp Terminal | D | C | C |
| NW La Center Road/NW Paradise Park Road | E | F | F |

As shown in Table 3, the NW $319^{\text {th }}$ Street/NW $31^{\text {st }}$ Avenue, NW La Center Road/Southbound Ramp, and NW La Center Road/Northbound Ramp intersections satisfy the LOS criteria. Although these intersections meet the overall LOS criteria, some intersection approaches are near capacity during the weekday AM and weekend peak periods. In addition, considerations should be made for additional lanes at these intersections as described in the next section.


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## 2037 Build Analysis

While the $319^{\text {th }}$ Street $/ 31^{\text {st }}$ Avenue and ramp terminal intersections meet the overall LOS criteria, the long-term 2037 design should consider the following improvement measures (beyond those needed in 2017) to mitigate for long-term local and regional growth not accounted for in the RTC travel demand models and not associated with the Cowlitz Reservation Development:

- a second eastbound and westbound through lane along NW $319^{\text {th }}$ Street west of the NW $31^{\text {st }}$ Avenue intersection;
- a second eastbound through lane on the overpass between the l-5 ramp terminal intersections;
- a second westbound and eastbound left-turn lane on the overpass between the l-5 ramp terminal intersections;
- a traffic signal at NW La Center Road/NW Paradise Park Road with two thru lanes on the eastbound and westbound approaches.

Figure 4 illustrates the assumed potential 2037 build lane configurations. Figure 5 illustrates the 2037 signalized design concept at the study intersection. Table 4 provides level of service (LOS) results for the signalized intersections during the weekday AM and weekend peak hours (also shown in Figure 4).

Appendix " $C$ " includes the 2037 build total intersection operations analysis worksheets.
Table 42037 Signalized Intersection Operations (Build)

| Intersection | Operating <br> Standard | Weekday AM <br> Hour | Weekend <br> Hour |
| :--- | :---: | :---: | :---: |
| NW 319 ${ }^{\text {th }}$ Street/NW 31 ${ }^{\text {st }}$ Avenue | D | B | C |
| NW La Center Road/I-5 SB Ramp Terminal | D | B | B |
| NW La Center Road/I-5 NB Ramp Terminal ${ }^{1}$ | D | B | C |
| NW La Center Road/NW Paradise Park Road | D | A | B |

${ }^{1}$ Lane utilization at this intersection assumed all westbound traffic turning left onto the I-5 southbound on-ramp at the NW 319th Street/l-5 SB Ramp intersection, would line up in the westbound left/through lane (left lane) at the NW La Center Road/I-5 NB Ramp Terminal.

As shown in Table 4, all intersections are projected to operate acceptably in 2037 with signal control and the lane configurations shown in Figure 4 . Table 5 provides projected $95^{\text {th }}$ percentile queue lengths. Available storage lengths are provided based on the conceptual design illustrated in Figure 5.


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Table 52037 Signalized Intersection $95^{\text {th }}$ Percentile Queue Lengths (feet) (Build)

| Intersection | Approach Lane | Weekday AM Peak Hour | Weekend Peak Hour | Available Storage | Adequate Storage? |
| :---: | :---: | :---: | :---: | :---: | :---: |
| NW 319 ${ }^{\text {th }}$ Street/ NW 31 ${ }^{\text {st }}$ Avenue (Traffic Signal) | SB Left | 100 | 350 | 350 | Yes |
|  | SB Through/Right | 50 | 50 | 300 | Yes |
|  | EB Left | 25 | 25 | 150 | Yes |
|  | EB Through | 75 | 150 | 500+ | Yes |
|  | EB Through/Right | 100 | 300 | 500+ | Yes |
|  | NB Left | 25 | 25 | 100 | Yes |
|  | NB Through/Right | 100 | 175 | 500+ | Yes |
|  | WB Left | 150 | 175 | 375 | Yes |
|  | WB Through | 75 | 225 | $550{ }^{1}$ | Yes |
|  | WB Through/Right | 125 | 325 | $550{ }^{1}$ | Yes |
| NW $319^{\text {th }}$ Street/ I-5 SB Ramp Terminal (Traffic Signal) | SB Through/Left | 225 | 250 | 500+ | Yes |
|  | SB Right | 75 | 150 | 425 | Yes |
|  | EB Through | 200 | 175 | $550{ }^{1}$ | Yes |
|  | EB Through | 150 | 100 | $550{ }^{1}$ | Yes |
|  | WB Through | 100 | 150 | $450{ }^{1}$ | Yes |
|  | WB Through | 125 | 200 | $450{ }^{1}$ | Yes |
|  | WB Left | 125 | 50 | 225 | Yes |
|  | WB Left | 150 | 75 | 225 | Yes |
| NW La Center Road/ I-5 NB Ramp Terminal (Traffic Signal) | NB Left | 150 | 350 | 350 | Yes |
|  | NB Left | 200 | 400 | 500+ | Yes |
|  | NB Through/Right | 175 | 375 | 500+ | Yes |
|  | WB Through | 250 | 225 | $425^{1}$ | Yes |
|  | WB Through/Right | 150 | 250 | $425^{1}$ | Yes |
|  | EB Left | 100 | 75 | 175 | Yes |
|  | EB Left | 125 | 100 | 175 | Yes |
|  | EB Through | 75 | 75 | $450{ }^{1}$ | Yes |
|  | EB Through | 100 | 100 | $450{ }^{1}$ | Yes |
| NW La Center Road/ NW Paradise Park Road (Traffic Signal) | SB Left | 100 | 75 | 175 | Yes |
|  | SB Through/Right | 75 | 50 | 500+ | Yes |
|  | EB Left | 75 | 75 | 175 | Yes |
|  | EB Through | 100 | 175 | $400^{1}$ | Yes |
|  | EB Through/Right | 150 | 200 | $400^{1}$ | Yes |
|  | NB Left | 100 | 175 | 125 | Yes |
|  | NB Through/Right | 100 | 100 | 500+ | Yes |
|  | WB Left | 125 | 100 | 100 | Yes |
|  | WB Through | 150 | 150 | 500+ | Yes |
|  | WB Through/Right | 125 | 125 | 275 | Yes |

${ }^{1}$ Distance to adjacent intersection
$E B=E a s t b o u n d, N B=$ Northbound, $\mathrm{SB}=$ Southbound, WB=Westbound

Table 5 shows the projected $95^{\text {th }}$ percentile queues can be accommodated within the available storage areas.

## CONSTRUCTION PHASING CONSIDERATIONS

Preliminary construction phasing insights are summarized below.

## I-5 Overpass Alignment Options

There are two options for the NW $319^{\text {th }}$ Street-NW La Center Road alignment across the I-5 overpass; each with its own bridge construction approach.

- Option \#1 - Maintain existing NW $319^{\text {th }}$ Street alignment (west side of I-5). Half of the new bridge (to accommodate 2017 traffic conditions) will be built to the south of the existing bridge. During construction, traffic will then be shifted onto the new bridge, while the existing bridge is being removed and the north half of the bridge is being completed. To accommodate future 2037 traffic conditions the bridge will be widening to the north.
- Option \#2 - Realign NW $319^{\text {th }}$ Street to the south of its current location. The entire new bridge (to accommodate 2017 traffic conditions) will be built to the south of the existing bridge. To accommodate future 2037 traffic conditions the bridge will be widened to the north.

For the signalized option, construction phasing between 2017 and 2037 would be planned so that future 2037 roadway needs would be widened to the outside from the 2017 configuration. This phased implementation approach will minimize "throw-away" work and outlines an approach to locate and construct signal equipment to accommodate the ultimate configuration, while serving the near-term configuration with narrower cross sections. Special attention should be given to drainage (especially with the installation of curbed facilities) to minimize reconstruction.

Existing on-ramp and off-ramp alignments could be maintained, reducing overall impacts to the project. All ramp widening could be accomplished by maintaining the inside edge of the existing ramp and widening to the outside based on capacity needs. However, the geometry of the northbound offand southbound on-ramps will be revisited to address existing undesirable horizontal alignments (i.e., radius of curve closets to the freeway).

## CONCLUSIONS

Based on the operations and queueing assessment presented within this memorandum, signals can be constructed at the ramp terminals and frontage roads of the NW La Center Road/I-5 Interchange to support projected future traffic conditions. There are advantages and constraints associated with this option. For one, signals have the advantage of being easier to construct while maintaining traffic during construction.

The information presented in this memorandum was used to inform the decision process and selection of traffic control as part of the NW La Center Road/I-5 Interchange IJR.

## Appendix A 2017 Build Total Intersection Operations Analysis Worksheets

|  | $\rangle$ | $\rightarrow$ | 7 | $\downarrow$ | $\leftarrow$ | 4 | 4 | $\dagger$ | $>$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | $\hat{\square}$ |  | \% | $\uparrow$ | 「 | \% | 1 |  | ${ }^{7}$ | F |  |
| Volume (veh/h) | 5 | 155 | 15 | 49 | 192 | 146 | 5 | 5 | 78 | 110 | 5 | 5 |
| Number | 5 | 2 | 12 | 1 | 6 | 16 | 3 | 8 | 18 | 7 | 4 | 14 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 0.99 |  | 0.98 | 0.98 |  | 0.98 | 0.99 |  | 0.99 | 0.99 |  | 0.99 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1900 | 1833 | 1900 | 1712 | 1863 | 1881 | 1900 | 1562 | 1900 | 1881 | 1881 | 1900 |
| Adj Flow Rate, veh/h | 5 | 155 | 15 | 49 | 192 | 146 | 5 | 5 | 78 | 110 | 5 | 5 |
| Adj No. of Lanes | 1 | 1 | 0 | 1 | 1 | 1 | 1 | 1 | 0 | 1 | 1 | 0 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh, \% | 0 | 4 | 4 | 11 | 2 | 1 | 0 | 1 | 1 | 1 | 1 | 1 |
| Cap, veh/h | 608 | 558 | 54 | 629 | 633 | 532 | 606 | 16 | 247 | 522 | 171 | 171 |
| Arrive On Green | 0.34 | 0.34 | 0.34 | 0.34 | 0.34 | 0.34 | 0.20 | 0.20 | 0.20 | 0.20 | 0.20 | 0.20 |
| Sat Flow, veh/h | 1046 | 1642 | 159 | 1095 | 1863 | 1564 | 1410 | 80 | 1244 | 1310 | 858 | 858 |
| Grp Volume(v), veh/h | 5 | 0 | 170 | 49 | 192 | 146 | 5 | 0 | 83 | 110 | 0 | 10 |
| Grp Sat Flow(s),veh/h/ln | 1046 | 0 | 1801 | 1095 | 1863 | 1564 | 1410 | 0 | 1323 | 1310 | 0 | 1717 |
| Q Serve(g_s), s | 0.1 | 0.0 | 1.5 | 0.7 | 1.6 | 1.5 | 0.1 | 0.0 | 1.2 | 1.7 | 0.0 | 0.1 |
| Cycle Q Clear(g_c), s | 1.7 | 0.0 | 1.5 | 2.2 | 1.6 | 1.5 | 0.2 | 0.0 | 1.2 | 2.9 | 0.0 | 0.1 |
| Prop In Lane | 1.00 |  | 0.09 | 1.00 |  | 1.00 | 1.00 |  | 0.94 | 1.00 |  | 0.50 |
| Lane Grp Cap(c), veh/h | 608 | 0 | 612 | 629 | 633 | 532 | 606 | 0 | 263 | 522 | 0 | 341 |
| V/C Ratio(X) | 0.01 | 0.00 | 0.28 | 0.08 | 0.30 | 0.27 | 0.01 | 0.00 | 0.32 | 0.21 | 0.00 | 0.03 |
| Avail Cap(c_a), veh/h | 1459 | 0 | 2077 | 1520 | 2149 | 1804 | 1951 | 0 | 1526 | 1773 | 0 | 1980 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 5.9 | 0.0 | 5.2 | 6.0 | 5.3 | 5.2 | 7.1 | 0.0 | 7.4 | 8.6 | 0.0 | 7.0 |
| Incr Delay (d2), s/veh | 0.0 | 0.0 | 0.2 | 0.1 | 0.3 | 0.3 | 0.0 | 0.0 | 0.7 | 0.2 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.0 | 0.0 | 0.7 | 0.2 | 0.8 | 0.6 | 0.0 | 0.0 | 0.5 | 0.6 | 0.0 | 0.1 |
| LnGrp Delay(d),s/veh | 5.9 | 0.0 | 5.5 | 6.1 | 5.5 | 5.5 | 7.1 | 0.0 | 8.1 | 8.8 | 0.0 | 7.0 |
| LnGrp LOS | A |  | A | A | A | A | A |  | A | A |  | A |
| Approach Vol, veh/h |  | 175 |  |  | 387 |  |  | 88 |  |  | 120 |  |
| Approach Delay, s/veh |  | 5.5 |  |  | 5.6 |  |  | 8.0 |  |  | 8.7 |  |
| Approach LOS |  | A |  |  | A |  |  | A |  |  | A |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Assigned Phs |  | 2 |  | 4 |  | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), s |  | 12.4 |  | 9.3 |  | 12.4 |  | 9.3 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ) , s |  | 5.0 |  | 5.0 |  | 5.0 |  | 5.0 |  |  |  |  |
| Max Green Setting (Gmax), s |  | 25.0 |  | 25.0 |  | 25.0 |  | 25.0 |  |  |  |  |
| Max Q Clear Time (g_c+l1), s |  | 3.7 |  | 4.9 |  | 4.2 |  | 3.2 |  |  |  |  |
| Green Ext Time (p_c), s |  | 2.6 |  | 0.8 |  | 2.6 |  | 0.8 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 6.3 |  |  |  |  |  |  |  |  |  |
| HCM 2010 LOS |  |  | A |  |  |  |  |  |  |  |  |  |

## Notes

User approved pedestrian interval to be less than phase max green.

|  | 4 |  |  | $\dagger$ | $\leftarrow$ | 4 | 4 | 4 | $p$ | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ | 「 | \％ | 个个 |  |  |  |  |  | $\uparrow$ | F |
| Volume（veh／h） | 0 | 118 | 225 | 535 | 361 | 0 | 0 | 0 | 0 | 118 | 4 | 25 |
| Number | 5 | 2 | 12 | 1 | 6 | 16 |  |  |  | 7 | 4 | 14 |
| Initial $\mathrm{Q}(\mathrm{Qb})$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 |  |  |  | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow，veh／h／ln | 0 | 1583 | 1863 | 1827 | 1863 | 0 |  |  |  | 1900 | 1664 | 1759 |
| Adj Flow Rate，veh／h | 0 | 118 | 0 | 535 | 361 | 0 |  |  |  | 118 | 4 | 25 |
| Adj No．of Lanes | 0 | 1 | 1 | 1 | 2 | 0 |  |  |  | 0 | 1 | 1 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh，\％ | 0 | 20 | 2 | 4 | 2 | 0 |  |  |  | 8 | 50 | 8 |
| Cap，veh／h | 0 | 258 | 258 | 614 | 2279 | 0 |  |  |  | 154 | 5 | 150 |
| Arrive On Green | 0.00 | 0.16 | 0.00 | 0.59 | 1.00 | 0.00 |  |  |  | 0.10 | 0.10 | 0.10 |
| Sat Flow，veh／h | 0 | 1583 | 1583 | 1740 | 3632 | 0 |  |  |  | 1535 | 52 | 1495 |
| Grp Volume（v），veh／h | 0 | 118 | 0 | 535 | 361 | 0 |  |  |  | 122 | 0 | 25 |
| Grp Sat Flow（s），veh／h／ln | 0 | 1583 | 1583 | 1740 | 1770 | 0 |  |  |  | 1587 | 0 | 1495 |
| Q Serve（g＿s），s | 0.0 | 2.6 | 0.0 | 10.2 | 0.0 | 0.0 |  |  |  | 2.9 | 0.0 | 0.6 |
| Cycle Q Clear（g＿c），s | 0.0 | 2.6 | 0.0 | 10.2 | 0.0 | 0.0 |  |  |  | 2.9 | 0.0 | 0.6 |
| Prop In Lane | 0.00 |  | 1.00 | 1.00 |  | 0.00 |  |  |  | 0.97 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 0 | 258 | 258 | 614 | 2279 | 0 |  |  |  | 160 | 0 | 150 |
| V／C Ratio（X） | 0.00 | 0.46 | 0.00 | 0.87 | 0.16 | 0.00 |  |  |  | 0.76 | 0.00 | 0.17 |
| Avail Cap（c＿a），veh／h | 0 | 485 | 485 | 1600 | 4792 | 0 |  |  |  | 689 | 0 | 649 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.67 | 1.67 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 0.00 | 0.99 | 0.00 | 0.93 | 0.93 | 0.00 |  |  |  | 1.00 | 0.00 | 1.00 |
| Uniform Delay（d），s／veh | 0.0 | 14.8 | 0.0 | 7.3 | 0.0 | 0.0 |  |  |  | 17.2 | 0.0 | 16.1 |
| Incr Delay（d2），s／veh | 0.0 | 1.2 | 0.0 | 3.7 | 0.0 | 0.0 |  |  |  | 7.4 | 0.0 | 0.5 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.0 | 1.2 | 0.0 | 5.2 | 0.0 | 0.0 |  |  |  | 1.6 | 0.0 | 0.3 |
| LnGrp Delay（d），s／veh | 0.0 | 16.1 | 0.0 | 11.0 | 0.0 | 0.0 |  |  |  | 24.6 | 0.0 | 16.6 |
| LnGrp LOS |  | B |  | B | A |  |  |  |  | C |  | B |
| Approach Vol，veh／h |  | 118 |  |  | 896 |  |  |  |  |  | 147 |  |
| Approach Delay，s／veh |  | 16.1 |  |  | 6.6 |  |  |  |  |  | 23.2 |  |
| Approach LOS |  | B |  |  | A |  |  |  |  |  | C |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Assigned Phs | 1 | 2 |  | 4 |  | 6 |  |  |  |  |  |  |
| Phs Duration（ $G+Y+R \mathrm{c}$ ），s | 59.7 | 11.4 |  | 8.9 |  | 71.1 |  |  |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），s | 5.0 | 5.0 |  | 5.0 |  | 5.0 |  |  |  |  |  |  |
| Max Green Setting（Gmax），s | 36.0 | 12.0 |  | 17.0 |  | 53.0 |  |  |  |  |  |  |
| Max Q Clear Time（ $\mathrm{g}_{\sim} \mathrm{c}+11$ ），s | 12.2 | 4.6 |  | 4.9 |  | 2.0 |  |  |  |  |  |  |
| Green Ext Time（p＿c），s | 1.7 | 1.6 |  | 0.0 |  | 3.1 |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 9.7 |  |  |  |  |  |  |  |  |  |
| HCM 2010 LOS |  |  | A |  |  |  |  |  |  |  |  |  |



| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 5.3 |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 91 | 384 | 5 | 10 | 628 | 9 | 10 | 0 | 5 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 5 | 0 | 5 | 0 | 0 | 5 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | 200 | - | - | 200 | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 42 | 13 | 0 | 25 | 3 | 20 | 14 | 0 | 25 |
| Mumt Flow | 91 | 384 | 5 | 10 | 628 | 9 | 10 | 0 | 5 |
| Major/Minor | Major1 |  |  | Major2 |  |  | Minor1 |  |  |
| Conflicting Flow All | 642 | 0 | 0 | 394 | 0 | 0 | 1266 | 1236 | 397 |
| Stage 1 | - | - | - | - | - | - | 574 | 574 |  |
| Stage 2 | - | - | - | - | - | - | 692 | 662 |  |
| Critical Hdwy | 4.52 | - | - | 4.35 | - | - | 7.24 | 6.5 | 6.45 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.24 | 5.5 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.24 | 5.5 |  |
| Follow-up Hdwy | 2.578 | - | - | 2.425 | - | - | 3.626 | 4 | 3.525 |
| Pot Cap-1 Maneuver | 778 | - | - | 1050 | - | - | 138 | 178 | 605 |
| Stage 1 | - | - | - | - | - | - | 483 | 506 |  |
| Stage 2 | - | - | - | - | - | - | 415 | 462 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 778 | - | - | 1046 | - | - | 102 | 154 | 600 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 102 | 154 |  |
| Stage 1 | - | - | - | - | - | - | 425 | 445 |  |
| Stage 2 | - | - | - | - | - | - | 344 | 456 |  |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 1.9 | 0.1 | 33.5 |
| HCM LOS |  |  | D |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 141 | 778 | - | - | 1046 | - | - | 186 |
| HCM Lane V/C Ratio | 0.106 | 0.117 | - | - | 0.01 | - | - | 0.581 |
| HCM Control Delay (s) | 33.5 | 10.2 | - | - | 8.5 | - | - | 48.2 |
| HCM Lane LOS | D | B | - | - | A | - | - | E |
| HCM 95th \%tile Q(veh) | 0.3 | 0.4 | - | - | 0 | - | - | 3.1 |


| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | SBL | SBT | SBR |
| Vol, veh/h | 39 | 4 | 65 |
| Conflicting Peds, \#/hr | 5 | 0 | 0 |
| Sign Control | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | - | - | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 |
| Heavy Vehicles, \% | 69 | 100 | 30 |
| Mvmt Flow | 39 | 4 | 65 |
|  |  |  |  |


| Major/Minor | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Conflicting Flow All | 1234 | 1234 | 638 |
| $\quad$ Stage 1 | 658 | 658 | - |
| $\quad$ Stage 2 | 576 | 576 | - |
| Critical Hdwy | 7.79 | 7.5 | 6.5 |
| Critical Hdwy Stg 1 | 6.79 | 6.5 | - |
| Critical Hdwy Stg 2 | 6.79 | 6.5 | - |
| Follow-up Hdwy | 4.121 | 4.9 | 3.57 |
| Pot Cap-1 Maneuver | 113 | 116 | 430 |
| $\quad$ Stage 1 | 359 | 339 | - |
| $\quad$ Stage 2 | 403 | 375 | - |
| Platoon blocked, \% |  |  |  |
| Mov Cap-1 Maneuver | 100 | 101 | 428 |
| Mov Cap-2 Maneuver | 100 | 101 | - |
| Stage 1 | 316 | 334 | - |
| Stage 2 | 351 | 330 | - |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | 48.2 |
| HCM LOS | E |

[^4]Intersection: 102: NW 31st Ave/East Access \& NW 319th St

| Movement | EB | EB | WB | WB | WB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | T | R | L | TR | L | TR |
| Maximum Queue (ft) | 28 | 92 | 76 | 140 | 102 | 28 | 78 | 94 | 23 |
| Average Queue (ft) | 4 | 33 | 25 | 40 | 35 | 3 | 35 | 41 | 6 |
| 95th Queue (ft) | 19 | 71 | 61 | 97 | 76 | 17 | 67 | 74 | 22 |
| Link Distance (ft) |  | 650 |  | 532 | 532 |  | 1521 |  | 545 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  | 305 |  |  | 300 |  | 300 |  |
| Storage Bay Dist (ft) | 300 |  | 325 |  |  |  |  |  |  |

Intersection: 103: I-5 SB On Ramp/l-5 SB Off Ramp \& NW 319th St/NW La Center Rd

| Movement | EB | WB | WB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | L | T | T | LT | R |
| Maximum Queue (ft) | 182 | 180 | 161 | 147 | 165 | 45 |
| Average Queue (ft) | 85 | 78 | 80 | 62 | 74 | 14 |
| 95th Queue (ft) | 161 | 139 | 141 | 119 | 135 | 35 |
| Link Distance (ft) | 532 |  | 502 | 502 | 656 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  | 400 |  |
| Storage Bay Dist (ft) |  | 225 |  |  |  |  |

Intersection: 104: I-5 NB Off Ramp/l-5 NB On Ramp \& NW La Center Rd

| Movement | EB | EB | WB | WB | NB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | T | T | TR | L | L | TR |
| Maximum Queue (ft) | 143 | 109 | 215 | 120 | 143 | 155 | 172 |
| Average Queue (ft) | 64 | 25 | 119 | 40 | 77 | 71 | 76 |
| 95th Queue (ft) | 123 | 74 | 203 | 89 | 133 | 123 | 132 |
| Link Distance (ft) | 502 | 502 | 211 | 211 |  | 810 | 810 |
| Upstream Blk Time (\%) |  |  | 0 |  |  |  |  |
| Queuing Penalty (veh) |  |  | 2 |  |  |  |  |
| Storage Bay Dist (ft) |  |  |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  |  |

Intersection: 105: NW Paradise Park Rd \& NW La Center Rd

| Movement | EB | EB | WB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | TR | LTR | LTR |
| Maximum Queue (ft) | 115 | 39 | 45 | 17 | 51 | 149 |
| Average Queue (ft) | 49 | 1 | 5 | 1 | 12 | 62 |
| 95th Queue (ft) | 96 | 17 | 25 | 7 | 38 | 124 |
| Link Distance (ft) |  | 189 |  | 2587 | 1309 | 964 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  | 200 |  |  |  |
| Storage Bay Dist (ft) | 200 |  |  |  |  |  |

## Zone Summary

[^5]|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |

## Notes

User approved pedestrian interval to be less than phase max green.

|  | 4 |  |  | $\checkmark$ | 4 | 4 | 4 | 4 | $p$ | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ | 「 | * | 个4 |  |  |  |  |  | $\uparrow$ | 7 |
| Volume (veh/h) | 0 | 146 | 636 | 375 | 982 | 0 | 0 | 0 | 0 | 172 | 4 | 141 |
| Number | 5 | 2 | 12 | 1 | 6 | 16 |  |  |  | 7 | 4 | 14 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 |  |  |  | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1845 | 1863 | 1863 | 1881 | 0 |  |  |  | 1900 | 1829 | 1759 |
| Adj Flow Rate, veh/h | 0 | 146 | 0 | 375 | 982 | 0 |  |  |  | 172 | 4 | 141 |
| Adj No. of Lanes | 0 | 1 | 1 | 1 | 2 | 0 |  |  |  | 0 | 1 | 1 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh, \% | 0 | 3 | 2 | 2 | 1 | 0 |  |  |  | 8 | 0 | 8 |
| Cap, veh/h | 0 | 423 | 363 | 698 | 2518 | 0 |  |  |  | 224 | 5 | 197 |
| Arrive On Green | 0.00 | 0.23 | 0.00 | 0.79 | 1.00 | 0.00 |  |  |  | 0.13 | 0.13 | 0.13 |
| Sat Flow, veh/h | 0 | 1845 | 1583 | 1774 | 3668 | 0 |  |  |  | 1704 | 40 | 1495 |
| Grp Volume(v), veh/h | 0 | 146 | 0 | 375 | 982 | 0 |  |  |  | 176 | 0 | 141 |
| Grp Sat Flow(s), veh/h/ln | 0 | 1845 | 1583 | 1774 | 1787 | 0 |  |  |  | 1743 | 0 | 1495 |
| Q Serve(g_s), s | 0.0 | 4.0 | 0.0 | 4.8 | 0.0 | 0.0 |  |  |  | 6.0 | 0.0 | 5.5 |
| Cycle Q Clear(g_c), s | 0.0 | 4.0 | 0.0 | 4.8 | 0.0 | 0.0 |  |  |  | 6.0 | 0.0 | 5.5 |
| Prop In Lane | 0.00 |  | 1.00 | 1.00 |  | 0.00 |  |  |  | 0.98 |  | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 423 | 363 | 698 | 2518 | 0 |  |  |  | 229 | 0 | 197 |
| V/C Ratio(X) | 0.00 | 0.35 | 0.00 | 0.54 | 0.39 | 0.00 |  |  |  | 0.77 | 0.00 | 0.72 |
| Avail Cap(c_a), veh/h | 0 | 423 | 363 | 698 | 2518 | 0 |  |  |  | 486 | 0 | 417 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.00 | 0.71 | 0.00 | 0.84 | 0.84 | 0.00 |  |  |  | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 19.7 | 0.0 | 4.5 | 0.0 | 0.0 |  |  |  | 25.6 | 0.0 | 25.4 |
| Incr Delay (d2), s/veh | 0.0 | 0.3 | 0.0 | 2.5 | 0.4 | 0.0 |  |  |  | 5.3 | 0.0 | 4.8 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.0 | 2.1 | 0.0 | 2.7 | 0.1 | 0.0 |  |  |  | 3.2 | 0.0 | 2.5 |
| LnGrp Delay(d),s/veh | 0.0 | 20.0 | 0.0 | 7.0 | 0.4 | 0.0 |  |  |  | 30.9 | 0.0 | 30.2 |
| LnGrp LOS |  | C |  | A | A |  |  |  |  | C |  | C |
| Approach Vol, veh/h |  | 146 |  |  | 1357 |  |  |  |  |  | 317 |  |
| Approach Delay, s/veh |  | 20.0 |  |  | 2.2 |  |  |  |  |  | 30.6 |  |
| Approach LOS |  | C |  |  | A |  |  |  |  |  | C |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Assigned Phs | 1 | 2 |  | 4 |  | 6 |  |  |  |  |  |  |
| Phs Duration ( $G+Y+R c$ ), $s$ | 29.0 | 19.0 |  | 13.0 |  | 48.0 |  |  |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ) , s | 5.0 | 5.0 |  | 5.0 |  | 5.0 |  |  |  |  |  |  |
| Max Green Setting (Gmax), s | 24.0 | 14.0 |  | 17.0 |  | 43.0 |  |  |  |  |  |  |
| Max Q Clear Time (g_c+l1), s | 6.8 | 6.0 |  | 8.0 |  | 2.0 |  |  |  |  |  |  |
| Green Ext Time (p_c), s | 1.0 | 4.3 |  | 0.1 |  | 9.2 |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 8.6 |  |  |  |  |  |  |  |  |  |
| HCM 2010 LOS |  |  | A |  |  |  |  |  |  |  |  |  |


|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 2.8 |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 82 | 721 | 5 | 5 | 455 | 8 | 10 | 5 | 5 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 5 | 0 | 5 | 0 | 0 | 5 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | 200 | - | - | 200 | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 13 | 4 | 17 | 0 | 3 | 17 | 11 | 0 | 50 |
| Mumt Flow | 82 | 721 | 5 | 5 | 455 | 8 | 10 | 5 | 5 |
| Major/Minor | Major1 |  |  | Major2 |  |  | Minor1 |  |  |
| Conflicting Flow All | 468 | 0 | 0 | 731 | 0 | 0 | 1386 | 1371 | 734 |
| Stage 1 | - | - | - | - | - | - | 893 | 893 |  |
| Stage 2 | - | - | - | - | - | - | 493 | 478 |  |
| Critical Hdwy | 4.23 | - | - | 4.1 | - | - | 7.21 | 6.5 | 6.7 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.21 | 5.5 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.21 | 5.5 |  |
| Follow-up Hdwy | 2.317 | - | - | 2.2 | - | - | 3.599 | 4 | 3.75 |
| Pot Cap-1 Maneuver | 1038 | - | - | 883 | - | - | 115 | 147 | 350 |
| Stage 1 | - | - | - | - | - | - | 324 | 363 |  |
| Stage 2 | - | - | - | - | - | - | 541 | 559 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1038 | - | - | 879 | - | - | 99 | 133 | 347 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 99 | 133 |  |
| Stage 1 | - | - | - | - | - | - | 297 | 333 |  |
| Stage 2 | - | - | - | - | - | - | 503 | 554 |  |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0.9 | 0.1 | 37.4 |
| HCM LOS |  |  | E |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 131 | 1038 | - | - | 879 | - | - | 186 |
| HCM Lane V/C Ratio | 0.153 | 0.079 | - | - | 0.006 | - | - | 0.36 |
| HCM Control Delay (s) | 37.4 | 8.8 | - | - | 9.1 | - | - | 34.9 |
| HCM Lane LOS | E | A | - | - | A | - | - | D |
| HCM 95th \%tile Q(veh) | 0.5 | 0.3 | - | - | 0 | - | - | 1.5 |


| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | 30 | 4 | 33 |
| Vol, veh/h | SBT | SBR |  |
| Conflicting Peds, \#/hr | 5 | 0 | 0 |
| Sign Control | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | - | - | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 |
| Heavy Vehicles, \% | 0 | 0 | 13 |
| Mvmt Flow | 30 | 4 | 33 |
|  |  |  |  |


| Major/Minor | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Conflicting Flow All | 1372 | 1369 | 464 |
| $\quad$ Stage 1 | 474 | 474 | - |
| $\quad$ Stage 2 | 898 | 895 | - |
| Critical Hdwy | 7.1 | 6.5 | 6.33 |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - |
| Follow-up Hdwy | 3.5 | 4 | 3.417 |
| Pot Cap-1 Maneuver | 124 | 148 | 576 |
| $\quad$ Stage 1 | 575 | 561 | - |
| $\quad$ Stage 2 | 337 | 362 | - |
| Platoon blocked, \% |  |  |  |
| Mov Cap-1 Maneuver | 110 | 134 | 574 |
| Mov Cap-2 Maneuver | 110 | 134 | - |
| Stage 1 | 527 | 555 | - |
| Stage 2 | 300 | 332 | - |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | 34.9 |
| HCM LOS | D |

[^6]Intersection: 102: NW 31st Ave/East Access \& NW 319th St

| Movement | EB | EB | WB | WB | WB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | T | R | L | TR | L | TR |
| Maximum Queue (ft) | 30 | 209 | 168 | 375 | 217 | 47 | 91 | 234 | 31 |
| Average Queue (ft) | 6 | 95 | 49 | 153 | 59 | 6 | 39 | 113 | 6 |
| 95th Queue (ft) | 24 | 166 | 117 | 289 | 144 | 27 | 72 | 198 | 23 |
| Link Distance (ft) |  | 650 |  | 532 | 532 |  | 1521 |  | 545 |
| Upstream Blk Time (\%) |  |  |  | 0 | 0 |  |  |  |  |
| Queuing Penalty (veh) |  |  |  | 0 | 0 |  |  | 300 |  |
| Storage Bay Dist (ft) | 300 |  | 325 |  |  | 300 |  | 0 |  |
| Storage Blk Time (\%) |  | 0 |  | 1 |  |  |  | 0 |  |
| Queuing Penalty (veh) |  | 0 |  | 1 |  |  |  |  |  |

Intersection: 103: I-5 SB On Ramp/l-5 SB Off Ramp \& NW 319th St/NW La Center Rd

| Movement | EB | WB | WB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | L | T | T | LT | R |
| Maximum Queue (ft) | 145 | 51 | 178 | 138 | 173 | 104 |
| Average Queue (ft) | 70 | 9 | 82 | 67 | 85 | 45 |
| 95th Queue (ft) | 116 | 36 | 148 | 119 | 142 | 84 |
| Link Distance (ft) | 532 |  | 503 | 503 | 656 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |
| Storage Bay Dist (ft) |  | 225 |  |  |  |  |
| Storage Blk Time (\%) |  |  | 0 |  |  |  |
| Queuing Penalty (veh) |  |  | 1 |  |  |  |

Intersection: 104: I-5 NB Off Ramp/l-5 NB On Ramp \& NW La Center Rd

| Movement | EB | EB | WB | WB | NB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | T | T | TR | L | L | TR |
| Maximum Queue (ft) | 110 | 140 | 186 | 126 | 208 | 328 | 243 |
| Average Queue (ft) | 56 | 45 | 134 | 56 | 124 | 122 | 113 |
| 95th Queue (ft) | 101 | 97 | 198 | 104 | 186 | 237 | 200 |
| Link Distance (ft) |  | 503 | 175 | 175 |  | 817 | 817 |
| Upstream Blk Time (\%) |  |  | 3 |  |  | 0 |  |
| Queuing Penalty (veh) |  |  | 8 |  |  | 0 |  |
| Storage Bay Dist (ft) | 175 |  |  |  | 350 |  |  |
| Storage Blk Time (\%) |  | 0 |  |  |  |  |  |
| Queuing Penalty (veh) |  | 0 |  |  |  |  |  |

Intersection: 105: NW Paradise Park Rd \& NW La Center Rd

| Movement | EB | EB | WB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | TR | L | TR | LTR | LTR |
| Maximum Queue (ft) | 76 | 31 | 19 | 18 | 66 | 86 |
| Average Queue (ft) | 30 | 2 | 1 | 1 | 20 | 33 |
| 95th Queue (ft) | 64 | 17 | 9 | 8 | 55 | 66 |
| Link Distance (ft) |  | 230 |  | 2587 | 1309 | 964 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |
| Storage Bay Dist (ft) | 200 |  | 200 |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  |

## Zone Summary

Zone wide Queuing Penalty: 10

## Appendix B 2037 No-build Total Intersection Operations Analysis Worksheets

|  | $\rangle$ | $\rightarrow$ | 7 | $\downarrow$ | $\leftarrow$ | 4 | 4 | $\dagger$ | $>$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | $\hat{\beta}$ |  | \% | $\uparrow$ | 「 | \% | 1 |  | ${ }^{7}$ | F |  |
| Volume (veh/h) | 5 | 211 | 15 | 193 | 234 | 146 | 5 | 5 | 168 | 110 | 5 | 5 |
| Number | 5 | 2 | 12 | 1 | 6 | 16 | 3 | 8 | 18 | 7 | 4 | 14 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 0.99 |  | 0.98 | 0.99 |  | 0.98 | 0.99 |  | 0.99 | 0.99 |  | 0.99 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1900 | 1832 | 1900 | 1712 | 1863 | 1881 | 1900 | 1553 | 1900 | 1881 | 1881 | 1900 |
| Adj Flow Rate, veh/h | 5 | 211 | 15 | 193 | 234 | 146 | 5 | 5 | 168 | 110 | 5 | 5 |
| Adj No. of Lanes | 1 | 1 | 0 | 1 | 1 | 1 | 1 | 1 | 0 | 1 | 1 | 0 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh, \% | 0 | 4 | 4 | 11 | 2 | 1 | 0 | 1 | 1 | 1 | 1 | 1 |
| Cap, veh/h | 562 | 708 | 50 | 574 | 782 | 659 | 600 | 10 | 346 | 417 | 233 | 233 |
| Arrive On Green | 0.42 | 0.42 | 0.42 | 0.42 | 0.42 | 0.42 | 0.27 | 0.27 | 0.27 | 0.27 | 0.27 | 0.27 |
| Sat Flow, veh/h | 1009 | 1688 | 120 | 1045 | 1863 | 1570 | 1414 | 38 | 1276 | 1212 | 860 | 860 |
| Grp Volume(v), veh/h | 5 | 0 | 226 | 193 | 234 | 146 | 5 | 0 | 173 | 110 | 0 | 10 |
| Grp Sat Flow(s),veh/h/ln | 1009 | 0 | 1808 | 1045 | 1863 | 1570 | 1414 | 0 | 1314 | 1212 | 0 | 1720 |
| Q Serve(g_s), s | 0.1 | 0.0 | 2.7 | 4.9 | 2.7 | 1.9 | 0.1 | 0.0 | 3.6 | 2.7 | 0.0 | 0.1 |
| Cycle Q Clear(g_c), s | 2.8 | 0.0 | 2.7 | 7.5 | 2.7 | 1.9 | 0.2 | 0.0 | 3.6 | 6.3 | 0.0 | 0.1 |
| Prop In Lane | 1.00 |  | 0.07 | 1.00 |  | 1.00 | 1.00 |  | 0.97 | 1.00 |  | 0.50 |
| Lane Grp Cap(c), veh/h | 562 | 0 | 759 | 574 | 782 | 659 | 600 | 0 | 356 | 417 | 0 | 467 |
| V/C Ratio(X) | 0.01 | 0.00 | 0.30 | 0.34 | 0.30 | 0.22 | 0.01 | 0.00 | 0.49 | 0.26 | 0.00 | 0.02 |
| Avail Cap(c_a), veh/h | 1167 | 0 | 1843 | 1201 | 1899 | 1601 | 959 | 0 | 690 | 725 | 0 | 903 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 7.2 | 0.0 | 6.2 | 8.7 | 6.2 | 6.0 | 8.7 | 0.0 | 9.9 | 12.5 | 0.0 | 8.6 |
| Incr Delay (d2), s/veh | 0.0 | 0.0 | 0.2 | 0.3 | 0.2 | 0.2 | 0.0 | 0.0 | 1.0 | 0.3 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.0 | 0.0 | 1.4 | 1.4 | 1.4 | 0.8 | 0.0 | 0.0 | 1.4 | 0.9 | 0.0 | 0.1 |
| LnGrp Delay(d),s/veh | 7.2 | 0.0 | 6.4 | 9.1 | 6.4 | 6.2 | 8.7 | 0.0 | 10.9 | 12.9 | 0.0 | 8.7 |
| LnGrp LOS | A |  | A | A | A | A | A |  | B | B |  | A |
| Approach Vol, veh/h |  | 231 |  |  | 573 |  |  | 178 |  |  | 120 |  |
| Approach Delay, s/veh |  | 6.5 |  |  | 7.3 |  |  | 10.9 |  |  | 12.5 |  |
| Approach LOS |  | A |  |  | A |  |  | B |  |  | B |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Assigned Phs |  | 2 |  | 4 |  | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), s |  | 18.6 |  | 13.8 |  | 18.6 |  | 13.8 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ) , s |  | 5.0 |  | 5.0 |  | 5.0 |  | 5.0 |  |  |  |  |
| Max Green Setting (Gmax), s |  | 33.0 |  | 17.0 |  | 33.0 |  | 17.0 |  |  |  |  |
| Max Q Clear Time (g_c+l1), s |  | 4.8 |  | 8.3 |  | 9.5 |  | 5.6 |  |  |  |  |
| Green Ext Time (p_c), s |  | 4.2 |  | 0.9 |  | 4.0 |  | 1.1 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 8.2 |  |  |  |  |  |  |  |  |  |
| HCM 2010 LOS |  |  | A |  |  |  |  |  |  |  |  |  |

## Notes

User approved pedestrian interval to be less than phase max green.

|  | 4 |  |  | $\checkmark$ | 4 | 4 | 4 | 4 | $p$ | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ | 「 | * | 个4 |  |  |  |  |  | $\uparrow$ | 7 |
| Volume (veh/h) | 0 | 225 | 264 | 627 | 445 | 0 | 0 | 0 | 0 | 177 | 3 | 127 |
| Number | 5 | 2 | 12 | 1 | 6 | 16 |  |  |  | 7 | 4 | 14 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 |  |  |  | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1583 | 1863 | 1827 | 1863 | 0 |  |  |  | 1900 | 1672 | 1759 |
| Adj Flow Rate, veh/h | 0 | 225 | 0 | 627 | 445 | 0 |  |  |  | 177 | 3 | 127 |
| Adj No. of Lanes | 0 | 1 | 1 | 1 | 2 | 0 |  |  |  | 0 | 1 | 1 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh, \% | 0 | 20 | 2 | 4 | 2 | 0 |  |  |  | 8 | 50 | 8 |
| Cap, veh/h | 0 | 307 | 307 | 679 | 2387 | 0 |  |  |  | 228 | 4 | 217 |
| Arrive On Green | 0.00 | 0.19 | 0.00 | 0.65 | 1.00 | 0.00 |  |  |  | 0.15 | 0.15 | 0.15 |
| Sat Flow, veh/h | 0 | 1583 | 1583 | 1740 | 3632 | 0 |  |  |  | 1567 | 27 | 1495 |
| Grp Volume(v), veh/h | 0 | 225 | 0 | 627 | 445 | 0 |  |  |  | 180 | 0 | 127 |
| Grp Sat Flow(s), veh/h/ln | 0 | 1583 | 1583 | 1740 | 1770 | 0 |  |  |  | 1594 | 0 | 1495 |
| Q Serve(g_s), s | 0.0 | 7.4 | 0.0 | 17.5 | 0.0 | 0.0 |  |  |  | 6.0 | 0.0 | 4.4 |
| Cycle Q Clear(g_c), s | 0.0 | 7.4 | 0.0 | 17.5 | 0.0 | 0.0 |  |  |  | 6.0 | 0.0 | 4.4 |
| Prop In Lane | 0.00 |  | 1.00 | 1.00 |  | 0.00 |  |  |  | 0.98 |  | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 307 | 307 | 679 | 2387 | 0 |  |  |  | 231 | 0 | 217 |
| V/C Ratio(X) | 0.00 | 0.73 | 0.00 | 0.92 | 0.19 | 0.00 |  |  |  | 0.78 | 0.00 | 0.58 |
| Avail Cap(c_a), veh/h | 0 | 371 | 371 | 1413 | 4023 | 0 |  |  |  | 489 | 0 | 459 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.67 | 1.67 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 0.00 | 0.97 | 0.00 | 0.89 | 0.89 | 0.00 |  |  |  | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 21.0 | 0.0 | 8.9 | 0.0 | 0.0 |  |  |  | 22.8 | 0.0 | 22.1 |
| Incr Delay (d2), s/veh | 0.0 | 5.7 | 0.0 | 5.4 | 0.0 | 0.0 |  |  |  | 5.6 | 0.0 | 2.5 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.0 | 3.7 | 0.0 | 8.8 | 0.0 | 0.0 |  |  |  | 3.0 | 0.0 | 1.9 |
| LnGrp Delay(d),s/veh | 0.0 | 26.6 | 0.0 | 14.3 | 0.0 | 0.0 |  |  |  | 28.4 | 0.0 | 24.6 |
| LnGrp LOS |  | C |  | B | A |  |  |  |  | C |  | C |
| Approach Vol, veh/h |  | 225 |  |  | 1072 |  |  |  |  |  | 307 |  |
| Approach Delay, s/veh |  | 26.6 |  |  | 8.4 |  |  |  |  |  | 26.8 |  |
| Approach LOS |  | C |  |  | A |  |  |  |  |  | C |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Assigned Phs | 1 | 2 |  | 4 |  | 6 |  |  |  |  |  |  |
| Phs Duration ( $G+Y+R c$ ), $s$ | 61.2 | 15.8 |  | 13.0 |  | 77.0 |  |  |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ) , s | 5.0 | 5.0 |  | 5.0 |  | 5.0 |  |  |  |  |  |  |
| Max Green Setting (Gmax), s | 45.0 | 13.0 |  | 17.0 |  | 63.0 |  |  |  |  |  |  |
| Max Q Clear Time (g_c+l1), s | 19.5 | 9.4 |  | 8.0 |  | 2.0 |  |  |  |  |  |  |
| Green Ext Time (p_c), s | 2.1 | 1.4 |  | 0.1 |  | 4.6 |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 14.5 |  |  |  |  |  |  |  |  |  |
| HCM 2010 LOS |  |  | B |  |  |  |  |  |  |  |  |  |


|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 147.3 |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 96 | 439 | 170 | 147 | 728 | 11 | 78 | 2 | 52 |
| Conflicting Peds, \#hr | 0 | 0 | 0 | 5 | 0 | 5 | 0 | 0 | 5 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | 200 | - | - | 200 | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 100 | 92 | 100 | 92 | 100 | 100 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 25 | 2 | 20 | 2 | 0 | 25 |
| Mvmt Flow | 104 | 477 | 185 | 147 | 791 | 11 | 85 | 2 | 52 |
| Major/Minor | Major1 |  |  | Major2 |  |  | Minor1 |  |  |
| Conflicting Flow All | 807 | 0 | 0 | 667 | 0 | 0 | 1924 | 1884 | 580 |
| Stage 1 | - | - | - | - | - | - | 783 | 783 |  |
| Stage 2 | - | - | - | - | - | - | 1141 | 1101 |  |
| Critical Hdwy | 4.12 | - | - | 4.35 | - | - | 7.12 | 6.5 | 6.45 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.12 | 5.5 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.12 | 5.5 |  |
| Follow-up Hdwy | 2.218 | - | - | 2.425 | - | - | 3.518 | 4 | 3.525 |
| Pot Cap-1 Maneuver | 818 | - | - | 823 | - | - | $\sim 51$ | 72 | 474 |
| Stage 1 | - | - | - | - | - | - | 387 | 407 | - |
| Stage 2 | - | - | - | - | - | - | 244 | 290 | - |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 818 | - | - | 820 | - | - | $\sim 26$ | 51 | 470 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | $\sim 26$ | 51 |  |
| Stage 1 | - | - | - | - | - | - | 336 | 354 |  |
| Stage 2 | - | - | - | - | - | - | 150 | 237 |  |


| Approach | EB | WB | NB |
| :--- | :--- | :---: | :---: |
| HCM Control Delay, s | 1.4 | 1.6 | $\$ 1278.8$ |
| HCM LOS |  |  | F |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 41 | 818 | - | - | 820 | - | - | 56 |
| HCM Lane V/C Ratio | 3.385 | 0.128 | - | - | 0.179 | - | - | 2.462 |
| HCM Control Delay (s) | $\$ 1278.8$ | 10 | - | - | 10.3 | - | $-\$ 821.8$ |  |
| HCM Lane LOS | F | B | - | - | $B$ | - | - | F |
| HCM 95th \%tile Q(veh) | 15.6 | 0.4 | - | - | 0.7 | - | - | 13.9 |
| Notes |  |  |  |  |  |  |  |  |

$\sim$ : Volume exceeds capacity $\quad \$$ : Delay exceeds $300 \mathrm{~s} \quad+$ : Computation Not Defined $\quad *:$ All major volume in platoon

| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | SBL | SBT | SBR |
| Vol, veh/h | 47 | 5 | 79 |
| Conflicting Peds, \#/hr | 5 | 0 | 0 |
| Sign Control | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | - | - | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 92 |
| Heavy Vehicles, \% | 69 | 100 | 2 |
| Mvmt Flow | 47 | 5 | 86 |
|  |  |  |  |


| Major/Minor | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Conflicting Flow All | 1906 | 1972 | 802 |
| Stage 1 | 1096 | 1096 | - |
| $\quad$ Stage 2 | 810 | 876 | - |
| Critical Hdwy | 7.79 | 7.5 | 6.22 |
| Critical Hdwy Stg 1 | 6.79 | 6.5 | - |
| Critical Hdwy Stg 2 | 6.79 | 6.5 | - |
| Follow-up Hdwy | 4.121 | 4.9 | 3.318 |
| Pot Cap-1 Maneuver | $\sim 35$ | 35 | 384 |
| $\quad$ Stage 1 | 194 | 195 | - |
| $\quad$ Stage 2 | 291 | 259 | - |
| Platoon blocked, \% |  |  |  |
| Mov Cap-1 Maneuver | $\sim 23$ | 25 | 382 |
| Mov Cap-2 Maneuver | $\sim 23$ | 25 | - |
| Stage 1 | 169 | 159 | - |
| Stage 2 | 224 | 225 | - |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | $\$ 821.8$ |
| HCM LOS | F |

## Minor Lane/Major Mvmt

|  | $\rangle$ | $\rightarrow$ | $\nabla$ | $\dagger$ | 4 | 4 | 4 | $\dagger$ | $>$ | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | 1 |  | \% | $\uparrow$ | F | \% | F |  | \% | 1 |  |
| Volume (veh/h) | 5 | 410 | 12 | 149 | 573 | 493 | 5 | 15 | 168 | 329 | 10 | 5 |
| Number | 5 | 2 | 12 | 1 | 6 | 16 | 3 | 8 | 18 | 7 | 4 | 14 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 0.98 | 1.00 |  | 0.98 | 1.00 |  | 0.98 | 1.00 |  | 0.99 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1881 | 1829 | 1900 | 1792 | 1863 | 1881 | 1520 | 1831 | 1900 | 1881 | 1881 | 1900 |
| Adj Flow Rate, veh/h | 5 | 410 | 12 | 149 | 573 | 493 | 5 | 15 | 168 | 329 | 10 | 5 |
| Adj No. of Lanes | 1 | 1 | 0 | 1 | 1 | 1 | 1 | 1 | 0 | 1 | 1 | 0 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh, \% | 1 | 4 | 4 | 6 | 2 | 1 | 25 | 1 | 1 | 1 | 1 | 1 |
| Cap, veh/h | 201 | 804 | 24 | 356 | 848 | 1055 | 8 | 19 | 213 | 381 | 421 | 211 |
| Arrive On Green | 0.45 | 0.45 | 0.45 | 0.45 | 0.45 | 0.45 | 0.01 | 0.15 | 0.15 | 0.21 | 0.36 | 0.36 |
| Sat Flow, veh/h | 532 | 1767 | 52 | 925 | 1863 | 1573 | 1448 | 127 | 1424 | 1792 | 1181 | 591 |
| Grp Volume(v), veh/h | 5 | 0 | 422 | 149 | 573 | 493 | 5 | 0 | 183 | 329 | 0 | 15 |
| Grp Sat Flow(s),veh/h/ln | 532 | 0 | 1819 | 925 | 1863 | 1573 | 1448 | 0 | 1551 | 1792 | 0 | 1772 |
| Q Serve(g_s), s | 0.6 | 0.0 | 13.5 | 11.2 | 19.8 | 12.5 | 0.3 | 0.0 | 9.3 | 14.5 | 0.0 | 0.5 |
| Cycle Q Clear(g_c), s | 20.5 | 0.0 | 13.5 | 24.7 | 19.8 | 12.5 | 0.3 | 0.0 | 9.3 | 14.5 | 0.0 | 0.5 |
| Prop In Lane | 1.00 |  | 0.03 | 1.00 |  | 1.00 | 1.00 |  | 0.92 | 1.00 |  | 0.33 |
| Lane Grp Cap(c), veh/h | 201 | 0 | 828 | 356 | 848 | 1055 | 8 | 0 | 232 | 381 | 0 | 632 |
| V/C Ratio(X) | 0.02 | 0.00 | 0.51 | 0.42 | 0.68 | 0.47 | 0.66 | 0.00 | 0.79 | 0.86 | 0.00 | 0.02 |
| Avail Cap(c_a), veh/h | 316 | 0 | 1220 | 556 | 1250 | 1395 | 71 | 0 | 322 | 721 | 0 | 994 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 25.6 | 0.0 | 15.9 | 24.6 | 17.6 | 6.6 | 40.7 | 0.0 | 33.6 | 31.1 | 0.0 | 17.1 |
| Incr Delay (d2), s/veh | 0.0 | 0.0 | 0.5 | 0.8 | 1.0 | 0.3 | 68.2 | 0.0 | 8.6 | 5.9 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.1 | 0.0 | 6.8 | 2.9 | 10.4 | 5.3 | 0.3 | 0.0 | 4.6 | 7.8 | 0.0 | 0.2 |
| LnGrp Delay(d),s/veh | 25.7 | 0.0 | 16.3 | 25.4 | 18.5 | 6.9 | 108.9 | 0.0 | 42.2 | 37.1 | 0.0 | 17.1 |
| LnGrp LOS | C |  | B | C | B | A | F |  | D | D |  | B |
| Approach Vol, veh/h |  | 427 |  |  | 1215 |  |  | 188 |  |  | 344 |  |
| Approach Delay, s/veh |  | 16.5 |  |  | 14.7 |  |  | 44.0 |  |  | 36.2 |  |
| Approach LOS |  | B |  |  | B |  |  | D |  |  | D |  |


| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


| Intersection Summary |  |
| :--- | :--- |
| HCM 2010 Ctrl Delay | 21.0 |
| HCM 2010 LOS |  |

HCM 2010 LOS

## Notes

User approved pedestrian interval to be less than phase max green.

|  | $\stackrel{ }{ }$ | $\rightarrow$ |  | 7 | 4 | 4 | 4 | $\dagger$ | 7 | + | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ | 「 | * | 个4 |  |  |  |  |  | $\uparrow$ | F |
| Volume (veh/h) | 0 | 211 | 697 | 563 | 1034 | 0 | 0 | 0 | 0 | 229 | 3 | 182 |
| Number | 5 | 2 | 12 | 1 | 6 | 16 |  |  |  | 7 | 4 | 14 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 |  |  |  | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 0 | 1845 | 1863 | 1863 | 1881 | 0 |  |  |  | 1900 | 1828 | 1759 |
| Adj Flow Rate, veh/h | 0 | 211 | 0 | 563 | 1034 | 0 |  |  |  | 229 | 3 | 182 |
| Adj No. of Lanes | 0 | 1 | 1 | 1 | 2 | 0 |  |  |  | 0 | 1 | 1 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh, \% | 0 | 3 | 2 | 2 | 1 | 0 |  |  |  | 8 | 0 | 8 |
| Cap, veh/h | 0 | 400 | 344 | 858 | 2680 | 0 |  |  |  | 261 | 3 | 227 |
| Arrive On Green | 0.00 | 0.22 | 0.00 | 0.97 | 1.00 | 0.00 |  |  |  | 0.15 | 0.15 | 0.15 |
| Sat Flow, veh/h | 0 | 1845 | 1583 | 1774 | 3668 | 0 |  |  |  | 1719 | 23 | 1495 |
| Grp Volume(v), veh/h | 0 | 211 | 0 | 563 | 1034 | 0 |  |  |  | 232 | 0 | 182 |
| Grp Sat Flow(s),veh/h/ln | 0 | 1845 | 1583 | 1774 | 1787 | 0 |  |  |  | 1742 | 0 | 1495 |
| Q Serve(g_s), s | 0.0 | 10.3 | 0.0 | 2.9 | 0.0 | 0.0 |  |  |  | 13.2 | 0.0 | 11.9 |
| Cycle Q Clear(g_c), s | 0.0 | 10.3 | 0.0 | 2.9 | 0.0 | 0.0 |  |  |  | 13.2 | 0.0 | 11.9 |
| Prop In Lane | 0.00 |  | 1.00 | 1.00 |  | 0.00 |  |  |  | 0.99 |  | 1.00 |
| Lane Grp Cap(c), veh/h | 0 | 400 | 344 | 858 | 2680 | 0 |  |  |  | 264 | 0 | 227 |
| V/C Ratio(X) | 0.00 | 0.53 | 0.00 | 0.66 | 0.39 | 0.00 |  |  |  | 0.88 | 0.00 | 0.80 |
| Avail Cap(c_a), veh/h | 0 | 400 | 344 | 858 | 2680 | 0 |  |  |  | 412 | 0 | 354 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 2.00 | 2.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 0.00 | 0.75 | 0.00 | 0.78 | 0.78 | 0.00 |  |  |  | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 0.0 | 35.1 | 0.0 | 0.9 | 0.0 | 0.0 |  |  |  | 42.1 | 0.0 | 41.5 |
| Incr Delay (d2), s/veh | 0.0 | 1.0 | 0.0 | 3.1 | 0.3 | 0.0 |  |  |  | 12.6 | 0.0 | 7.1 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.0 | 5.3 | 0.0 | 1.4 | 0.1 | 0.0 |  |  |  | 7.3 | 0.0 | 5.4 |
| LnGrp Delay(d),s/veh | 0.0 | 36.0 | 0.0 | 4.0 | 0.3 | 0.0 |  |  |  | 54.7 | 0.0 | 48.7 |
| LnGrp LOS |  | D |  | A | A |  |  |  |  | D |  | D |
| Approach Vol, veh/h |  | 211 |  |  | 1597 |  |  |  |  |  | 414 |  |
| Approach Delay, s/veh |  | 36.0 |  |  | 1.6 |  |  |  |  |  | 52.1 |  |
| Approach LOS |  | D |  |  | A |  |  |  |  |  | D |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Assigned Phs | 1 | 2 |  | 4 |  | 6 |  |  |  |  |  |  |
| Phs Duration ( $G+Y+R c$ ), $s$ | 54.0 | 27.0 |  | 20.4 |  | 81.0 |  |  |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ) , s | 5.0 | 5.0 |  | 5.0 |  | 5.0 |  |  |  |  |  |  |
| Max Green Setting (Gmax), s | 49.0 | 22.0 |  | 24.0 |  | 76.0 |  |  |  |  |  |  |
| Max Q Clear Time (g_c+11), s | 4.9 | 12.3 |  | 15.2 |  | 2.0 |  |  |  |  |  |  |
| Green Ext Time (p_c), s | 1.9 | 5.4 |  | 0.1 |  | 11.2 |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 14.3 |  |  |  |  |  |  |  |  |  |
| HCM 2010 LOS |  |  | B |  |  |  |  |  |  |  |  |  |


|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 260.7 |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 91 | 727 | 116 | 101 | 478 | 14 | 215 | 8 | 174 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 5 | 0 | 5 | 0 | 0 | 5 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | 200 | - | - | 200 | - | - | 200 | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 92 | 92 | 92 | 100 | 92 | 100 | 92 | 100 | 100 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 0 | 2 | 17 | 2 | 0 | 50 |
| Mumt Flow | 99 | 790 | 126 | 101 | 520 | 14 | 234 | 8 | 174 |
| Major/Minor | Major1 |  |  | Major2 |  |  | Minor1 |  |  |
| Conflicting Flow All | 539 | 0 | 0 | 921 | 0 | 0 | 1814 | 1797 | 863 |
| Stage 1 | - | - | - | - | - | - | 1056 | 1056 |  |
| Stage 2 | - | - | - | - | - | - | 758 | 741 |  |
| Critical Hdwy | 4.12 | - | - | 4.1 | - | - | 7.12 | 6.5 | 6.7 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.12 | 5.5 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.12 | 5.5 |  |
| Follow-up Hdwy | 2.218 | - | - | 2.2 | - | - | 3.518 | 4 | 3.75 |
| Pot Cap-1 Maneuver | 1029 | - | - | 750 | - | - | $\sim 60$ | 81 | 292 |
| Stage 1 | - | - | - | - | - | - | 272 | 305 |  |
| Stage 2 | - | - | - | - | - | - | 399 | 426 | - |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1029 | - | - | 747 | - | - | $\sim 43$ | 63 | 290 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | $\sim 43$ | 63 |  |
| Stage 1 | - | - | - | - | - | - | 245 | 275 |  |
| Stage 2 | - | - | - | - | - | - | 313 | 367 |  |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0.9 | 1.7 | $\$ 1248.8$ |
| HCM LOS |  |  | F |


| Minor Lane/Major Mvmt | NBLn1 | NBLn2 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| SBLn2 |  |  |  |  |  |  |  |  |  |
| Capacity (veh/h) | 43 | 250 | 1029 | - | - | 747 | - | - | 16 |
| HCM Lane V/C Ratio | 5.435 | 0.728 | 0.096 | - | - | 0.135 | - | - | 2.25 |
| HCM Control Delay (s) | $\$ 2182.2$ | 50.2 | 8.9 | - | - | 10.6 | - | $-\$ 1065.2$ | 19.8 |
| HCM Lane LOS | F | F | A | - | - | B | - | - | F |
| HCM 95th \%tile Q(veh) | 27.1 | 5 | 0.3 | - | - | 0.5 | - | - | 5.1 |

## Notes

~: Volume exceeds capacity $\quad \$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ *: All major volume in platoon

| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | SBL | SBT | SBR |
| Vol, veh/h | 56 | 5 | 40 |
| Conflicting Peds, \#/hr | 5 | 0 | 0 |
| Sign Control | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | 200 | - | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 92 |
| Heavy Vehicles, \% | 0 | 0 | 2 |
| Mvmt Flow | 36 | 5 | 43 |
|  |  |  |  |


| Major/Minor | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Conflicting Flow All | 1881 | 1853 | 532 |
| Stage 1 | 734 | 734 | - |
| Stage 2 | 1147 | 1119 | - |
| Critical Hdwy | 7.1 | 6.5 | 6.22 |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - |
| Follow-up Hdwy | 3.5 | 4 | 3.318 |
| Pot Cap-1 Maneuver | 55 | 75 | 547 |
| $\quad$ Stage 1 | 415 | 429 | - |
| Stage 2 | 244 | 285 | - |
| Platoon blocked, \% | $\sim 16$ | 58 | 545 |
| Mov Cap-1 Maneuver | $\sim 16$ | 58 | - |
| Mov Cap-2 Maneuver | 374 | 369 | - |
| Stage 1 | 85 | 257 | - |
| Stage 2 |  |  |  |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | $\$ 465.3$ |
| HCM LOS | F |

[^7]
## Appendix C 2037 Build Total Intersection Operations Analysis Worksheets



## Notes

User approved pedestrian interval to be less than phase max green.

|  | 4 |  |  | $\checkmark$ | $\leftarrow$ | 4 | 4 | 4 | $p$ | $t$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 个个 | 「 | ${ }^{17}$ | 个4 |  |  |  |  |  | $\uparrow$ | 「 |
| Volume（veh／h） | 0 | 225 | 264 | 627 | 445 | 0 | 0 | 0 | 0 | 177 | 3 | 127 |
| Number | 5 | 2 | 12 | 1 | 6 | 16 |  |  |  | 7 | 4 | 14 |
| Initial $\mathrm{Q}(\mathrm{Qb})$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 |  |  |  | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow，veh／h／ln | 0 | 1583 | 1863 | 1827 | 1863 | 0 |  |  |  | 1900 | 1672 | 1759 |
| Adj Flow Rate，veh／h | 0 | 225 | 0 | 627 | 445 | 0 |  |  |  | 177 | 3 | 127 |
| Adj No．of Lanes | 0 | 2 | 1 | 2 | 2 | 0 |  |  |  | 0 | 1 | 1 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh，\％ | 0 | 20 | 2 | 4 | 2 | 0 |  |  |  | 8 | 50 | 8 |
| Cap，veh／h | 0 | 627 | 330 | 915 | 2130 | 0 |  |  |  | 242 | 4 | 231 |
| Arrive On Green | 0.00 | 0.21 | 0.00 | 0.27 | 0.60 | 0.00 |  |  |  | 0.15 | 0.15 | 0.15 |
| Sat Flow，veh／h | 0 | 3088 | 1583 | 3375 | 3632 | 0 |  |  |  | 1567 | 27 | 1495 |
| Grp Volume（v），veh／h | 0 | 225 | 0 | 627 | 445 | 0 |  |  |  | 180 | 0 | 127 |
| Grp Sat Flow（s），veh／h／ln | 0 | 1504 | 1583 | 1688 | 1770 | 0 |  |  |  | 1594 | 0 | 1495 |
| Q Serve（g＿s），s | 0.0 | 2.6 | 0.0 | 6.8 | 2.3 | 0.0 |  |  |  | 4.4 | 0.0 | 3.2 |
| Cycle Q Clear（g＿c），s | 0.0 | 2.6 | 0.0 | 6.8 | 2.3 | 0.0 |  |  |  | 4.4 | 0.0 | 3.2 |
| Prop In Lane | 0.00 |  | 1.00 | 1.00 |  | 0.00 |  |  |  | 0.98 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 0 | 627 | 330 | 915 | 2130 | 0 |  |  |  | 246 | 0 | 231 |
| V／C Ratio（X） | 0.00 | 0.36 | 0.00 | 0.68 | 0.21 | 0.00 |  |  |  | 0.73 | 0.00 | 0.55 |
| Avail Cap（c＿a），veh／h | 0 | 1615 | 850 | 2801 | 5270 | 0 |  |  |  | 1128 | 0 | 1059 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 0.00 | 0.98 | 0.00 | 0.84 | 0.84 | 0.00 |  |  |  | 1.00 | 0.00 | 1.00 |
| Uniform Delay（d），s／veh | 0.0 | 13.9 | 0.0 | 13.4 | 3.7 | 0.0 |  |  |  | 16.5 | 0.0 | 16.0 |
| Incr Delay（d2），s／veh | 0.0 | 0.3 | 0.0 | 0.8 | 0.0 | 0.0 |  |  |  | 4.2 | 0.0 | 2.0 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.0 | 1.1 | 0.0 | 3.2 | 1.1 | 0.0 |  |  |  | 2.2 | 0.0 | 1.4 |
| LnGrp Delay（d），s／veh | 0.0 | 14.2 | 0.0 | 14.1 | 3.8 | 0.0 |  |  |  | 20.7 | 0.0 | 18.1 |
| LnGrp LOS |  | B |  | B | A |  |  |  |  | C |  | B |
| Approach Vol，veh／h |  | 225 |  |  | 1072 |  |  |  |  |  | 307 |  |
| Approach Delay，s／veh |  | 14.2 |  |  | 9.8 |  |  |  |  |  | 19.6 |  |
| Approach LOS |  | B |  |  | A |  |  |  |  |  | B |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Assigned Phs | 1 | 2 |  | 4 |  | 6 |  |  |  |  |  |  |
| Phs Duration（ $G+Y+R \mathrm{c}$ ），s | 75.1 | 13.5 |  | 11.3 |  | 88.7 |  |  |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），s | 5.0 | 5.0 |  | 5.0 |  | 5.0 |  |  |  |  |  |  |
| Max Green Setting（Gmax），s | 34.0 | 22.0 |  | 29.0 |  | 61.0 |  |  |  |  |  |  |
| Max Q Clear Time（ $\mathrm{g}_{\sim} \mathrm{c}+11$ ），s | 8.8 | 4.6 |  | 6.4 |  | 4.3 |  |  |  |  |  |  |
| Green Ext Time（p＿c），s | 2.3 | 3.9 |  | 0.1 |  | 4.8 |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 12.3 |  |  |  |  |  |  |  |  |  |
| HCM 2010 LOS |  |  | B |  |  |  |  |  |  |  |  |  |


|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


|  | $\rangle$ | $\rightarrow$ | 7 | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\dagger$ | $>$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | 个 ${ }^{\text {P }}$ |  | \% | 个t |  | \% | F |  | ${ }^{7}$ | F |  |
| Volume (veh/h) | 96 | 439 | 170 | 147 | 728 | 11 | 78 | 2 | 52 | 47 | 5 | 79 |
| Number | 5 | 2 | 12 | 1 | 6 | 16 | 3 | 8 | 18 | 7 | 4 | 14 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 0.99 |  | 0.99 | 0.99 |  | 0.99 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1900 | 1520 | 1858 | 1900 | 1863 | 1531 | 1900 | 1727 | 1769 | 1900 |
| Adj Flow Rate, veh/h | 104 | 477 | 0 | 147 | 791 | 11 | 85 | 2 | 52 | 47 | 5 | 86 |
| Adj No. of Lanes | 1 | 2 | 0 | 1 | 2 | 0 | 1 | 1 | 0 | 1 | 1 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 1.00 | 0.92 | 1.00 | 0.92 | 1.00 | 1.00 | 1.00 | 1.00 | 0.92 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 25 | 2 | 2 | 2 | 0 | 0 | 10 | 100 | 100 |
| Cap, veh/h | 501 | 2068 | 0 | 619 | 2157 | 30 | 233 | 8 | 206 | 248 | 14 | 234 |
| Arrive On Green | 0.09 | 1.00 | 0.00 | 0.07 | 0.61 | 0.61 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 | 0.17 |
| Sat Flow, veh/h | 1774 | 3632 | 0 | 1448 | 3565 | 50 | 1291 | 48 | 1249 | 1237 | 83 | 1421 |
| Grp Volume(v), veh/h | 104 | 477 | 0 | 147 | 392 | 410 | 85 | 0 | 54 | 47 | 0 | 91 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1770 | 0 | 1448 | 1765 | 1849 | 1291 | 0 | 1297 | 1237 | 0 | 1503 |
| Q Serve(g_s), s | 1.8 | 0.0 | 0.0 | 3.2 | 9.1 | 9.1 | 5.1 | 0.0 | 2.9 | 2.8 | 0.0 | 4.4 |
| Cycle Q Clear(g_c), s | 1.8 | 0.0 | 0.0 | 3.2 | 9.1 | 9.1 | 9.4 | 0.0 | 2.9 | 5.7 | 0.0 | 4.4 |
| Prop In Lane | 1.00 |  | 0.00 | 1.00 |  | 0.03 | 1.00 |  | 0.96 | 1.00 |  | 0.95 |
| Lane Grp Cap(c), veh/h | 501 | 2068 | 0 | 619 | 1068 | 1119 | 233 | 0 | 214 | 248 | 0 | 248 |
| V/C Ratio(X) | 0.21 | 0.23 | 0.00 | 0.24 | 0.37 | 0.37 | 0.37 | 0.00 | 0.25 | 0.19 | 0.00 | 0.37 |
| Avail Cap(c_a), veh/h | 663 | 2068 | 0 | 882 | 1068 | 1119 | 418 | 0 | 401 | 426 | 0 | 464 |
| HCM Platoon Ratio | 2.00 | 2.00 | 2.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 5.6 | 0.0 | 0.0 | 5.5 | 8.1 | 8.1 | 34.2 | 0.0 | 29.5 | 31.9 | 0.0 | 30.0 |
| Incr Delay (d2), s/veh | 0.2 | 0.3 | 0.0 | 0.2 | 1.0 | 0.9 | 1.0 | 0.0 | 0.6 | 0.4 | 0.0 | 0.9 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.9 | 0.1 | 0.0 | 1.3 | 4.6 | 4.8 | 1.9 | 0.0 | 1.1 | 1.0 | 0.0 | 1.9 |
| LnGrp Delay(d),s/veh | 5.8 | 0.3 | 0.0 | 5.7 | 9.1 | 9.0 | 35.2 | 0.0 | 30.1 | 32.3 | 0.0 | 31.0 |
| LnGrp LOS | A | A |  | A | A | A | D |  | C | C |  | C |
| Approach Vol, veh/h |  | 581 |  |  | 949 |  |  | 139 |  |  | 138 |  |
| Approach Delay, s/veh |  | 1.3 |  |  | 8.5 |  |  | 33.2 |  |  | 31.4 |  |
| Approach LOS |  | A |  |  | A |  |  | C |  |  | C |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), s | 10.3 | 71.3 |  | 18.4 | 8.6 | 73.0 |  | 18.4 |  |  |  |  |
| Change Period (Y+Rc), s | 5.0 | 5.0 |  | 5.0 | 5.0 | 5.0 |  | 5.0 |  |  |  |  |
| Max Green Setting (Gmax), s | 20.0 | 40.0 |  | 25.0 | 11.0 | 49.0 |  | 25.0 |  |  |  |  |
| Max Q Clear Time (g_c+l1), s | 5.2 | 2.0 |  | 7.7 | 3.8 | 11.1 |  | 11.4 |  |  |  |  |
| Green Ext Time (p_c), s | 0.3 | 9.5 |  | 1.1 | 0.1 | 9.5 |  | 1.0 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 9.8 |  |  |  |  |  |  |  |  |  |
| HCM 2010 LOS |  |  | A |  |  |  |  |  |  |  |  |  |

Intersection: 102: NW 31st Ave/East Access \& NW 319th St

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | T | TR | L | T | TR | L | TR | L | TR |
| Maximum Queue (ft) | 33 | 83 | 120 | 161 | 95 | 138 | 33 | 102 | 111 | 36 |
| Average Queue (ft) | 4 | 36 | 48 | 75 | 21 | 57 | 4 | 48 | 52 | 9 |
| 95th Queue (ft) | 21 | 74 | 93 | 132 | 64 | 107 | 20 | 78 | 95 | 32 |
| Link Distance (ft) |  | 649 | 649 |  | 526 | 526 |  | 1509 |  | 543 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  | 375 |  |  | 300 |  | 300 |  |
| Storage Bay Dist (ft) | 300 |  |  |  |  |  |  |  |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |

Intersection: 103: I-5 SB On Ramp/l-5 SB Off Ramp \& NW 319th St/NW La Center Rd

| Movement | EB | EB | WB | WB | WB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | T | L | L | T | T | LT | R |
| Maximum Queue (ft) | 218 | 168 | 183 | 204 | 127 | 136 | 244 | 91 |
| Average Queue (ft) | 113 | 72 | 33 | 57 | 43 | 52 | 129 | 38 |
| 95th Queue (ft) | 192 | 138 | 106 | 143 | 102 | 109 | 210 | 73 |
| Link Distance (ft) | 526 | 526 |  |  | 503 | 503 | 650 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  | 400 |
| Storage Bay Dist (ft) |  |  | 225 | 225 |  |  |  |  |
| Storage Blk Time (\%) |  |  | 0 | 0 |  |  |  |  |
| Queuing Penalty (veh) |  |  | 0 | 0 |  |  |  |  |

Intersection: 104: I-5 NB Off Ramp/l-5 NB On Ramp \& NW La Center Rd

| Movement | EB | EB | EB | EB | WB | WB | NB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | L | T | T | T | TR | L | L | TR |
| Maximum Queue (ft) | 122 | 140 | 89 | 107 | 204 | 190 | 167 | 201 | 203 |
| Average Queue (ft) | 30 | 54 | 26 | 34 | 157 | 68 | 81 | 120 | 89 |
| 95th Queue (ft) | 86 | 108 | 68 | 88 | 231 | 136 | 150 | 181 | 159 |
| Link Distance (ft) |  |  | 503 | 503 | 194 | 194 |  | 800 | 800 |
| Upstream Blk Time (\%) |  |  |  |  | 4 | 0 |  |  |  |
| Queuing Penalty (veh) |  |  |  |  | 17 | 0 |  |  |  |
| Storage Bay Dist (ft) | 175 | 175 |  |  |  |  | 350 |  |  |
| Storage Blk Time (\%) | 0 | 0 |  |  |  |  |  |  |  |

Intersection: 105: NW Paradise Park Rd \& NW La Center Rd

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | T | TR | L | T | TR | L | TR | L | TR |
| Maximum Queue (ft) | 71 | 144 | 166 | 137 | 163 | 146 | 124 | 125 | 93 | 90 |
| Average Queue (ft) | 35 | 29 | 67 | 58 | 63 | 46 | 53 | 35 | 40 | 37 |
| 95th Queue (ft) | 63 | 88 | 133 | 113 | 132 | 112 | 99 | 84 | 81 | 74 |
| Link Distance (ft) |  | 270 | 270 |  | 2579 | 2579 |  | 1296 |  | 965 |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  | 200 |  |  | 100 |  | 150 |  |
| Storage Bay Dist (ft) | 200 |  |  |  | 0 |  | 2 | 0 |  |  |
| Storage Blk Time (\%) |  | 0 |  |  | 0 |  | 1 | 0 |  |  |
| Queuing Penalty (veh) |  | 0 |  |  |  |  |  |  |  |  |

## Zone Summary

[^8]|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |

Intersection Summary
HCM 2010 Ctrl Delay
HCM 2010 LOS

## Notes

User approved pedestrian interval to be less than phase max green.

|  | 4 |  |  | $\checkmark$ | $\leftarrow$ | 4 | 4 | 4 | $p$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 个个 | 「 | ${ }^{17}$ | 个4 |  |  |  |  |  | $\uparrow$ | 「 |
| Volume（veh／h） | 0 | 211 | 697 | 563 | 1034 | 0 | 0 | 0 | 0 | 229 | 3 | 182 |
| Number | 5 | 2 | 12 | 1 | 6 | 16 |  |  |  | 7 | 4 | 14 |
| Initial $\mathrm{Q}(\mathrm{Qb})$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 |  |  |  | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow，veh／h／ln | 0 | 1845 | 1863 | 1863 | 1881 | 0 |  |  |  | 1900 | 1828 | 1759 |
| Adj Flow Rate，veh／h | 0 | 211 | 0 | 563 | 1034 | 0 |  |  |  | 229 | 3 | 182 |
| Adj No．of Lanes | 0 | 2 | 1 | 2 | 2 | 0 |  |  |  | 0 | 1 | 1 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh，\％ | 0 | 3 | 2 | 2 | 1 | 0 |  |  |  | 8 | 0 | 8 |
| Cap，veh／h | 0 | 816 | 369 | 1567 | 2649 | 0 |  |  |  | 263 | 3 | 229 |
| Arrive On Green | 0.00 | 0.39 | 0.00 | 0.46 | 0.74 | 0.00 |  |  |  | 0.15 | 0.15 | 0.15 |
| Sat Flow，veh／h | 0 | 3597 | 1583 | 3442 | 3668 | 0 |  |  |  | 1719 | 23 | 1495 |
| Grp Volume（v），veh／h | 0 | 211 | 0 | 563 | 1034 | 0 |  |  |  | 232 | 0 | 182 |
| Grp Sat Flow（s），veh／h／ln | 0 | 1752 | 1583 | 1721 | 1787 | 0 |  |  |  | 1742 | 0 | 1495 |
| Q Serve（g＿s），s | 0.0 | 3.9 | 0.0 | 10.1 | 10.0 | 0.0 |  |  |  | 12.3 | 0.0 | 11.1 |
| Cycle Q Clear（g＿c），s | 0.0 | 3.9 | 0.0 | 10.1 | 10.0 | 0.0 |  |  |  | 12.3 | 0.0 | 11.1 |
| Prop In Lane | 0.00 |  | 1.00 | 1.00 |  | 0.00 |  |  |  | 0.99 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 0 | 816 | 369 | 1567 | 2649 | 0 |  |  |  | 267 | 0 | 229 |
| V／C Ratio（X） | 0.00 | 0.26 | 0.00 | 0.36 | 0.39 | 0.00 |  |  |  | 0.87 | 0.00 | 0.80 |
| Avail Cap（c＿a），veh／h | 0 | 816 | 369 | 1567 | 2649 | 0 |  |  |  | 738 | 0 | 633 |
| HCM Platoon Ratio | 1.00 | 1.67 | 1.67 | 1.00 | 1.00 | 1.00 |  |  |  | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 0.00 | 0.80 | 0.00 | 0.67 | 0.67 | 0.00 |  |  |  | 1.00 | 0.00 | 1.00 |
| Uniform Delay（d），s／veh | 0.0 | 23.3 | 0.0 | 16.8 | 4.5 | 0.0 |  |  |  | 39.1 | 0.0 | 38.6 |
| Incr Delay（d2），s／veh | 0.0 | 0.6 | 0.0 | 0.4 | 0.3 | 0.0 |  |  |  | 8.5 | 0.0 | 6.2 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.0 | 1.9 | 0.0 | 4.9 | 5.0 | 0.0 |  |  |  | 6.6 | 0.0 | 4.9 |
| LnGrp Delay（d），s／veh | 0.0 | 23.9 | 0.0 | 17.2 | 4.7 | 0.0 |  |  |  | 47.6 | 0.0 | 44.7 |
| LnGrp LOS |  | C |  | B | A |  |  |  |  | D |  | D |
| Approach Vol，veh／h |  | 211 |  |  | 1597 |  |  |  |  |  | 414 |  |
| Approach Delay，s／veh |  | 23.9 |  |  | 9.1 |  |  |  |  |  | 46.3 |  |
| Approach LOS |  | C |  |  | A |  |  |  |  |  | D |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Assigned Phs | 1 | 2 |  | 4 |  | 6 |  |  |  |  |  |  |
| Phs Duration（ $G+Y+R \mathrm{c}$ ），s | 48.0 | 52.5 |  | 19.5 |  | 100.5 |  |  |  |  |  |  |
| Change Period（ $\mathrm{Y}+\mathrm{Rc}$ ），s | 5.0 | 5.0 |  | 5.0 |  | 5.0 |  |  |  |  |  |  |
| Max Green Setting（Gmax），s | 43.0 | 22.0 |  | 40.0 |  | 70.0 |  |  |  |  |  |  |
| Max Q Clear Time（ $\mathrm{g}_{\sim} \mathrm{c}+11$ ），s | 12.1 | 5.9 |  | 14.3 |  | 12.0 |  |  |  |  |  |  |
| Green Ext Time（p＿c），s | 2.1 | 7.5 |  | 0.2 |  | 11.2 |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 17.5 |  |  |  |  |  |  |  |  |  |
| HCM 2010 LOS |  |  | B |  |  |  |  |  |  |  |  |  |


|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |


|  | $\rangle$ | $\rightarrow$ | 7 | 7 | 4 | 4 | 4 | $\dagger$ | $\pm$ | * | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | 蚛 |  | \% | 个 ${ }^{\text {¢ }}$ |  | * | $\stackrel{1}{ }$ |  | \% | F |  |
| Volume (veh/h) | 91 | 727 | 116 | 101 | 478 | 14 | 215 | 8 | 174 | 36 | 5 | 40 |
| Number | 5 | 2 | 12 | 1 | 6 | 16 | 3 | 8 | 18 | 7 | 4 | 14 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 0.99 | 1.00 |  | 0.99 | 1.00 |  | 0.99 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1863 | 1863 | 1900 | 1900 | 1856 | 1900 | 1863 | 1864 | 1900 | 1900 | 1867 | 1900 |
| Adj Flow Rate, veh/h | 99 | 790 | 0 | 101 | 520 | 14 | 234 | 8 | 174 | 36 | 5 | 43 |
| Adj No. of Lanes | 1 | 2 | 0 | 1 | 2 | 0 | 1 | 1 | 0 | 1 | 1 | 0 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 1.00 | 0.92 | 1.00 | 0.92 | 1.00 | 1.00 | 1.00 | 1.00 | 0.92 |
| Percent Heavy Veh, \% | 2 | 2 | 2 | 0 | 2 | 2 | 2 | 0 | 0 | 0 | 0 | 0 |
| Cap, veh/h | 488 | 1272 | 0 | 378 | 1334 | 36 | 487 | 19 | 419 | 368 | 46 | 397 |
| Arrive On Green | 0.06 | 0.36 | 0.00 | 0.06 | 0.38 | 0.38 | 0.28 | 0.28 | 0.28 | 0.28 | 0.28 | 0.28 |
| Sat Flow, veh/h | 1774 | 3632 | 0 | 1810 | 3507 | 94 | 1345 | 70 | 1517 | 1217 | 167 | 1437 |
| Grp Volume(v), veh/h | 99 | 790 | 0 | 101 | 261 | 273 | 234 | 0 | 182 | 36 | 0 | 48 |
| Grp Sat Flow(s),veh/h/ln | 1774 | 1770 | 0 | 1810 | 1763 | 1838 | 1345 | 0 | 1587 | 1217 | 0 | 1604 |
| Q Serve(g_s), s | 1.6 | 9.1 | 0.0 | 0.0 | 5.3 | 5.3 | 7.8 | 0.0 | 4.6 | 1.2 | 0.0 | 1.1 |
| Cycle Q Clear(g_c), s | 1.6 | 9.1 | 0.0 | 0.0 | 5.3 | 5.3 | 8.9 | 0.0 | 4.6 | 5.9 | 0.0 | 1.1 |
| Prop In Lane | 1.00 |  | 0.00 | 1.00 |  | 0.05 | 1.00 |  | 0.96 | 1.00 |  | 0.90 |
| Lane Grp Cap(c), veh/h | 488 | 1272 | 0 | 378 | 670 | 699 | 487 | 0 | 438 | 368 | 0 | 443 |
| V/C Ratio(X) | 0.20 | 0.62 | 0.00 | 0.27 | 0.39 | 0.39 | 0.48 | 0.00 | 0.42 | 0.10 | 0.00 | 0.11 |
| Avail Cap(c_a), veh/h | 669 | 3869 | 0 | 598 | 1999 | 2084 | 1260 | 0 | 1349 | 1066 | 0 | 1364 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 8.5 | 13.0 | 0.0 | 16.9 | 11.1 | 11.1 | 16.6 | 0.0 | 14.6 | 17.0 | 0.0 | 13.3 |
| Incr Delay (d2), s/veh | 0.2 | 0.5 | 0.0 | 0.4 | 0.4 | 0.4 | 0.7 | 0.0 | 0.6 | 0.1 | 0.0 | 0.1 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.8 | 4.5 | 0.0 | 1.3 | 2.6 | 2.7 | 3.0 | 0.0 | 2.1 | 0.4 | 0.0 | 0.5 |
| LnGrp Delay(d),s/veh | 8.7 | 13.5 | 0.0 | 17.2 | 11.5 | 11.5 | 17.4 | 0.0 | 15.2 | 17.1 | 0.0 | 13.4 |
| LnGrp LOS | A | B |  | B | B | B | B |  | B | B |  | B |
| Approach Vol, veh/h |  | 889 |  |  | 635 |  |  | 416 |  |  | 84 |  |
| Approach Delay, s/veh |  | 13.0 |  |  | 12.4 |  |  | 16.4 |  |  | 15.0 |  |
| Approach LOS |  | B |  |  | B |  |  | B |  |  | B |  |


| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Assigned Phs | 1 | 2 | 4 | 5 | 6 | 8 |  |
| Phs Duration (G+Y+Rc), s | 8.0 | 22.8 | 18.6 | 7.0 | 23.8 | 8 |  |
| Change Period (Y+Rc), s | 5.0 | ${ }^{2} 5$ | 5.0 | 4.0 | 5.0 | 18.6 |  |
| Max Green Setting (Gmax), s | 9.0 | ${ }^{*} 54$ | 42.0 | 8.0 | 56.0 | 5.0 |  |
| Max Q Clear Time (g_c+11), s | 2.0 | 11.1 | 7.9 | 3.6 | 7.3 | 42.0 |  |
| Green Ext Time (p_c), s | 1.8 | 6.7 | 2.3 | 0.1 | 3.2 | 10.9 |  |


| Intersection Summary |  |
| :--- | ---: |
| HCM 2010 Ctrl Delay | 13.6 |
| HCM 2010 LOS | $B$ |

## Notes

* HCM 2010 computational engine requires equal clearance times for the phases crossing the barrier.

Intersection: 102: NW 31st Ave/East Access \& NW 319th St

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | T | TR | L | T | TR | L | TR | L | TR |
| Maximum Queue (ft) | 34 | 172 | 301 | 190 | 298 | 385 | 47 | 206 | 384 | 43 |
| Average Queue (ft) | 3 | 67 | 181 | 109 | 105 | 175 | 4 | 86 | 220 | 11 |
| 95th Queue (ft) | 18 | 137 | 283 | 174 | 215 | 316 | 23 | 169 | 355 | 35 |
| Link Distance (ft) |  | 945 | 945 |  | 526 | 526 |  | 1509 |  | 789 |
| Upstream Blk Time (\%) |  |  |  |  |  | 0 |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  | 0 |  |  | 400 |  |
| Storage Bay Dist (ft) | 300 |  |  | 375 |  |  | 300 | 0 | 0 |  |
| Storage Blk Time (\%) |  |  |  |  | 0 |  |  | 0 | 0 |  |
| Queuing Penalty (veh) |  |  |  |  | 0 |  |  |  | 0 |  |

Intersection: 103: I-5 SB On Ramp/l-5 SB Off Ramp \& NW 319th St/NW La Center Rd

| Movement | EB | EB | WB | WB | WB | WB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | T | T | L | L | T | T | LT | R |
| Maximum Queue (ft) | 208 | 114 | 106 | 120 | 182 | 195 | 290 | 174 |
| Average Queue (ft) | 91 | 41 | 5 | 14 | 80 | 112 | 156 | 77 |
| 95th Queue (ft) | 165 | 93 | 47 | 67 | 152 | 179 | 252 | 141 |
| Link Distance (ft) | 526 | 526 |  |  | 503 | 503 | 650 |  |
| Upstream Blk Time (\%) |  |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  |  |  |  |  |  |  | 400 |
| Storage Bay Dist (ft) |  |  | 225 | 225 |  |  |  |  |
| Storage Blk Time (\%) |  |  |  | 0 | 0 |  |  |  |
| Queuing Penalty (veh) |  |  |  | 0 | 0 |  |  |  |

Intersection: 104: I-5 NB Off Ramp/l-5 NB On Ramp \& NW La Center Rd

| Movement | EB | EB | EB | EB | WB | WB | NB | NB | NB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | L | T | T | T | TR | L | L | TR |
| Maximum Queue (ft) | 69 | 102 | 76 | 97 | 211 | 206 | 389 | 522 | 415 |
| Average Queue (ft) | 31 | 59 | 33 | 38 | 203 | 131 | 225 | 276 | 155 |
| 95th Queue (ft) | 71 | 92 | 73 | 81 | 209 | 229 | 342 | 383 | 255 |
| Link Distance (ft) |  |  | 503 | 503 | 198 | 198 |  | 985 | 985 |
| Upstream Blk Time (\%) |  |  |  |  | 37 | 4 |  | 0 | 0 |
| Queuing Penalty (veh) |  |  |  |  | 168 | 18 |  | 0 | 0 |
| Storage Bay Dist (ft) | 175 | 175 |  |  |  |  | 350 |  |  |
| Storage Blk Time (\%) |  |  |  |  |  |  | 0 | 1 |  |
| Queuing Penalty (veh) |  |  |  |  |  |  | 1 | 7 |  |

Intersection: 105: NW Paradise Park Rd \& NW La Center Rd

| Movement | EB | EB | EB | WB | WB | WB | NB | NB | SB | SB |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Directions Served | L | T | TR | L | T | TR | L | TR | L | TR |
| Maximum Queue (ft) | 88 | 220 | 250 | 108 | 190 | 170 | 175 | 120 | 61 | 45 |
| Average Queue (ft) | 36 | 87 | 113 | 43 | 69 | 47 | 92 | 49 | 23 | 19 |
| 95th Queue (ft) | 67 | 166 | 193 | 84 | 148 | 112 | 156 | 95 | 55 | 43 |
| Link Distance (ft) |  | 287 | 287 |  | 2579 | 2579 |  | 1296 |  | 965 |
| Upstream Blk Time (\%) |  | 0 | 0 |  |  |  |  |  |  |  |
| Queuing Penalty (veh) |  | 0 | 1 |  |  |  | 400 |  | 400 |  |
| Storage Bay Dist (ft) | 200 |  |  | 400 |  |  |  |  |  |  |
| Storage Blk Time (\%) |  | 0 |  |  |  |  |  |  |  |  |

## Zone Summary

[^9]
## Appendix G Single-Line Sketches of Interchange Concept Alternatives












## Appendix H Detailed Interchange Design Concept Review

## APPENDIX H: DETAILED CONCEPT REVIEW

## Concept 1 - Signalized Diamond Interchange

Transportation Operations (+1): the existing interchange can accommodate projected traffic volumes by widening the existing bridge structure and adding additional lanes at the ramp terminals.

Land Use (+1): Right-of-way impacts would be minimal with this concept, and existing businesses/land uses within the vicinity of the interchange could be maintained.

Multimodal Accessibility (+1): bike lanes and sidewalks can be provided by improving the existing interchange. Traffic signals at the ramp terminals control high-speed movements from the freeway, helping protect bicyclists and pedestrians.

Cost (+2): improvement costs to the existing interchange would likely be to the lower end compared to the other concepts.

Environmental Impact (+1): the environmental impact would be minimized by not significantly expanding the footprint of the interchange or altering the freeway ramps.

Constructability (+1): construction of this improvement could be done in phases and would have minimal impacts to adjacent land uses and traffic operations during construction. This improvement requires minimal alternations to the existing freeway ramps.

Accessibility \& Connectivity (0): this concept would not inhibit local connectivity. However, accommodating some existing private property accesses along NW La Center Road that would be located within the intersection influence area may be challenging.

## Concept 2 - Roundabout Diamond Interchange

Transportation Operations (+2): the existing interchange can accommodate projected traffic volumes by widening the existing bridge structure and adding additional lanes at the ramp terminals. Using roundabouts at the ramp terminals improves operations and requires fewer lanes across the bridge structure.

Land Use (+1): Right-of-way impacts would be minimal with this concept, and existing businesses/land uses within the vicinity of the interchange could be maintained.

Multimodal Accessibility (+1): bike lanes and sidewalks can be provided by improving the existing interchange. Roundabouts at the ramp terminals control high-speed movements from the freeway, helping protect bicyclists and pedestrians.

Cost (+2): improvement costs to the existing interchange would likely be to the lower end compared to the other concepts.

Environmental Impact (+1): the environmental impact would be minimized by not significantly expanding the footprint of the interchange or altering the freeway ramps.

Constructability (+1): construction of this improvement could be done in phases and would have minimal impacts to adjacent land uses during construction. Maintaining traffic operations during construction would be more difficult than under the signalized concepts. This improvement requires minimal alternations to the existing freeway ramps.

Accessibility \& Connectivity (0): this concept would not inhibit local connectivity or access to any property. Accesses between roundabouts can be limited to right-in/right-out, because left-turns can be accommodated at the roundabouts.

## CoNcept 3 - Partial Cloverleaf Interchange (Southbound parclo A)

Transportation Operations (+2): a partial cloverleaf interchange would provide additional capacity for the southbound on-ramp during the AM peak.

Land Use (-1): the interchange configuration would have a large footprint to the northwest of the interchange.

Multimodal Accessibility (0): the movements with loop ramp would be potentially high speed, causing potential conflicts for bicycle and pedestrian users. Running the right-turns associated with the loop ramp through a signal would create a controlled environment. The south side of the overpass will have fewer conflicts associated with bicycles and pedestrians through the interchange ramp terminal area.

Cost (-1): construction of this interchange would require reconstruction of the overpass and southbound onand off-ramps.

Environmental Impact (-1): environmental impacts would be significant with the expansion of the footprint of the interchange, particularly on the north side of the interchange.

Constructability (0): construction of this improvement could be done in phases, but could require significant disruption of existing traffic operations, particularly for the impacted ramps.

Accessibility \& Connectivity (0): this concept would not inhibit local connectivity or access to any property. However, accommodating some existing private property accesses along NW La Center Road that would be located within the intersection influence area may be challenging.

## Concept 4 - Partial Cloverleaf Interchange (Northbound parclo B)

Transportation Operations (+2): a partial cloverleaf interchange would provide additional capacity for the northbound off-ramp during the PM peak.

Land Use (-1): the interchange configuration would have a large footprint to the northeast of the interchange, which would impact the existing gas station.

Multimodal Accessibility (0): the movements with loop ramp would be potentially high speed, causing significant conflicts for bicycle and pedestrian users. Running the right-turns associated with the loop ramp through a signal would create a controlled environment. The south side of the overpass will have fewer conflicts associated with bicycles and pedestrians through the interchange ramp terminal area.

Cost (-1): construction of this interchange would require reconstruction of the overpass and northbound onand off-ramps.

Environmental Impact (-1): environmental impacts would be significant with the expansion of the footprint of the interchange, particularly on the north side of the interchange.

Constructability ( $\mathbf{0}$ ): construction of this improvement could be done in phases, but could require significant disruption of existing traffic operations, particularly for the impacted ramps.

Accessibility \& Connectivity (0): this concept would impact property and access to the existing gas station northeast of the interchange. Otherwise, it would not inhibit local connectivity. However, accommodating some existing private property accesses along NW La Center Road that would be located within the intersection influence area may be challenging.

## Concept 5 - Partial Cloverleaf Interchange (Northbound parclo B and " $A$ " Ramp)

Transportation Operations (+2): a partial cloverleaf interchange would provide additional capacity for the northbound off-ramp during the PM peak.

Land Use (-2): the interchange configuration would have a large footprint to the northeast of the interchange, which would impact the existing gas station.

Multimodal Accessibility (0): the movements with loop ramp would be potentially high speed, causing significant conflicts for bicycle and pedestrian users. Running the right-turns associated with the loop ramp through a signal would create a controlled environment. However, the south side of the overpass will have fewer conflicts associated with bicycles and pedestrians through the interchange ramp terminal area.

Cost (-1): construction of this interchange would require reconstruction of the overpass and northbound onand off-ramps.

Environmental Impact (-1): environmental impacts would be significant with the expansion of the footprint of the interchange, particularly on the north side of the interchange.

Constructability (0): construction of this improvement could be done in phases, but could require significant disruption of existing traffic operations, particularly for the impacted ramps.

Accessibility \& Connectivity ( $\mathbf{- 1}$ ): this concept would impact property and access to the existing gas station northeast of the interchange. Otherwise, it would not inhibit local connectivity.

## Concept 6 - Partial Cloverleaf Interchange (Southbound Parclo A, Northbound Parclo B, and "A" Ramp)

Transportation Operations (+2): a partial cloverleaf interchange would provide additional capacity for the southbound on-ramp during the AM peak and northbound off-ramp during the PM peak.

Land Use (-2): the interchange configuration would have a large footprint to the north of the interchange, which would impact the existing gas station.

Multimodal Accessibility (-1): the movements with loop ramps would be potentially high speed, causing significant conflicts for bicycle and pedestrian users. Running the right-turns associated with the loop ramp through a signal would create a controlled environment. However, the south side of the overpass will have fewer conflicts associated with bicycles and pedestrians through the interchange ramp terminal area.

Cost (-2): construction of this interchange would require reconstruction of the overpass and all ramps.
Environmental Impact (-2): environmental impacts would be significant with the expansion of the footprint of the interchange, particularly on the north side of the interchange on both sides of I-5.

Constructability (-1): construction of this improvement could be done in phases, but could require significant disruption of existing traffic operations, particularly for the impacts associated with two new loop ramps.

Accessibility \& Connectivity (-1): this concept would impact property and access to the existing gas station northeast of the interchange. Otherwise, it would not inhibit local connectivity.

## Concept 7 - Single-Point Urban Interchange (SPUI) Configuration

Transportation Operations (+2): a SPUI configuration would provide significant additional capacity for the interchange.

Land Use (+2): while the bridge would have a large footprint, impacts to the quadrants of the interchange and existing businesses or land uses are minimal.

Multimodal Accessibility (-2): bicyclists and pedestrians cannot easily be accommodated with a SPUI configuration and will face significant challenges navigating the interchange due to exposure associated with the large intersection footprint.

Cost (-1): construction of this interchange would require significant reconstruction of a large overpass structure and approach realignments.

Environmental Impact (+1): environmental impacts would be minimal, as the interchange does not require significant changes to the freeway ramps.

Constructability (-1): construction of this improvement has challenges constructing it in phases and would require significant disruption of existing traffic operations.

Accessibility \& Connectivity (+1): this concept would not inhibit local connectivity or access to any property.

## Concept 8 - Diverging Diamond Interchange (DDI)

Transportation Operations (+2): a diverging diamond would provide significant additional capacity for the interchange.

Land Use (+1): while the bridge would have to be widened, the right-of-way impacts would not be significant with this concept.

Multimodal Accessibility (-1): bicyclists and pedestrians may be unfamiliar with the interchange form.
Cost (+2): construction of this interchange would likely be to the lower end compared to the other concepts, as it only requires minimal alternations to the existing freeway ramps.

Environmental Impact (+1): environmental impact would be minimized by not significantly expanding the footprint of the interchange or the freeway ramps.

Constructability (+1): construction of this improvement could be done in phases, but would require longer disruption of existing traffic operations. This improvement requires minimal alternations to the existing freeway ramps.

Accessibility \& Connectivity (0): this concept would not inhibit local connectivity or access to any property, but would be unfamiliar to users. Additionally, exiting freeway traffic cannot immediately re-enter through the ramp terminals.

## Concept 9 - Diamond Interchange with Additional Overcrossing

Transportation Operations (+1): the existing interchange can accommodate projected traffic volumes by widening the existing bridge structure and adding additional lanes at the ramp terminals. The additional overcrossing south of the interchange provides capacity for local trips, but these are relatively low volume.

Land Use (-2): Right-of-way impacts directly adjacent to the interchange would be minimal with this concept. However, the additional overcrossing would significantly impact the properties further southeast of the interchange.

Multimodal Accessibility (+2): bike lanes and sidewalks can be provided by improving the existing interchange and on the additional overcrossing.

Cost (-2): adding an additional overcrossing and improving the existing interchange would have significant costs.

Environmental Impact (-2): the environmental impacts associated with the additional overcrossing would be significant.

Constructability (+1): construction of this improvement could be done in phases and would have minimal impacts to adjacent land uses and traffic operations during construction. This improvement requires minimal alternations to the existing freeway ramps.

Accessibility \& Connectivity (0): this concept would not inhibit local connectivity and is consistent with the City of La Center's plans (developed as part of La Center Junction Subarea Plan).

## Concept 10 - Partial Cloverleaf Interchange (Parclo A)

Transportation Operations (+2): a partial cloverleaf interchange would provide additional capacity for the southbound on-ramp during the AM peak, but the northbound loop on-ramp does not serve a dominant movement.

Land Use (-2): the interchange configuration would have a large footprint to the northwest and southeast quadrants of the interchange.

Multimodal Accessibility (-2): the movements with loop ramps would be potentially high speed, causing significant conflicts for bicycle and pedestrian users. Running the right-turns associated with the loop ramp through a signal would create a controlled environment.

Cost (-2): construction of this interchange would require reconstruction of the overpass and all ramps.
Environmental Impact (-2): environmental impacts would be significant with the expansion of the footprint of the interchange and movement of the ramps.

Constructability (-1): construction of this improvement could be done in phases, but could require significant disruption of existing traffic operations, particularly for the impacts associated with two new loop ramps.

Accessibility \& Connectivity (0): this concept would not inhibit local connectivity or access to any property. However, accommodating some existing private property accesses along NW La Center Road that would be located within the intersection influence area may be challenging.

## Appendix I Single-Line Sketches of Frontage Road Options



CARLSON/ FUDGE: OPTION A


CARLSON/ BURK/ LANDON/ FUDGE: OPTION B


CARLSON/ LA CENTER ROAD UNDERPASS: OPTION C


LANDON/ LA CENTER ROAD UNDERPASS: OPTION D


BURK/ LANDON: OPTION E1


CARLSON/BURK/ LANDON/FUDGE/3B: OPTION E2


BURK/ LANDON: OPTION E3


BURK/ VANVESSEM: OPTION F


KITTELSON \& ASSOCIATES, INC.
TRANSPORTATION ENGINEERING/PLANNING

## Appendix J Cowlitz Reservation Development IJR Analysis <br> Methodology

# TECHNICAL MEMORANDUM Cowlitz Reservation Development IJR Analysis Methodology 

Date: $\quad$ October $16^{\text {th }}, 2014$<br>Project \#: 12393<br>To: Ray Shank, Washington Department of Transportation<br>Rick Keniston, PE, Washington Department of Transportation<br>Dave Bellinger, PE, Washington Department of Transportation<br>Matt Hughart, AICP; Marc Butorac, PE, PTOE; Chris Brehmer, PE, \& Kelly Laustsen; Kittelson \& Associates, Inc.

This memorandum documents the freeway analysis methodology proposed for inclusion in the I-5/La Center Interchange Justification Report (IJR) and supplements the information contained in the approved IJR Methods \& Assumptions document, dated October 2013.

This incremental memorandum is being provided to allow WSDOT an opportunity to review and comment on the transportation methodology and assumptions as the IJR is being prepared. Our intent it to secure consensus on the study methodology and findings in an incremental manner that will also allow the Applicant's project team an opportunity to make adjustments as needed prior to submittal of the formal IJR document. This memorandum largely reflects and confirms our email discussions with WSDOT staff, with documentation of these discussions provided in Attachment A.

## BACKGROUND \& ANALYSIS METHODOLOGY

Figure 1 illustrates the site vicinity and the study interchange. Kittelson \& Associates, Inc. (KAI) staff visited the study area and inventoried the existing transportation system in September 2012 and in July 2014. In addition, Quality Counts, LLC collected traffic volume data at several locations, as documented later in this memorandum.

The operational methodology presented in this memorandum is consistent with the methods described in the approved IJR Methods and Assumptions document, dated October 2013. As a component of the IJR process, the WSDOT Design Manual requires a 'Methods and Assumptions Document' be developed to record assumptions, criteria, and support team decisions used in the IJR. The Methods and Assumptions document for the I-5/La Center Interchange was approved in October 2013.

In addition to the IJR, a transportation impact analysis (TIA) will be prepared to document the impacts of the proposed Cowlitz Reservation development on the local system. The TIA will incorporate the preferred alternative from the IJR and will report analysis of the IJR study intersections along NW La Center Road/NW 319 ${ }^{\text {th }}$ Street under existing and forecast future conditions as per the IJR.

## METHODOLOGY

The freeway mainline and freeway merge/diverge operational analyses presented in this report were prepared following Highway Capacity Manual 2010 (HCM 2010) analysis procedures using Highway Capacity Software (HCS) 2010 traffic analysis software. HCS 2010 is a software package that analyzes ramp merge and diverge areas focusing on an influence area of 1,500 feet, including the acceleration or deceleration lane and adjacent freeway lanes.

## Measures of Effectiveness (MOE)

The WSDOT Design Manual, Chapter 320 describes the measure of effectiveness (MOE) used for determining a highway facilities' level of service (LOS) as follows:

- The level of service (LOS) for operating state highway facilities is based upon measures of effectiveness (MOEs), in accordance with the latest version of the Highway Capacity Manual.
- These MOEs (see Table 1 below) describe the measures best suited for analyzing state highway facilities, such as freeway segments and on- or off-ramps. Depending on the facility, WSDOT LOS thresholds are LOS C and LOS D on state highway facilities.

Table 1 WSDOT Measures of Effectiveness by Facility Type

| Type of Facility | Measure of Effectiveness (MOE) |
| :--- | :--- |
| Basic Freeway Segments | Density (pc/mi/ln) |
| Ramps | Density (pc/mi/ln) |
| Ramp Terminals | Delay (sec/veh) |
| Multilane Highways | Density (pc/mi/ln) |

$\mathrm{pc} / \mathrm{mi} / \mathrm{ln}=$ passenger cars per mile per lane
The level of service (LOS) for freeway merge, diverge, and weave operations is determined by traffic density based on criteria outlined in the Highway Capacity Manual (HCM) 2010, as shown in Table 2.

Table 2 LOS Criteria for Freeway Merge/Diverge/Weave (HCM 2010)

| LOS | Maximum Density (pc/mi/ln) |  |
| :---: | :---: | :---: |
|  | Merge/Diverge | Weave |
| A | $\leq 10$ | $0-10$ |
| B | $>10-20$ | $>10-20$ |
| C | $>20-28$ | $>20-28$ |
| D | $>28-35$ | $>28-35$ |
| E | $>35$ | $>35$ |
| F | Demand Exceeds Capacity | Demand Exceeds Capacity |

Speed (mph) and travel time (minutes) are also indicators of the performance of an individual segment and the overall freeway facility.

## WSDOT Operating Standards

WSDOT provides a table of LOS standards for state highways of statewide significance (HSS) based on RCW 47.06.140(2). Regional transportation planning organizations (RTPOs) and WSDOT jointly develop and RTPOs establish LOS standards for regionally significant state highways based on RCW 47.80.030(1)(c). Table 3 presents the WSDOT standards for state facilities in Clark County and Cowlitz County.

Table 3 WSDOT Level of Service Standards for Washington State Highways, January 1, 2010

| Regional Organization/County | LOS for Non-HHS ${ }^{1}$ |  | LOS for HSS ${ }^{1}$ |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Urban | Rural | Urban | Rural |
| (RTC) Southwest Washington Regional Transportation Council - MA/MP/RTPO <br> Clark County <br> Cowlitz County | $\begin{aligned} & \mathrm{E} \\ & \mathrm{D} \end{aligned}$ | C | D | C |

${ }^{1}$ HSS=Highway of Statewide Significance
Per WSDOT direction, LOS C will be the standard used for the I-5 mainline and merge/diverge operations for the existing conditions analysis. As noted in the IJR Methods \& Assumptions, LOS C will also be the standard used through the 2017 analysis scenarios, while LOS D will be used for the 2037 scenarios.

## Analysis Years/Periods

In order to assess the impact of the proposed Cowlitz Reservation Development, three analysis years (existing 2014, 2017, and 2037) will be required. Conditions were analyzed during the following time periods:

- Weekday morning peak period (7:00-9:00 AM)
- Weekday evening roadway peak period (4:00-6:00 PM)
- Weekend peak period (Friday 3:00-6:00 PM)

The weekend peak period was selected to address the unique trip generating characteristics of the casino and recreational travel on I-5. As recorded in the Cowlitz Reservation Development Trip Generation Memo dated October 2012, the trip generation profile of a casino was reviewed over the weekend, recognizing that casino trip generation typically peaks during the weekend. Traffic volumes in the vicinity of the site and on l-5 were assessed to better understand weekend traffic conditions and peaking characteristics in the area; particularly the distinct recreational directional trip patterns between the Portland and Seattle/Tacoma metropolitan areas. The cumulative impact of the background volumes and development trips is anticipated to typically be highest during the Friday PM peak. The two graphs in Exhibit 1 provide a profile of weekend volumes on l-5 from September 2012 (provided in the Trip Generation Memo ${ }^{1}$ ) and May 2013. In both cases, l-5 volumes are highest during Friday afternoon in both the northbound and southbound directions.

As described in detail in the October 2013 trip generation memo, trip generation rates anticipated at the casino over the course of a typical weekend were also assessed. Data from a number of other sites were reviewed and showed that the individual casinos peaked at different times and days of the weekend. However, considering both the existing volumes on l-5 and the measured casino generated traffic at other sites, Friday evening was selected to capture the highest cumulative impact from existing l-5 volumes and anticipated casino-generated traffic. Most of the casinos experience a Friday peak near 5:00 PM, indicating that the combination of traffic on the roadway system and produced by the proposed casino is likely to peak near this time as well. As discussed later in this memorandum, the counts were compared to the $30^{\text {th }}$ highest hour volumes on I-5 to ensure they are representative of design hour volumes.

[^10]Exhibit 1: l-5 Weekend Volume Profiles


Note: Data in top graph is from WSDOT for Friday, September $17^{\text {th }}, 2012$ - Sunday, September $19^{\text {th }}, 2012$; data in bottom graph is for Friday, May $24^{\text {th }}, 2013$ - Sunday, May $26^{\text {th }}, 2013$

## Analysis Inputs

Where possible, inputs for the freeway mainline and merge/diverge analysis were derived from available data. The lengths of deceleration and acceleration lanes for the merge analysis were measured in Google Maps. All heavy vehicles were entered as "trucks and buses" as the data collected did not specify recreational vehicles. Where data was not available, defaults values from the HCM 2010 were applied. Free-flow speed was assumed as 35 miles per hour ( mph ) on the ramps and 70 mph on the mainline, based on default values from the HCM 2010.

## TRAFFIC VOLUMES DEVELOPMENT

Turning-movement counts were collected at the I-5/La Center Ramp terminals for a typical weekday and Friday in mid-May 2014. At the same time, I-5 mainline counts were collected south of the interchange. Traffic data from the weigh station on northbound I-5 located south of the NW La Center Road interchange was received from WSDOT for June 2014. The turning movement counts and mainline data are provided in Attachments $C$ and D, respectively. Data from the weigh station is provided in Attachment $E$. The following sub-sections describe the development of traffic volumes for use in the existing and future analysis.

## Peak Hour Factor

The ramp volumes at l-5/La Center were derived from the turning movement counts collected at the ramp terminals. In accordance with the HCM 2010 methodology, the peak hour volumes were developed by multiplying the peak 15 minutes by four and a peak hour factor of 1.0 was used for the analysis.

## Seasonal Adjustment Factor

The WSDOT automatic traffic recorder (ATR) 045 is located just north of the NW La Center Road interchange with no ingress/egress points in-between. It therefore serves as a good proxy for l-5 mainline volumes at the interchange. Based on 2013 data collected at the ATR, the seasonal adjustment factor for May is 1.04 (2013 Annual Traffic Report, Attachment F). The traffic volumes on the I-5 mainline were multiplied by this factor to be representative of average traffic volumes.

## Design Hour Volumes

WSDOT typically uses volumes representative of the $30^{\text {th }}$ highest hour for design hour volumes. In order to ensure that the volumes used in the IJR analysis are representative of the design hour volumes, we compared the seasonally adjusted May 2014 volumes to the $29^{\text {th }}, 30^{\text {th }}$, and $31^{\text {st }}$ highest hours collected at ATR 045 in 2013. The results are shown in Table 4.

Table 4 I-5 Volumes north of La Center Interchange

| Location | 29 ${ }^{\text {th }}$ Highest Hourly Volume (1 PM, Nov 30, 2013) | $30^{\text {th }}$ Highest Hourly Volume (4 PM, Jul 28, 2013) | 31 ${ }^{\text {st }}$ Highest Hourly Volume (3 PM, Dec 1, 2013) | Weekend Counts* (4:45 PM, <br> May 16, 2014) | Weekend Counts* (seasonally adjusted) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| NB Mainline | 3,295 | 2,917 | 3,450 | 3,141 | 3,267 |
| SB Mainline | 3,196 | 3,568 | 3,032 | 2,933 | 3,050 |
| Total | 6,491 | 6,485 | 6,482 | 6,074 | 6,317 |

*Based on $4 \times$ peak 15 minute volume
As seen in the table, the seasonally adjusted weekend peak hour counts (collected on Friday, May $16^{\text {th }}$, 2014) are of similar magnitude to the $30^{\text {th }}$ highest hour counts. Therefore, these volumes are appropriate for use in the existing conditions assessment and as a basis for estimating future volumes.

## Truck Percentages and Volumes at the Weigh Station

I-5 mainline counts were collected south of the interchange for a typical weekday and Friday in midMay 2014. Based on the data collection method used, the counts reflect total vehicles and do not differentiate between vehicle classifications. Therefore, I-5 mainline data from 2012 at the ATR station 045 was used to estimate truck percentages on I-5 both northbound and southbound for the analysis periods. The summarized data and truck percentages used for the analysis are provided in Attachment $G$.

Traffic data from the weigh station on northbound I-5 located south of the NW La Center Road interchange was received from WSDOT for June 2014. The data provides volumes on I-5 and entering the weigh station for the weekday and Friday peak periods of analysis. The average truck volumes at the weigh station for the peak periods were derived from the data for each analysis time period (weekday AM, weekday PM, and weekend peak). The data from WSDOT reflects the number of trucks at the weigh station for the entire peak period (i.e. 7:00 to 9:00 AM). In order to estimate the number of trucks within the peak hour, the total volume was multiplied by the proportion of trucks on l-5 during just the peak hour within the peak period (based on I-5 data from 2013 also provided by WSDOT). The data from the weigh station and calculations performed to estimate the number of trucks entering/exiting the weigh station during the analysis periods are provided in Attachment $E$.

## Future Volumes

## Near-term 2017

The 2017 background volumes on the l-5 mainline were developed by applying a $2 \%$ linear annual growth rate to the seasonally adjusted volumes used in the existing conditions analysis. The growth rate was developed based on comparison of the Southwest Washington Regional Transportation Council (RTC) travel demand models for the horizon years 2005 and 2035. The 2035 RTC model used in
this analysis does not reflect recently revised (lower) county-wide population growth rate assumptions adopted by Clark County (the County's population growth estimate is now an average 1.12 percent annual growth county-wide). We understand the RTC models will be revised in the future to reflect the County's lower population growth assumptions and, as a result, the future volumes developed for this analysis using two percent annual growth are likely conservatively high.

The ramp volumes were extrapolated from counts at the ramp terminals. The ramp terminal counts were developed by applying an annual growth rate to existing traffic count data and adding the inprocess traffic volumes. Annual growth rates were applied to the existing traffic count data by intersection approach per agency scoping direction. Growth rates were selected by reviewing historical traffic counts around the interchange area, which indicated a rate of $2 \%$ at the I-5 on- and off-ramps and approximately $3 \%$ along La Center Road. At the interchange, volumes were balanced following the application of annual growth rates.

## Long-term 2037

Consistent with the horizon year 2017 model volume development, the 2037 background mainline volumes on I-5 were developed by applying a $2 \%$ linear annual growth rate to the seasonally adjusted peak hour volumes. For purposes of the 2037 analysis, the growth rate was applied to the seasonally adjusted ( $30^{\text {th }}$ highest hour) peak hour volumes (as opposed to applying the annual growth rate to volumes derived using four times the peak fifteen minute volumes). Use of the actual hourly volume instead of volumes derived by multiplying the peak 15-minute volume by four recognizes that travel demand on $\mathrm{I}-5$ is expected to spread over the hour in the long-term and exhibit less of the existing peaking characteristic. This approach is consistent with applying a peak hour factor of 1.0 in the longterm analysis.

Year 2037 traffic volume projections were developed using existing traffic count data and forecast future volume data provided by RTC's regional travel demand model. A summary of the volume development methodology and assumptions is provided in the following sections.

## Travel Demand Model

RTC uses the travel demand forecasting program VISUM to estimate future traffic volumes on primary roadways such as freeways, arterials, and collectors. RTC's travel demand forecast model was developed in part based on the 2011 Metropolitan Transportation Plan for Clark County (MTP). Horizon year 2035 land uses are based on the adopted Comprehensive Growth Management Plan for Clark County (Clark County, September 2007) which has a horizon year of 2024 extended a further eleven years to the MTP's 2035 horizon. The 2035 demographic projections and land use allocations were developed by local jurisdictions working in partnership with RTC.

The model's data input includes population and employment for both "base year" conditions (Year 2010) and future "design year" conditions (Year 2035). The 2035 RTC model used in this analysis does
not reflect recently revised (lower) county-wide population growth rate assumptions adopted by Clark County (as of the time this report was prepared, the County's population growth estimate was reduced to an average 1.12 percent annual growth county-wide). It is understood that the 2035 RTC model will be revised in the future to reflect the County's lower population growth assumptions and, as a result, the future volumes developed for the 2037 analysis using two percent annual growth are likely conservatively high.

## 2037 Background Traffic Model Post Processing for Weekday PM and Friday PM (Weekend) Peak Hour

The RTC VISUM model provides PM peak hour volumes including directional flows on key roadway links (i.e. road segment between intersections) and turning movement volumes at key intersections. Appendix " $P$ " contains the VISUM output sheets for both the 2010 base year and 2035 design year for the project area roadways and intersections.

Because the RTC model does not include all local streets and driveway connections, the raw forecast turning movements at individual intersections from the model are not typically used for design purposes. Rather, the model is used to identify the order-of-magnitude future growth along the primary travel corridors, based on planned changes to the land use and transportation systems within the region. Output from the model is "post-processed" (manually adjusted) using field traffic data and engineering judgment to identify turning movements at each study intersection. This method of refining the raw traffic volumes is standard practice for planning and forecasting analyses and is discussed further and in more detail below.

The RTC model volumes were refined using techniques outlined in NCHRP Report 255 to "post-process" the data. In this process, the future traffic projections from the model were evaluated with respect to current year 2014 traffic counts and the relative differences between the model scenarios. The results of using both the "ratio" method and the "difference" method, as outlined in the NCHRP report, were compared. In this case, the average of the "ratio" and "difference" methods was used to establish the initial projected volume of through traffic. Manual adjustments were made to the projected turning movements at individual intersections to better reflect the existing traffic counts and the anticipated build-out conditions to achieve 2035 developed volumes. Finally, a two percent growth rate was applied to the 2035 turning movement volumes to estimate year 2037 volumes.

All of the calculations and adjustments described above are provided in Appendix " $Q$ ".

## 2037 Background Traffic for Weekday AM Peak Hour

Because the RTC regional travel demand model provides forecast volumes only for the weekday PM peak hour, projections for the 2035 weekday AM and weekend peak hours were developed manually assuming similar growth patterns from the PM peak hour projections. The projected growth at the interchange from the weekday PM peak hour was factored according to the ratio of existing AM to PM
peak hour volumes. This factored growth was then applied to the existing weekday AM peak hour counts and distributed according to existing travel patterns. Manual adjustments were made to the projected turning movements at each intersection to reflect the anticipated build-out conditions during the 2035 weekday AM peak hour. Finally, a two percent growth rate was applied to the 2035 turning movement volumes to estimate year 2037 volumes.

For methodology validation purposes, the resultant 2037 projections were compared to the RTC 2035 model volumes and year 2030 volumes derived in the Ridgefield IJR completed in 2009. The results of this comparison are shown in Table 5.

Table 5 Future I-5 Volumes south of La Center Interchange

| Location | Ridgefield IJR <br> (2030 Build PM) | RTC Model <br> (2035 PM Peak) | 2037 Background <br> Weekend Peak <br> (30 |
| :--- | :---: | :---: | :---: |
| Northbound Mainline | 4,485 | 4,910 | 4,997 |
| Southbound Mainline | 4,330 | 3,816 | 4,506 |
| Total | $\mathbf{8 , 8 1 5}$ | $\mathbf{8 , 7 2 6}$ | $\mathbf{9 , 5 0 3}$ |

As seen in the table, the weekend peak hour volumes used in the I-5/La Center IJR are significantly higher than those used in the Ridgefield $I J R^{2}$ or forecasted in the RTC model (recognize that the RTC model volumes will likely be reduced in the future due to the revised Clark County population growth projections). Based on the above comparison, we conclude the methodology employed to develop the year 2037 traffic volume projections results in volume projections that are reasonably conservative (high).

## NEXT STEPS

The I-5 freeway conditions assessment was presented in Technical Memorandum \#2: Cowlitz Reservation Development Preliminary Interchange Evaluation and discussed in the I-5/La Center Interchange Improvement Project IJR Workshop on July $14^{\text {th }}, 2014$. The analysis will also be incorporated into the draft IJR document being prepared as part of the Cowlitz Reservation Development project. This memorandum will also be referenced in the IJR.

Recognizing that this methodology serves as an essential foundation for the remainder of the study, we request that you review the material presented in this memorandum and provide us with any suggested revisions or questions that you may have.

[^11]
## ATTACHMENTS

A. Emails with WSDOT Staff documenting Methods and Assumptions
B. Cowlitz Reservation Development Trip Generation Memo
C. Turning Movement Counts at I-5/La Center Road Ramp Terminals
D. I-5 volumes mainline volumes south of La Center Road
E. Weigh Station Data from June 2014
F. Seasonal Adjustment Factor for R045
G. Truck Percentages for l-5

From:<br>Sent:<br>To:<br>Cc:<br>Subject:<br>Shank, Ray [ShankR@wsdot.wa.gov](mailto:ShankR@wsdot.wa.gov)<br>Wednesday, July 09, 2014 4:25 PM<br>Kelly Laustsen<br>Matt Hughart; Chris Brehmer; Clark, Mike; Bellinger, Dave; Keniston, Rick<br>RE: Follow-Up - I-5/La Center Analysis<br>Kelly,

As mentioned in our phone discussion earlier today, using your proposed methodology of seasonally adjusting the Friday PM counts appears to be acceptable. When comparing the adjusted short count data to our typical design hour methodology, the resulting volumes were very similar (within $\sim 15$ vehicles for the peak direction). Since we've gone through these steps, we may want to include some discussion that we used data from the adjacent PTR to validate using the adjusted short count data.

After looking at the PTR data, it appears that while the heaviest northbound volumes on I-5 occur during the Friday PM Peak, the heaviest southbound volumes occur on Sunday. We talked about this a little bit on the phone. You mentioned that the cumulative impact of southbound I-5 volumes and new trips generated by the development on the Friday PM Peak may be more than that of the impacts anticipated on Sunday. I think we are still good with our current set of scenarios, but perhaps we should confirm this direction with the rest of the stakeholders at Monday's meeting.

Let us know if you have any questions.
Ray Shank
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From: Kelly Laustsen [mailto:klaustsen@kittelson.com]
Sent: Tuesday, July 08, 2014 11:22 AM
To: Shank, Ray
Cc: Matt Hughart; Chris Brehmer; Clark, Mike; Bellinger, Dave; Keniston, Rick
Subject: RE: Follow-Up - I-5/La Center Analysis
Hi Ray,
Thanks for the additional information. I looked at the ATR data you sent and prepared the table below showing volumes north of the interchange under a number of scenarios. As you can see, the distribution of volumes northbound/southbound varies between the $29^{\text {th }}, 30^{\text {th }}$, and $31^{\text {st }}$ highest hourly volumes, likely influenced by the time of day, week and month or area events. I'd suggest that we maintain the distribution from the counts we collected (based on a review of the ATR data, this is pretty typical of a Friday PM). If we apply the same seasonal factor that we used for the $A M$ and PM counts of 1.04 , the volumes are relatively close to the $30^{\text {th }}$ highest hour.

| $29^{\text {th }}$ Highest |
| :---: | :---: | :---: | :---: | :---: |
| Hourly Vol (1pm, |
| Nov 30, 2013) | | $30^{\text {th }}$ Highest |
| :---: |
| Hourly |
| $(4 \mathrm{pm}$, Jul 28, | | $31^{\text {st }}$ Highest |
| :---: |
| Hourly Vol (3pm, |
| Dec 1, 2013) | | Friday PM Counts* |
| :---: |
| $(4: 45 \mathrm{pm}$, May 16, |
| 2014) | | Friday PM Counts* |
| :---: |
| (seasonally |
| adjusted) |


|  |  | 2013) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| NB Mainline | 3295 | 2917 | 3450 | 3141 | 3267 |
| SB Mainline | 3196 | 3568 | 3032 | 2933 | 3050 |
| Total | 6491 | 6485 | 6482 | 6074 | 6317 |

*Based on 4*peak 15 minute volume
We suggest using the Friday PM counts we collected with the seasonal adjustment of 1.04. Although these volumes are slightly lower than the $30^{\text {th }}$ highest hourly volume, we are using the long-term analysis (with a $2 \% /$ year growth rate) for our design, which is conservative. Please let me know if you think this is reasonable.

Thanks!
Kelly

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From: Shank, Ray [mailto:ShankR@wsdot.wa.gov]
Sent: Monday, July 07, 2014 9:02 AM
To: Kelly Laustsen
Cc: Matt Hughart; Chris Brehmer; Clark, Mike; Bellinger, Dave; Keniston, Rick
Subject: RE: Follow-Up - I-5/La Center Analysis
Kelly,
Thanks for providing the September 2012 count data for comparison. As you mentioned, these counts are relatively similar. The methodology proposed in an earlier e-mail, using May 2014 counts with a 1.04 adjustment factor for interstate volumes, uses the most recent data along with historical temporal trends and will likely provide us with representative peak hour volumes.

Attached you will find the 2013 data for PTR R045 which is located just south of the I-5/SR 503 Interchange near Woodland. Please review and let us know if it meets your needs.

For the Friday PM peak volumes, I'd like to use a volume set that is representative of the $30^{\text {th }}$ highest hour, which is our typical methodology for design hour volumes (DHV). As mentioned in my previous e-mail, historical trends seem to indicate that the $30^{\text {th }}$ highest hour occurs during the Friday PM peak. The amount of information that goes into developing DHV (hourly volume data over an entire year) is much more robust than using short count data (approx. one week of data). Therefore, I would prefer to use this methodology. However, if the derived DHV is similar to that of the adjusted short count data then we can consider using the short count data in the analysis.

Let us know if you need anything else.

## Ray Shank

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shankr@wsdot.wa.gov

From: Kelly Laustsen [mailto:klaustsen@kittelson.com]
Sent: Monday, July 07, 2014 5:01 AM
To: Shank, Ray
Cc: Matt Hughart; Chris Brehmer; Clark, Mike; Bellinger, Dave; Keniston, Rick
Subject: RE: Follow-Up - I-5/La Center Analysis
Hi Ray,

Thank you for your quick, thorough responses - I really appreciate all your help. A couple comments/questions:

- You asked for a comparison between the counts we collected in September 2012 and May 2014 - see the table below (note that l've shown the total volume recorded during the peak hour as opposed to 4*peak 15 minute volume). As you can see, our counts are relatively similar (with some increases and decreases of <10\%).

|  | Weekday AM | Weekday PM | Friday PM |
| :---: | :---: | :---: | :---: |
| NB Mainline (south of interchange) | $2067(2031)$ | $2850(2776)$ | $3372(3531)$ |
| SB Mainline (south of interchange) | $2395(2295)$ | $2543(2766)$ | $2999(3060)$ |

May 2014 (September 2012)

- You referenced the 2013 data from ATR 045. I received 2010-2012 data for I-5, but don’t believe I have 2013. Could you send along to me when you have an opportunity?
- For the Friday PM peak, you suggested identifying the $30^{\text {th }}$ highest hour volumes as design volumes. Would you suggest using these in place of the actual counts we collected during the Friday PM peak, or comparing to our counts to assess whether they are appropriate?

Thanks again! Hope you enjoyed the holiday.
Kelly
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From: Shank, Ray [mailto:ShankR@wsdot.wa.gov]
Sent: Thursday, July 03, 2014 2:15 PM
To: Kelly Laustsen
Cc: Matt Hughart; Chris Brehmer; Clark, Mike; Bellinger, Dave; Keniston, Rick
Subject: RE: Follow-Up - I-5/La Center Analysis
Kelly,

Please find my responses to your questions in the e-mail below.
Let us know if you need anything else.

## Ray Shank

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From: Kelly Laustsen [mailto:klaustsen@kittelson.com]
Sent: Wednesday, July 02, 2014 8:09 PM
To: Shank, Ray
Cc: Matt Hughart; Chris Brehmer
Subject: Follow-Up - I-5/La Center Analysis
Hi Ray,
Thanks again for talking with Chris, Matt and me this afternoon, particularly on such short notice. I really appreciate your help in our development of traffic volumes for the interchange analysis we are conducting at I-5/La Center Road for the proposed Cowlitz development. I've summarized our discussion points from today and noted in italics where I would appreciate your confirmation or additional information. I've also provided some supplemental background information.

## Background Information

- Time periods: weekday AM peak hour, weekday PM peak hour, Friday PM peak hour
- Analysis years: existing, 2017, 2037
- Analyzing l-5 mainline north and south of La Center, merge/diverge at La Center Road and weigh station
- Data collected: we collected counts on the I-5 mainline (just south of La Center Road) on May $16^{\text {th }}$ and $20^{\text {th }}$. For reference, our peak hour volumes are summarized below (note that this reflects a peak hour factor of 1.00 - see Analysis Methodology Question \#1).

|  | Weekday AM | Weekday PM | Friday PM |
| :---: | :---: | :---: | :---: |
| NB Off Ramp | 312 | 579 | 589 |
| NB On Ramp | 172 | 133 | 162 |
| SB On Ramp | 482 | 364 | 412 |
| SB Off Ramp | 112 | 208 | 257 |
| NB Mainline (south of interchange) | 2332 | 2956 | 3568 |
| SB Mainline (south of interchange) | 2628 | 2672 | 3088 |

## Analysis Methodology Questions

1. Peak Hour Factor - we have collected volumes on I-5 and at the La Center ramp terminals. We propose to develop peak hour counts by multiplying the peak 15 minutes by four and applying a PHF of 1.00. You indicated that you were likely comfortable with this approach - can you confirm?

I am comfortable with this approach as it should result in a more conservative analysis.
2. Seasonal Adjustment Factor - we collected our traffic counts in mid-May 2014. Our previous counts were collected in September 2012. We did not apply a seasonal adjustment factor to our counts before (since September is typically a higher month). The conversion factor for RO45 (the permanent traffic recorder on I-5 just north of La Center Road) for the month of May is 1.04, as shown in the attached page from the 2013 Annual Traffic Report.
Should we apply an adjustment to our May counts?

## AM and PM Peaks

Applying the 1.04 adjustment factor to the counts collected along the interstate in May seems like a practical approach to reach representative peak hour volumes. As a reasonableness check, I would be interested to know how this new volume set relates to the previously collected data back in September of 2012.

## Friday PM Peak

We should take advantage of the permanent traffic recorder (R045) as it is located just to the north, without any ingress or egress access points influencing volumes between the recorder and the LaCenter Interchange. I believe that you mentioned during our phone conversation that you received 2013 data for this recorder already (If not, I should be able to supply this information). From this year long data set, we can identify volumes that are representative of the $30^{\text {th }}$ highest hour, which is typically used as our design hour volumes. No adjustment factors will need to be applied using this approach. The peak hour report for this PTR can be located at the following webpage: http://www.wsdot.wa.gov/mapsdata/travel/peakhourreport.htm. Although, the latest report for 2013 has yet to be published, our Traffic Data Office has supplied us with some of the key information.

2013 PTR R045 Data
AADT: 67911
$K 30=9.55$
$K 100=8.99$
$K 200=8.64$
$D 30=50.63$

While the full 2013 report has yet to be published, the 2011 report seems to indicate that the design hour volumes should be representative of the Friday PM Peak Hour.

## Local Intersections

For volumes along the local roadway, see my response to question number 3.

- If we do need to apply a seasonal adjustment factor, should we just apply it to the l-5 mainline? I assume based on the uses surrounding La Center Road that volumes on the ramps do not fluctuate significantly during the year. See response above. I would recommend that the ramp volumes use the same approach as that of the Local Intersections.
- If we do need to apply a seasonal adjustment factor, should we grow the seasonally adjusted volumes for our future year (2017 and 2037) analyses? We are applying a $2 \%$ annual linear growth rate (based on our assessment of RTC's most updated model). Future volumes will be developed from our base year volumes. Any adjustments made to the base year would thereby be incorporated into the future volumes and further adjustment will not be required.

3. Additional Factors/Adjustments - you indicated that we should apply a factor of 1.3 for the existing conditions analysis as a sensitivity test (to account for the fact that we are using average volumes and not converting for design hour volumes). Can you confirm that we should apply this sensitivity test and just for the existing conditions assessment?

The sensitivity test that applies a factor of 1.3 to the existing conditions was intended for volumes at the local intersections (i.e. ramp terminals as well as any other intersections along La Center Road and 319 Street). We are applying this test since the adjustment factors developed from PTR R045 are not applicable as the temporal trends along l-5 are not similar to that of the local streets. This test, bumping up the volumes by 30\%, takes a high clip look to assess the level of risk we might be taking using the information from the limited short count data. If the higher volume does not have any practical implication for the design, then we can just use the short count data as is. However, if the higher volume does result in an impact to the design, then we will have to discuss possible adjustments to these volumes more thoroughly.

This test was previously suggested by our TDGO office. If you have a different approach that you would like to apply when developing the local volumes, I'd be willing to listen.
4. Weigh station volumes - we are assessing merge/diverge operations at the weigh station on I-5 south of La Center. Can you provide any volumes at the weigh station or estimate of typical volumes?

The attached excel file contains some weigh station data and the attached PDF helps to demonstrate where the counts are located. Please review and let me know if this is what you're looking for.

Please let me know if you have any questions about the information above and thanks again for your help. Kelly

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## Kittelson \& Associates, inc.

 TRANSPORTATIONENGINEERING/PLANNING 610 SW Alder Street, Suite 700, Portland, OR 97205 P 503.228.5230 F 503.273.8169TECHNICAL MEMORANDUM \#3:
Cowlitz Reservation Development Trip Generation

Date: November 12, 2012<br>To: Jeffrey B. Sarvis, City of La Center Public Works<br>Tony Cooper, PE, City of La Center Public Works<br>Rick Keniston, PE, Washington State Department of Transportation<br>Steve Schulte, PE, Clark County Department of Public Works<br>David Jardin, Clark County Department of Public Works<br>Chris Clemow, PE, Group Mackenzie on behalf of the City of La Center<br>Kelly Laustsen; Marc Butorac, PE, PTOE; \& Chris Brehmer, PE

Project \#: 12393

The memorandum documents proposed trip generation assumptions for the proposed Cowlitz Reservation Development to be located in in La Center, Washington. Pending review agency feedback, the trip rates proposed in this memorandum will be used to prepare a traffic impact analysis and interchange justification report (IJR) for the proposed development. In addition to the traditional morning (7:00-9:00 AM) and evening (4:00-6:00 PM) peak periods, the trip generation assessment identified the need to study Friday evening peak conditions during the 5:00-6:00 PM hour. The assessment includes the directional split of trips to and from the site, as well as an analysis of trip type. The remainder of this document describes the proposed development, the trip assessment methodology, the recommended peak hour analysis periods and the corresponding trip rates.

## PROPOSED COWLITZ RESERVATION DEVELOPMENT OVERVIEW

The proposed Cowlitz Reservation Development will be located west of the l-5/La Center interchange in La Center, Washington as shown in Figure 1. The site is located approximately 25 miles north of the Portland, Oregon metropolitan region and is targeted for opening in 2016.

While the final site land uses have yet to be determined, at full build-out the site may include up to:

- 3,500 gaming positions (2,000 slots, 60 banked tables, 15 poker tables as Phase One; 1,000 gaming positions in a future phase);
- 4 interior restaurants;
- 5,000-6,000 square feet of interior retail space;
- Casino bars;
- An event center with seating for up to 1,500 guests; and
- 250 -room hotel with restaurant and retail space.

Up to 3,450 parking spaces are expected on-site and valet parking services will be available.


## METHODOLOGY

Typically the City of La Center, the Washington State Department of Transportation (WSDOT), and Clark Country require analysis of weekday morning (7:00-9:00 AM) and evening (4:00-6:00 PM) peak commuter conditions. Other analysis periods may be identified on an as-needed basis. With the agency requirements in mind, trip generation estimates were developed for the site through a series of steps that included:

- Conducting a literary search of available trip generation data to identify analysis periods and available data;
- Synthesizing trip data collected at similar casino facilities;
- Collecting data at a comparable casino facility in Washington;
- Identifying recommended peak hour analysis periods based on the data collected; and
- Identifying recommended trips rates and volumes by analysis period.


## LITERATURE REVIEW

Several sources of data were reviewed to determine the appropriate approach for identifying the time periods to analyze the traffic impacts of the proposed Cowlitz development and anticipated trip generation of the development. Consistent with industry practice, weekday AM and PM peak trip data was first sought through the Institute of Transportation Engineers (ITE) Trip Generation.

Review of ITE Trip Generation, $9^{\text {th }}$ Edition identified limited data available for casino-related uses. Specifically, the most comparable land use was found to be ITE Land Use Code 473: Casino/Video Lottery Establishment. Trip Generation indicates the Land Use Code 473 database is limited to weekday p.m. peak hour data only and that the data was collected at six sites that provide electronic or manually-controlled slot machines. Trip Generation further indicates that full food service is generally not provided at the facilities; however, refreshments or alcoholic beverages may be served. ITE states the Trip Generation data does not include full-service casinos or casino/hotel facilities. Based on this information and the proposed development uses, additional trip data was sought.

Consistent with Trip Generation's recommendation to obtain additional data as needed, a literature review of available trip generation studies was conducted (highlights of the literature review results are provided in Appendix A). The literature review offered insights as to information needed to develop a reasonable trip rate for the proposed development while also offering several insights that included:

- Gaming positions correlate well with site trip generation and serve as a recommended independent variable.
- An entertainment venue in which concerts are held can also increase the trip generation potential of a casino.
- Casino/resort facilities located in Las Vegas and Reno are not indicative of trip generation potential for sites similar to the proposed development due to the sheer magnitude in size difference and the area in which they are located.
- Ancillary uses at a casino (i.e. restaurants, retail space) are encompassed in the casino's overall trip generation rate.
- The presence of an on-site hotel may reduce the casino's peak trip generation rate relative to sites without on-site housing.


## DATA SOURCES

Previously published trip data was obtained from five tribal casinos in the Northwest and one in the northeast which had qualities similar to the Cowlitz Reservation Development. In addition, trip data was collected as part of this study at a casino in Snoqualmie, Washington. Table 1 presents a summary of the sites considered in developing the final trip rates as well as the key characteristics of each.

Table 1: Summary of Casino Data Used to Develop Site Trip Estimates

| Casino | Location |  | Ancillary Uses | Gaming Positions (when data collected) | Data Collected |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Snoqualmie | Snoqualmie, WA | 25 miles east of Seattle, WA | Restaurants, Entertainment Venue | 2,185 | Seven Day Tube <br> Counts (Sept \& Oct 2012) |
| Mohegan Sun at Pocono Downs | Wilkes-Barre, PA | 15 miles southwest of Scranton, PA | Restaurants, Live harness racing, retail | $\begin{aligned} & \hline 2,466(2009) \\ & 1,099(2007) \end{aligned}$ | Seven Day Tube <br>  <br> Sept 2009) |
| Spirit Mountain | Grand Ronde, OR | 35 miles northwest of Salem, OR | Restaurants, Bingo, Arcade, Children's Area, Entertainment Venue, Hotel | 1,994 | Weekend Tube Counts (Aug 2005) |
| Seven Feathers | Canyonville, OR | 25 miles south of Roseburg, OR | Restaurants, Bingo, Hotel, Entertainment Venue, Gift Gallery, Hotel | 1,198 | Weekend Tube <br> Counts (Aug 2005) |
| Muckleshoot | Auburn, WA | 30 miles south of Seattle, WA | Restaurants, Bingo, Retail, Entertainment Venue, Convention and Meeting Space | 2,596 | Weekend Tube Counts (Aug 2005) |
| Tulalip Resort Casino | Tulalip, WA | 35 miles north of Seattle, WA | Restaurants, Entertainment Venue | 1,986 | Friday Evening Tube Counts (May 2004) |
| Northern Quest | Airway Heights, WA | 10 miles west of Spokane, WA | Restaurants, Entertainment Venue | 995 | Friday Evening Turning Movement Counts (May 2004) |

## TRIP GENERATION ANALYSIS

The trip data was reviewed in steps: first to identify analysis periods that would represent peak conditions; second to derive trip rates within each of the analysis periods; third to determine the directional split of trips to and from the site; and fourth to assess trip type, including any diverted or pass-by trips. This process is described below.

## Analysis Study Periods

In addition to typical weekday AM and PM commuter peak hour periods, the trip generation profile of casinos was reviewed over Fridays and weekends recognizing casino trip generation typically peaks during the weekend. Traffic volumes in the site vicinity were reviewed to better understand weekend traffic conditions and peaking characteristics in the area especially the distinct recreational directional trip patterns between the Portland and Seattle/Tacoma metropolitan areas.

## System Volume Profile

Traffic volume profiles on I-5 and at the I-5/La Center Road interchange were reviewed to better understand the peaking characteristics of the traffic system in the study area. Traffic volumes on I-5 were assessed using data collected at the WSDOT permanent recorder station R045, which is located north of the La Center/I-5 interchange at milepost 20.14. As shown in Exhibit 1, weekend traffic volumes peak at 4:00 PM on Friday for both northbound and southbound traffic. The directional split on I-5 during this period and throughout the weekend is roughly evenly split between northbound and southbound traffic.

Exhibit 1: I-5 Weekend Volume Profile


[^12]Traffic volumes on I-5 during the week were also reviewed to note any patterns in directional split or volumes. Exhibit 2 illustrates northbound and southbound volumes on I-5 from a Tuesday through Thursday.

Exhibit 2: I-5 Weekday Volume Profile


Note: Data shown is for Tuesday, September $14^{\text {th }}, 2010$ - Thursday, September $16^{\text {th }}, 2010$

As seen in the exhibit, weekday traffic volumes peak between 3:00 and 5:00 PM. Peak volumes increase gradually throughout the week. The directional split between northbound and southbound traffic is approximately even.

Traffic volume profiles in the study area were also assessed using 24-hour tube count data collected in September 2012 at the following locations (Data sheets are provided in Appendix B):

- I-5 southbound off-ramp to La Center Road;
- I-5 southbound on-ramp from La Center Road;
- I-5 northbound off-ramp to La Center Road; and
- I-5 northbound on-ramp from La Center Road.

The location of these sites relative to the proposed Cowlitz development is shown in Figure 2.
Exhibit 3 illustrates the hourly sum of traffic volumes at the four ramps between Friday morning and Sunday night. Based on this volume profile, traffic volumes at the I-5/La Center Road interchange peak at 5:00 PM on Friday afternoon.


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Exhibit 3: La Center/l-5 Ramps Weekend Volume Profile (Sum of Ramp Volumes)


Most traffic is anticipated to access the site by traveling north on I-5. Therefore, the traffic volume profile at the I-5 northbound off-ramp to La Center Road was assessed independently. The weekend profile is shown in Exhibit 4. As shown in the exhibit, traffic volumes also peak at 5:00 PM on Friday.

Exhibit 4: I-5 NB Off-Ramp to La Center Road Weekend Volume Profile


Based on this assessment, traffic volumes on I-5 in the vicinity of the site peak during the weekend on Friday at 4:00 PM, but are relatively constant between 3:00 and 6:00 PM. During this time, the directional split is approximately even between northbound and southbound traffic. Traffic volumes on the ramps at the I-5/La Center Road interchange peak at 5:00 PM on Friday and area also relatively constant between 3:00 and 6:00 PM.

## Casino Weekend Volume Profile

Trip generation rates were also reviewed at each of the casino sites over the course of a typical weekend. Table 2 identifies the day and time when peak trip generation was experienced during the Friday-Sunday period.

Table 2: Casino Weekend Peak Periods

| Casino | Peak Day | Peak Hour |
| :---: | :---: | :---: |
| Snoqualmie (September 2012) ${ }^{1}$ | Friday | 7:00-8:00 PM |
| Snoqualmie (October 2012) | Saturday | 5:00-6:00 PM |
| Pocono Downs (2007 data) ${ }^{2}$ | Saturday | 9:00-10:00 PM |
| Pocono Downs (2009 data) ${ }^{2}$ | Sunday | 4:00-5:00 PM |
| Spirit Mountain | Sunday | 2:00-3:00 PM |
| Seven Feathers | Saturday | 3:00-4:00PM |
| Muckleshoot | Friday | 10:00-11:00 PM |
| Tulalip ${ }^{3}$ | Friday | 7:00-8:00 PM |
| Northern Quest ${ }^{4}$ | Friday | 7:00-8:00 PM |

${ }^{1}$ Data was collected at Snoqualmie in both September and October 2012. The September data was collected from 12:00 AM on Friday to 10:00 AM on Saturday.
${ }^{2}$ Data was collected at Pocono Downs in both 2007 and 2009. The casino underwent a significant expansion between these years.
${ }^{3}$ Data was collected at Tulalip from 4:00-8:00 PM on Friday.
${ }^{4}$ Data was collected at Northern Quest from 2:00-8:00 PM on Friday.

Exhibit 5 illustrates the hourly trip rate at each of the casinos during the same period. As shown in both Table 2 and Exhibit 5, the individual casinos peak at different times and days of the weekend. In part, the peak times reflect the travel distance and level of congestions between the individual site and metropolitan areas in the vicinity. For example, facilities such as Spirit Mountain and Seven Feathers located further from metropolitan areas tend to require greater travel time to reach and thus tend to experience peaks outside typical commuter peak periods.

## Exhibit 5: Casino Weekend Trip Rate Profiles



Note: Data collection at Snoqualmie (in September 2012), Pocono (in 2007), Spirit Mountain, Seven Feathers, Muckleshoot, Tulalip, and Northern Quest shown for periods during which data was collected.

## Combined Roadway System and Casino Weekend Volumes

The combination of existing roadway network traffic volumes on the system near the Cowlitz site and the measured casino generated traffic at other sites were both considered to determine the most appropriate weekend peak period to study. I-5 peaks between 4:00 and 5:00 PM on Friday afternoon and the ramps at the I-5/La Center Road interchange peak between 5:00 and 6:00 PM on Friday afternoon, while the casinos show a large range of peaking characteristics. Although several of the casinos show weekend peaks on Saturday or Sunday, existing traffic volumes on the La Center area roadway system are notably lower during these days, as seen in Exhibit 1 and 3. Most of the casinos experience a Friday peak near 5:00 PM, so that the combination of traffic on the roadway system and produced by the proposed casino is likely to peak near this time as well.

The directionality of existing traffic and expected trips to the site was also considered to ensure a time period was not selected when traffic on the system and traffic to the site will be traveling in opposite directions. The directionality of traffic on I-5 Friday afternoon is approximately evenly split between northbound and southbound traffic, as shown in Exhibit 1. The majority of trips to the site are expected to arrive by traveling northbound on I-5. Therefore, Friday at 5:00PM is again a conservative analysis period. Based on this review, we propose Friday from 5:00 to 6:00 PM be used as the weekend peak analysis period.

## Snoqualmie Site Trip Data Collection

A trip generation study was completed at the Snoqualmie site based on the City of La Center's request to conduct an additional trip generation study at a casino in Washington state that it is directly comparable to the proposed Cowlitz Reservation Development in terms of size, content, and location. As shown in Table 1, the Snoqualmie site is similar in size and amenities, including an entertainment venue. Further, the location of the Snoqualmie site outside of the Seattle metropolitan area on an Interstate facility is akin to the Cowlitz Reservation Developments location north of the Portland metropolitan area. The Snoqualmie site is located immediately north of Interstate 90 and is readily accessible from the Seattle metropolitan area. Although traffic volumes on Interstate 90 are lower than those on Interstate 5 (ADT of 46,00 on I-90 compared to 65,000 on I-5 ${ }^{1}$ ), the proximity of Snoqualmie to a large metropolitan area is akin to the proposed Cowlitz development's proximity to the Portland metropolitan area.

Twenty-four hour tube count data was collected at the two accesses to the Snoqualmie Casino on Friday, September $21^{\text {st }}, 2012$ and the first full week in October, 2012 (provided in Appendix C for reference). The on-site entertainment venue was operational on both Fridays that data was collected, with the event in September likely drawing more visitors (Drew Carey performed at 8:00 PM on September $21^{\text {st }}$, 2012). The trip generation data from Snoqualmie was used in conjunction to the data

[^13]previously collected at the other six casino sites to develop the rates for the proposed Cowlitz development.

## Weekend Trip Generation Rate

After selecting Friday from 5:00 to 6:00 PM as the weekend analysis study period, the available trip data for the seven sites shown in Table 1 was further analyzed to determine the appropriate casino trip generation rate for the weekend period. The peak hour trip generation rate was identified and calculated at each site between the hours of 3:00 and 8:00 PM on a Friday using the trip rate data for each site. This longer time period was selected to produce a conservative analysis recognizing customer travel distance to each site varies and likely influences peak period timing. Table 3 summarizes the corresponding average Friday peak hour trip rates.

Table 3: Casino Trip Generation Rates between 3:00-8:00 PM on Friday

| Casino | Peak Time | Trip Rate <br> (trips/gaming position) |
| :--- | :---: | :---: |
| Snoqualmie (September 2012) | $7: 00-8: 00 \mathrm{PM}$ | 0.48 |
| Snoqualmie (October 2012) | $6: 00-7: 00$ PM | 0.37 |
| Pocono Downs (2007 data) | $3: 00-4: 00$ PM | 0.52 |
| Pocono Downs (2009 data) | $6: 00-7: 00 \mathrm{PM}$ | 0.51 |
| Spirit Mountain | $3: 00-4: 00$ PM | 0.40 |
| Seven Feathers | $3: 00-4: 00$ PM | 0.39 |
| Muckleshoot | $6: 00-7: 00$ PM | 0.40 |
| Tulalip | $6: 00-7: 00$ PM | 0.44 |
| Northern Quest | $7: 00-8: 00$ PM | 0.53 |

The resultant average trip rate of 0.45 trips/gaming position falls between the trip rates observed at the Snoqualmie site for the two dates in September and October (which is judged by the Applicant to be most comparable to the Cowlitz Reservation Development). A rate of 0.48 trips/gaming position was observed at the Snoqualmie site in September. While 0.48 trips/gaming position is lower than the rates reported at Pocono Downs in 2007 and 2009, the proposed Cowlitz Reservation Development is expected to more closely resemble the northwest casino sites and their trip rates. By comparison, Pocono Downs includes live harness racing and is located on the east coast with a large population base to draw from.

Based on this review, we propose to base the trip generation rate for the traffic analysis off the higher observed data at Snoqualmie in September 2012 and use 0.48 trips/gaming position for assessing

Friday 5:00-6:00 PM peak hour conditions. The 0.48 trips/gaming position rate is higher than the average rate shown in Table 3 and all is also higher than any of the other northwest casinos, thus yielding a conservative analysis.

## Weekday AM and PM Trip Generation Rates

As previously noted, traffic conditions at the proposed Cowlitz Reservation Development will also be studied during the weekday morning peak period (7:00 AM to 9:00 AM) and weekday evening peak period (4:00 PM to 6:00 PM). Traffic volume data collected at the Snoqualmie site in October, 2012 and Pocono Downs in 2007 was used to develop weekday trip rates given the lack of available weekday data for any of the other northwest sites. The Snoqualmie data was collected on a Wednesday and Thursday (and averaged), while the Pocono data was collected on a Tuesday. The volume profiles throughout the weekday for these two sites are shown in Exhibit 6.

Exhibit 6: Weekday Casino Volume Profiles


The weekday AM and PM peak trip generation rates were derived by averaging the rates from both sites, as shown in Table 4.

Table 4: Casino Weekday Trip Generation Rates

| Casino | AM Peak Time | Trip Rate <br> (trips/gaming position) | PM Peak Time | Trip Rate <br> (trips/gaming position) |
| :---: | :---: | :---: | :---: | :---: |
| Snoqualmie (October 2012) | $8: 00 \mathrm{AM}$ | 0.15 | $5: 00 \mathrm{PM}$ | 0.39 |
| Pocono Downs (2007 data) | $8: 00 \mathrm{AM}$ | 0.16 | $4: 00 \mathrm{PM}$ | 0.41 |
|  | Average | 0.15 | Average | 0.40 |

## Directional Split of Trips to and from Site

After identifying trip generation rates for each time period, the directional split of trips to and from the site during each time period was analyzed using the data collected from the seven casinos. The split of trips in and out of each site during the three analysis periods is provided in Table 5.

Table 5: Casino Weekday Trip Generation Rates

| Casino | Time Period |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Weekend Peak |  | Weekday AM |  | Weekday PM |  |
|  | In | Out | In | Out | In | Out |
| Snoqualmie (September 2012) | 62\% | 38\% |  |  |  |  |
| Snoqualmie (October 2012) | 58\% | 42\% | 54\% | 46\% | 55\% | 45\% |
| Pocono (2007 data) | 45\% | 55\% | 59\% | 41\% | 38\% | 62\% |
| Pocono (2009 data) | 61\% | 39\% |  |  |  |  |
| Spirit Mountain | 47\% | 53\% |  |  |  |  |
| 7 Feathers | 53\% | 47\% |  |  |  |  |
| Muckleshoot | 56\% | 44\% |  |  |  |  |
| Tulalip | 61\% | 39\% |  |  |  |  |
| Northern Quest | 59\% | 41\% |  |  |  |  |
| Minimum | 39\% | 39\% | 54\% | 41\% | 38\% | 45\% |
| Maximum | 61\% | 61\% | 59\% | 46\% | 55\% | 62\% |
| Average (Snoqualmie Data) | 60\% | 40\% |  |  |  |  |
| Average (All Data) | 55\% | 45\% | 57\% | 43\% | 47\% | 53\% |

As seen in the table, the proportion of trips in and out of each casino varies notably from site to site. The directional split of trips at the Snoqualmie site during the weekend peak shows trips in to the casino as the dominant movement. The average directional split calculated from all sites also shows trips in as the dominant movement. Therefore, it is proposed to use the average of the data collected at Snoqualmie ( $60 \%$ in and $40 \%$ out) to identify the directional split during the weekend peak period. During the weekday AM peak period, the directional split at Snoqualmie and Pocono both show trips in
to the site as the dominant movement. Therefore, it is proposed to use the average of both sites to develop the weekday AM peak period ( $57 \%$ in and $43 \%$ out). During the weekday PM peak period, data at Snoqualmie shows trips in as the dominant movement, while data at Pocono shows the reverse. Given the similarity between Snoqualmie and the proposed Cowlitz Reservation Development in terms of distance from a major metropolitan area, the development is likely to more closely remember Snoqualmie. Therefore, the directional distribution of trips during the weekday PM peak period proposed for the trip generation analysis is $55 \%$ in and $45 \%$ out (to match the data from Snoqualmie). The proposed directional splits of traffic are shown in Table 6.

Table 6: Proposed Cowlitz Reservation Development Trip Directional Splits

| Time Period | Directional Split |  |
| :--- | :---: | :---: |
|  | In | Out |
| Weekend Peak Period (Friday at 5:00 PM) | $60 \%$ | $40 \%$ |
| Weekday AM Peak Period | $57 \%$ | $43 \%$ |
| Weekday PM Peak Period | $55 \%$ | $45 \%$ |

## Trip Type

Lastly, the trip type was considered for the proposed development. Typically, a portion of trips to a commercial development will be pass-by or diverted trips. Pass-by trips represent patrons (and trips) that are currently traveling on the surrounding roadway network for some other primary purpose (such as a trip from work to home) and stop into the site en route during their normal travel. As such, pass-by trips do not result in a net increase in traffic on the surrounding transportation system and, typically, their only effect occurs at the immediate intersections and site driveways where they become turning movements. Diverted trips represent patrons (and trips) that are currently traveling on the roadway network in the site's vicinity, but must change their travel pattern to access the site. Therefore, diverted trips are not net new trips on the roadway network, but rather altered trips already on the network. All other trips to the site are considered net new trips, because they would not be present on the roadway network without the proposed development.

Traffic volumes and patterns in the vicinity of the site were reviewed to inform the assessment of trip type. Due to the relatively low volumes on NW $319^{\text {th }}$ Street which is immediately adjacent to the site, a small portion of trips generated by the proposed Cowlitz development are likely to be pass-by trips. A more significant portion of trips may be diverted from I-5 and use the interchange at La Center Road to access the site. These trips, although diverted, are still new trips to the local roadway network in the vicinity of the site.

In order to provide a conservative analysis, we are proposing to treat all trips to and from the site as net new trips. No adjustments will be made for pass-by or diverted trips.

## CONCLUSIONS

Peak trip generation rates for use in the proposed Cowlitz Reservation Development traffic analysis were derived based on a review of existing literature pertaining to casino trip generation and data collected at seven casinos. The proposed trip rates and directional splits to be used for the three identified peak hour time periods in the transportation impact analysis and IJR are summarized in Table 7.

Table 7: Proposed Cowlitz Reservation Development Trip Generation Rates and Directional Split

| Time Period | Trip Rate (trips/gaming position) | Directional Split |  |
| :---: | :---: | :---: | :---: |
|  |  | In | Out |
| Weekend Peak Period (Friday at 5:00 PM) | 0.48 | 60\% | 40\% |
| Weekday AM Peak Period | 0.15 | 57\% | 43\% |
| Weekday PM Peak Period | 0.40 | 55\% | 45s\% |

Please review this memorandum and provide us with any questions or comments by November 28, 2012 so that we may proceed with preparation of the respective studies in a timely manner. If you have questions, please contact us at (503) 228-5230.

## Appendix A Literature Review

## APPENDIX A: LITERATURE REVIEW

The literature review included the following studies:

Ackeret and Hosea. Trip Generation Rates for Las Vegas Area Hotel-Casinos. ITE Journal, May 1992.
This report summarized driveway counts conducted at various Las Vegas area casinos over a five-year period.

Box and Bunte. Gaming Casino Traffic. ITE Journal, March 1998.
This report summarized trip generation rates at the St. Charles Casino and Casino Queen, both located near St. Louis, MO based on the number of gaming positions.

## Trueblood and Gude. Trip Generation Characteristics of Small to Medium Sized Casinos. ITE Annual Meeting, 2001.

This report summarized rates at small to medium sized casinos in the Omaha metro area based on the number of slot machines.

Rowe, Kaseko, and Ackeret. Recalibration of Trip Generation Model for Las Vegas Hotel/Casinos. ITE Journal, May 2002.

This report summarized the trip generation of hotel-casinos in Las Vegas based on gaming positions, rooms, employees, and casino floor square footage.

Huntington and Butorac. Review of the Transportation Element of the Environmental Assessment for Cowlitz Indian Tribe. Kittelson \& Associates Report, June 7, 2004.

During the review of a TIA for another casino in the Pacific Northwest, KAI conducted counts at two similar casinos in the region, Northern Quest Casino and Tulalip Casino. Trip generation rates were developed based on the number of gaming machines.

Trip Generation, $9^{\text {th }}$ Edition. Institute of Transportation Engineers (ITE), 2012.
The ITE Trip Generation Manual was reviewed for casino land uses. It was determined that the only land use close to a casino in the manual, Casino/Video Lottery Establishment, was not an appropriate representation of the proposed Cascade Locks casino.

## Trip Generation Rates Summary

The following table is a summary of the trip generation rates found in the studies presented above. Specifically, the table summarizes rates for the Friday p.m. peak of the adjacent street using number of
gaming positions as the variable. A summary of Saturday peak hour rates is also included. However, only two of the studies summarized in this memorandum contained Saturday peak hour data and only one of those studies contained rates for the peak of the adjacent street.

|  | Average Trips per Gaming Position, Friday PM <br> Peak - Adj. Street | Average Trips per Gaming Position, Saturday |
| :--- | :--- | :--- |
| Casino St. Charles | 0.43 | 0.64 (Peak of Generator) |
| Casino Queen | 0.57 | $\mathrm{~N} / \mathrm{A}$ |
| Omaha Area | 0.59 | 0.64 (Peak of Adj. Street) |
| Vegas Local Casinos | 0.79 | $\mathrm{~N} / \mathrm{A}$ |
| Northern Quest | 0.49 | $\mathrm{~N} / \mathrm{A}$ |
| Tulalip Casino | 0.42 | $\mathrm{~N} / \mathrm{A}$ |
| Average | $\mathbf{0 . 5 5}$ | $\mathbf{0 . 6 4}$ |
| Average w/o Vegas | $\mathbf{0 . 5 0}$ | $\mathbf{0 . 6 4}$ |

As shown in the summary table, the average trip generation rate during the Friday p.m. peak hour is 0.55 vehicles/gaming position. If the Las Vegas casinos, which generally have different trip generation characteristics, are removed from the average, the resulting average is 0.50 vehicles/gaming position during the Friday p.m. peak hour. The Saturday peak hour average rate, although based on very limited data, is 0.64 vehicles/gaming position.

## Conclusions

After completing the literature review, we found that much of the national data was either incomplete or for casinos that were not similar in use, size, and geographic location to the Cowlitz Reservation Development (e.g. Las Vegas casinos and riverboat casinos). Although the literature review provided some interesting insights into the general trip generation characteristics of casinos, the rates provided in these studies did not necessarily reflect the rates of a tribal casino as is being proposed by Cowlitz. Some conclusions from the literature review include:

- Gaming positions correlate well with site trip generation and serve as a recommended independent variable.
- An entertainment venue in which concerts are held can also increase the trip generation potential of a casino.
- Casino/resort facilities located in Las Vegas and Reno are not indicative of trip generation potential for sites similar to the proposed development due to the sheer magnitude in size difference and the area in which they are located.
- Ancillary uses at a casino (i.e. restaurants, retail space) are encompassed in the casino's overall trip generation rate.
- The presence of an on-site hotel may reduce the casino's peak trip generation rate relative to sites without on-site housing.


## Appendix B Tube Count Volume Data Sheets from I-5/La Center Rd Ramps

| LOCATION: NW 319th St west of I-5 SB ramp SPECIFIC LOCATION: 0 ft from CITY/STATE: La Center, WA |  |  |  | QC JOB \#: 10797101DIRECTION: EB/WBDATE:Sep 14 2012-Sep 162012 |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Mon | Tue | Wed | Thu | $\begin{gathered} \text { Fri } \\ \text { 14-Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | $\begin{gathered} \text { Sat } \\ \text { 15-Sep-12 } \end{gathered}$ | $\begin{array}{\|c} \text { Sun-Sep-12 } \end{array}$ | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM |  |  |  |  | 1 | 1 | 18 | 18 | 12 | $\square$ |
| 1:00 AM |  |  |  |  | 2 | 2 | 11 | 22 | 12 | $\square$ |
| 2:00 AM |  |  |  |  | 3 | 3 | 6 | 0 | 3 | - |
| 3:00 AM |  |  |  |  | 2 | 2 | 2 | 8 | 4 | ] |
| 4:00 AM |  |  |  |  | 9 | 9 | 13 | 2 | 8 | $\square$ |
| 5:00 AM |  |  |  |  | 35 | 35 | 19 | 20 | 25 | $\square$ |
| 6:00 AM |  |  |  |  | 80 | 80 | 27 | 33 | 47 | $\square$ |
| 7:00 AM |  |  |  |  | 117 | 117 | 61 | 35 | 71 | $\square$ |
| 8:00 AM |  |  |  |  | 145 | 145 | 83 | 54 | 94 | $\square$ |
| 9:00 AM |  |  |  |  | 115 | 115 | 126 | 124 | 122 | $\square$ |
| 10:00 AM |  |  |  |  | 107 | 107 | 130 | 109 | 115 | $\square$ |
| 11:00 AM |  |  |  |  | 120 | 120 | 145 | 108 | 124 | $\square$ |
| 12:00 PM |  |  |  |  | 108 | 108 | 148 | 117 | 124 |  |
| 1:00 PM |  |  |  |  | 93 | 93 | 103 | 139 | 112 | $\square$ |
| 2:00 PM |  |  |  |  | 148 | 148 | 161 | 116 | 142 - |  |
| 3:00 PM |  |  |  |  | 166 | 166 - | 135 | 111 | 137 | - |
| 4:00 PM |  |  |  |  | 168 | 168 | 141 | 120 | 143 |  |
| 5:00 PM |  |  |  |  | 168 | 168 | 116 | 98 | 127 | - |
| 6:00 PM |  |  |  |  | 139 | 139 | 111 | 76 | 109 | ] |
| 7:00 PM |  |  |  |  | 90 | 90 | 78 | 62 | 77 | ] |
| 8:00 PM |  |  |  |  | 70 | 70 | 73 | 48 | 64 | ] |
| 9:00 PM |  |  |  |  | 33 | 33 | 54 | 21 | 36 |  |
| 10:00 PM |  |  |  |  | 35 | 35 | 45 | 12 | 31 |  |
| 11:00 PM |  |  |  |  | 15 | 15 | 19 | 5 | 13 | $\square$ |
| Day Total |  |  |  |  | 1969 | 1969 | 1825 | 1458 | 1752 |  |
| \% Weekday Average |  |  |  |  | 100.0\% |  |  |  |  |  |
| \% Week Average |  |  |  |  | 112.4\% | 112.4\% | 104.2\% | 83.2\% |  |  |
| AM Peak Volume |  |  |  |  | $\begin{gathered} 8: 00 \mathrm{AM} \\ 145 \end{gathered}$ | $\begin{gathered} 8: 00 \mathrm{AM} \\ 145 \end{gathered}$ | $\begin{gathered} \hline 11: 00 \mathrm{AM} \\ 145 \end{gathered}$ | $\begin{gathered} 9: 00 \mathrm{AM} \\ 124 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 124 \end{gathered}$ |  |
| PM Peak |  |  |  |  | 4:00 PM | 4:00 PM | 2:00 PM | 1:00 PM | 4:00 PM |  |
| Volume |  |  |  |  | 168 | 168 | 161 | 139 | 143 |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 10/8/2012 8:01 AM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net)

| LOCATION: NW 319th St west of I-5 SB ramp SPECIFIC LOCATION: 0 ft from CITY/STATE: La Center, WA |  |  |  |  |  |  |  |  | QC JOB \#: 10797101 <br> DIRECTION: EB/WB <br> DATE: Sep 17 2012 - Sep 23 2012 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | $\begin{gathered} \text { Mon } \\ 17-\text { Sep-12 } \end{gathered}$ | Tue 18-Sep-12 | Wed 19-Sep-12 | Thu 20-Sep-12 | $\begin{gathered} \text { Fri } \\ \text { 21-Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | $\begin{gathered} \text { Sat } \\ \text { 22-Sep-12 } \end{gathered}$ | $\begin{gathered} \text { Sun } \\ 23-\text { Sep-12 } \end{gathered}$ | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM | 1 | 6 | 3 | 11 | 11 | 6 | 10 | 30 | 10 | $\square$ |
| 1:00 AM | 9 | 1 | 2 | 0 | 2 | 3 | 20 | 15 | 7 | $\square$ |
| 2:00 AM | 6 | 5 | 2 | 4 | 5 | 4 | 3 | 2 | 4 | ] |
| 3:00 AM | 2 | 4 | 5 | 3 | 9 | 5 | 3 | 8 | 5 | ] |
| 4:00 AM | 16 | 11 | 5 | 13 | 18 | 13 | 4 | 1 | 10 | $\square$ |
| 5:00 AM | 30 | 41 | 31 | 35 | 30 | 33 | 17 | 0 | 26 | - |
| 6:00 AM | 89 | 68 | 74 | 68 | 87 | 77 | 23 | 12 | 60 | - |
| 7:00 AM | 124 | 158 | 145 | 159 | 137 | 145 | 69 | 28 | 117 |  |
| 8:00 AM | 89 | 105 | 158 | 141 | 116 | 122 | 117 | 73 | 114 |  |
| 9:00 AM | 97 | 96 | 71 | 77 | 75 | 83 | 88 | 98 | 86 | ] |
| 10:00 AM | 116 | 80 | 97 | 92 | 111 | 99 | 115 | 89 | 100 |  |
| 11:00 AM | 79 | 131 | 116 | 99 | 132 | 111 | 159 | 125 | 120 |  |
| 12:00 PM | 87 | 99 | 104 | 83 | 118 | 98 | 136 | 121 | 107 | ] |
| 1:00 PM | 108 | 132 | 102 | 123 | 124 | 118 | 114 | 163 | 124 |  |
| 2:00 PM | 105 | 111 | 87 | 114 | 149 | 113 | 138 | 104 | 115 | $\square$ |
| 3:00 PM | 101 | 135 | 147 | 156 | 142 | 136 | 117 | 92 | 127 |  |
| 4:00 PM | 123 | 134 | 146 | 112 | 136 | 130 | 133 | 98 | 126 |  |
| 5:00 PM | 117 | 129 | 140 | 129 | 143 | 132 | 116 | 93 | 124 |  |
| 6:00 PM | 115 | 88 | 102 | 112 | 140 | 111 | 110 | 77 | 106 | ] |
| 7:00 PM | 71 | 80 | 86 | 74 | 77 | 78 | 86 | 73 | 78 | ] |
| 8:00 PM | 44 | 50 | 38 | 59 | 35 | 45 | 76 | 41 | 49 | $\square$ |
| 9:00 PM | 25 | 39 | 30 | 35 | 46 | 35 | 42 | 44 | 37 |  |
| 10:00 PM | 31 | 23 | 11 | 26 | 49 | 28 | 33 | 19 | 27 |  |
| 11:00 PM | 4 | 6 | 7 | 7 | 24 | 10 | 34 | 3 | 12 | $\square$ |
| Day Total | 1589 | 1732 | 1709 | 1732 | 1916 | 1735 | 1763 | 1409 | 1691 |  |
| \% Weekday Average | 80.7\% | 99.8\% | 98.5\% | 99.8\% | 110.4\% |  |  |  |  |  |
| \% Week Average | 90.7\% | 102.4\% | 101.1\% | 102.4\% | 113.3\% | 102.6\% | 104.3\% | 83.3\% |  |  |
| AM Peak Volume | $\begin{gathered} 7: 00 \text { AM } \\ 124 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 158 \end{gathered}$ | $\begin{gathered} \text { 8:00 AM } \\ 158 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 159 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 137 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 145 \end{gathered}$ | $\begin{gathered} \hline 11: 00 \mathrm{AM} \\ 159 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 125 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 120 \end{gathered}$ |  |
| PM Peak Volume | $\begin{gathered} \text { 4:00 PM } \\ 123 \end{gathered}$ | $\begin{gathered} 3: 00 \text { PM } \\ 135 \end{gathered}$ | $\begin{gathered} \text { 3:00 PM } \\ 147 \end{gathered}$ | $\begin{gathered} \text { 3:00 PM } \\ 156 \end{gathered}$ | $\begin{gathered} \text { 2:00 PM } \\ 149 \end{gathered}$ | $\begin{gathered} \text { 3:00 PM } \\ 136 \end{gathered}$ | $\begin{gathered} \text { 2:00 PM } \\ 138 \end{gathered}$ | $\begin{gathered} 1: 00 \text { PM } \\ 163 \end{gathered}$ | $\begin{gathered} 3: 00 \text { PM } \\ 127 \end{gathered}$ |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 10/8/2012 8:01 AM


Report generated on 10/8/2012 8:01 AM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net)


Report generated on 10/8/2012 8:01 AM

| LOCATION: NW 319th St west of I-5 SB ramp SPECIFIC LOCATION: 0 ft from CITY/STATE: La Center, WA |  |  |  |  |  |  |  |  | QC JOB \#: 10797101DIRECTION: EB/WBDATE:Sep 10 2012-Sep 162012 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Mon $10-S e p-12$ | $\begin{gathered} \text { Tue } \\ \text { 11-Sep-12 } \end{gathered}$ | Wed 12-Sep-12 | Thu 13-Sep-12 | $\begin{gathered} \text { Fri } \\ \text { 14-Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | Sat 15-Sep-12 | $\underset{16-\text { Sun-12 }}{ }$ | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM | 1 | 6 | 3 | 11 | 1 | 4 | 18 | 18 | 8 | - |
| 1:00 AM | 9 | 1 | 2 | 0 | 2 | 3 | 11 | 22 | 7 | $\square$ |
| 2:00 AM | 6 | 5 | 2 | 4 | 3 | 4 | 6 | 0 | 4 | ] |
| 3:00 AM | 2 | 4 | 5 | 3 | 2 | 3 | 2 | 8 | 4 | ] |
| 4:00 AM | 16 | 11 | 5 | 13 | 9 | 11 | 13 | 2 | 10 | $\square$ |
| 5:00 AM | 30 | 41 | 31 | 35 | 35 | 34 | 19 | 20 | 30 | $\square$ |
| 6:00 AM | 89 | 68 | 74 | 68 | 80 | 76 | 27 | 33 | 63 |  |
| 7:00 AM | 124 | 158 | 145 | 159 | 117 | 141 | 61 | 35 | 114 |  |
| 8:00 AM | 89 | 105 | 158 | 141 | 145 | 128 | 83 | 54 | 111 |  |
| 9:00 AM | 97 | 96 | 71 | 77 | 115 | 91 | 126 | 124 | 101 | $\square$ |
| 10:00 AM | 116 | 80 | 97 | 92 | 107 | 98 | 130 | 109 | 104 |  |
| 11:00 AM | 79 | 131 | 116 | 99 | 120 | 109 | 145 | 108 | 114 |  |
| 12:00 PM | 87 | 99 | 104 | 83 | 108 | 96 | 148 | 117 | 107 | ] |
| 1:00 PM | 108 | 132 | 102 | 123 | 93 | 112 | 103 | 139 | 114 |  |
| 2:00 PM | 105 | 111 | 87 | 114 | 148 | 113 | 161 | 116 | 120 | - |
| 3:00 PM | 101 | 135 | 147 | 156 | 166 | 141 | 135 | 111 | 136 |  |
| 4:00 PM | 123 | 134 | 146 | 112 | 168 | 137 | 141 | 120 | 135 |  |
| 5:00 PM | 117 | 129 | 140 | 129 | 168 | 137 | 116 | 98 | 128 | I |
| 6:00 PM | 115 | 88 | 102 | 112 | 139 | 111 | 111 | 76 | 106 | ] |
| 7:00 PM | 71 | 80 | 86 | 74 | 90 | 80 | 78 | 62 | 77 | ] |
| 8:00 PM | 44 | 50 | 38 | 59 | 70 | 52 | 73 | 48 | 55 | $\square$ |
| 9:00 PM | 25 | 39 | 30 | 35 | 33 | 32 | 54 | 21 | 34 |  |
| 10:00 PM | 31 | 23 | 11 | 26 | 35 | 25 | 45 | 12 | 26 |  |
| 11:00 PM | 4 | 6 | 7 | 7 | 15 | 8 | 19 | 5 | 9 | $\square$ |
| Day Total | 1589 | 1732 | 1709 | 1732 | 1969 | 1746 | 1825 | 1458 | 1717 |  |
| \% Weekday Average | 91.0\% | 99.2\% | 97.9\% | 99.2\% | 112.8\% |  |  |  |  |  |
| \% Week Average | 92.5\% | 100.9\% | 99.5\% | 100.9\% | 114.7\% | 101.7\% | 106.3\% | 84.9\% |  |  |
| AM Peak Volume | 7:00 AM 124 | $\begin{gathered} 7: 00 \mathrm{AM} \\ 158 \end{gathered}$ | $\begin{gathered} 8: 00 \text { AM } \\ 158 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 159 \end{gathered}$ | $\begin{gathered} 8: 00 \mathrm{AM} \\ 145 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 141 \end{gathered}$ | $\begin{gathered} \hline 11: 00 \text { AM } \\ 145 \end{gathered}$ | $\begin{gathered} 9: 00 \mathrm{AM} \\ 124 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 114 \end{gathered}$ |  |
| PM Peak Volume | $\begin{gathered} \text { 4:00 PM } \\ 123 \end{gathered}$ | $\begin{gathered} \hline 3: 00 \mathrm{PM} \\ 135 \end{gathered}$ | $\begin{gathered} 3: 00 \mathrm{PM} \\ 147 \end{gathered}$ | $\begin{gathered} 3: 00 \mathrm{PM} \\ 156 \end{gathered}$ | $\begin{gathered} 4: 00 \text { PM } \\ 168 \end{gathered}$ | $\begin{gathered} \text { 3:00 PM } \\ 141 \end{gathered}$ | $\begin{gathered} \text { 2:00 PM } \\ 161 \end{gathered}$ | $\begin{gathered} 1: 00 \mathrm{PM} \\ 139 \end{gathered}$ | $\begin{gathered} \text { 3:00 PM } \\ 136 \end{gathered}$ |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 10/8/2012 8:01 AM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net)

| LOCATION: NW La Center Rd east of Paradise Park Rd SPECIFIC LOCATION: 0 ft from CITY/STATE: La Center, WA |  |  |  |  | QC JOB \#: 10797102DIRECTION: EB/WBDATE:Sep 14 2012-Sep 162012 |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Mon | Tue | Wed | Thu | $\begin{gathered} \text { Fri } \\ \text { 14-Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | $\begin{gathered} \text { Sat } \\ \text { 15-Sep-12 } \end{gathered}$ | $\begin{array}{\|c} \text { Sun-Sep-12 } \end{array}$ | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM |  |  |  |  | 137 | 137 | 173 | 191 | 167 | $\square$ |
| 1:00 AM |  |  |  |  | 91 | 91 | 155 | 124 | 123 | $\square$ |
| 2:00 AM |  |  |  |  | 89 | 89 | 100 | 89 | 93 | $\square$ |
| 3:00 AM |  |  |  |  | 85 | 85 | 88 | 82 | 85 | $\square$ |
| 4:00 AM |  |  |  |  | 166 | 166 | 110 | 99 | 125 | $\square$ |
| 5:00 AM |  |  |  |  | 277 | 277 | 160 | 100 | 179 | $\square$ |
| 6:00 AM |  |  |  |  | 536 | 536 | 182 | 158 | 292 |  |
| 7:00 AM |  |  |  |  | 784 | 784 | 308 | 250 | 447 |  |
| 8:00 AM |  |  |  |  | 644 | 644 | 417 | 279 | 447 |  |
| 9:00 AM |  |  |  |  | 498 | 498 | 507 | 430 | 478 |  |
| 10:00 AM |  |  |  |  | 492 | 492 | 579 | 486 | 519 | $\square$ |
| 11:00 AM |  |  |  |  | 568 | 568 | 625 | 464 | 552 | - |
| 12:00 PM |  |  |  |  | 574 | 574 | 677 | 583 | 611 |  |
| 1:00 PM |  |  |  |  | 619 | 619 | 675 | 580 | 625 |  |
| 2:00 PM |  |  |  |  | 674 | 674 | 667 | 546 | 629 | $\square$ |
| 3:00 PM |  |  |  |  | 869 | 869 | 690 | 599 | 719 | $\square$ |
| 4:00 PM |  |  |  |  | 848 | 848 | 723 | 630 | 734 |  |
| 5:00 PM |  |  |  |  | 895 | 895 | 680 | 586 | 720 | $\square$ |
| 6:00 PM |  |  |  |  | 784 | 784 | 599 | 571 | 651 | ] |
| 7:00 PM |  |  |  |  | 560 | 560 | 567 | 498 | 542 | I |
| 8:00 PM |  |  |  |  | 470 | 470 | 484 | 384 | 446 | - |
| 9:00 PM |  |  |  |  | 482 | 482 | 410 | 315 | 402 | I |
| 10:00 PM |  |  |  |  | 383 | 383 | 316 | 188 | 296 | ] |
| 11:00 PM |  |  |  |  | 281 | 281 | 268 | 180 | 243 |  |
| Day Total |  |  |  |  | 11806 | 11806 | 10160 | 8412 | 10125 |  |
| \% Weekday Average |  |  |  |  | 100.0\% |  |  |  |  |  |
| \% Week Average |  |  |  |  | 116.6\% | 116.6\% | 100.3\% | 83.1\% |  |  |
| AM Peak Volume |  |  |  |  | $\begin{gathered} 7: 00 \mathrm{AM} \\ 784 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 784 \end{gathered}$ | $\begin{aligned} & 11: 00 \text { AM } \\ & 625 \end{aligned}$ | $\begin{gathered} 10: 00 \text { AM } \\ 486 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 552 \end{gathered}$ |  |
| PM Peak |  |  |  |  | 5:00 PM | 5:00 PM | 4:00 PM | 4:00 PM | 4:00 PM |  |
| Volume |  |  |  |  | 895 | 895 | 723 | 630 | 734 |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 10/8/2012 8:02 AM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net)

| LOCATION: NW La Center Rd east of Paradise Park Rd SPECIFIC LOCATION: 0 ft from CITY/STATE: La Center, WA |  |  |  |  |  |  |  |  | QC JOB \#: 10797102DIRECTION: EB/WBDATE:Sep 17 2012-Sep 232012 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | $\begin{gathered} \text { Mon } \\ 17-\text { Sep-12 } \end{gathered}$ | Tue 18-Sep-12 | Wed 19-Sep-12 | Thu 20-Sep-12 | $\begin{gathered} \text { Fri } \\ 21-\text { Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | Sat <br> 22-Sep-12 | $\begin{gathered} \text { Sun } \\ 23-\text { Sep-12 } \end{gathered}$ | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM | 132 | 112 | 98 | 121 | 154 | 123 | 195 | 161 | 139 | ] |
| 1:00 AM | 80 | 71 | 87 | 85 | 90 | 83 | 124 | 127 | 95 | $\square$ |
| 2:00 AM | 65 | 57 | 92 | 78 | 75 | 73 | 132 | 120 | 88 | $\square$ |
| 3:00 AM | 88 | 89 | 77 | 80 | 89 | 85 | 101 | 89 | 88 | $\square$ |
| 4:00 AM | 165 | 133 | 149 | 142 | 137 | 145 | 99 | 87 | 130 | - |
| 5:00 AM | 321 | 308 | 309 | 311 | 267 | 303 | 142 | 91 | 250 |  |
| 6:00 AM | 575 | 583 | 594 | 554 | 551 | 571 | 209 | 136 | 457 | $\square$ |
| 7:00 AM | 770 | 827 | 785 | 744 | 735 | 772 | 343 | 263 | 638 |  |
| 8:00 AM | 592 | 659 | 665 | 624 | 604 | 629 | 424 | 317 | 555 | $\square$ |
| 9:00 AM | 536 | 460 | 443 | 448 | 521 | 482 | 465 | 436 | 473 |  |
| 10:00 AM | 440 | 420 | 463 | 419 | 492 | 447 | 571 | 427 | 462 |  |
| 11:00 AM | 483 | 503 | 457 | 480 | 553 | 495 | 614 | 475 | 509 |  |
| 12:00 PM | 501 | 448 | 505 | 480 | 556 | 498 | 580 | 533 | 515 | - |
| 1:00 PM | 499 | 506 | 514 | 566 | 600 | 537 | 589 | 563 | 548 |  |
| 2:00 PM | 545 | 640 | 597 | 624 | 736 | 628 | 635 | 626 | 629 | - |
| 3:00 PM | 764 | 758 | 759 | 817 | 826 | 785 | 669 | 637 | 747 |  |
| 4:00 PM | 788 | 865 | 886 | 850 | 864 | 851 | 668 | 549 | 781 | I |
| 5:00 PM | 922 | 913 | 945 | 929 | 919 | 926 | 653 | 568 | 836 |  |
| 6:00 PM | 745 | 705 | 700 | 776 | 838 | 753 | 577 | 509 | 693 | ] |
| 7:00 PM | 505 | 582 | 587 | 578 | 556 | 562 | 460 | 459 | 532 | - |
| 8:00 PM | 394 | 460 | 438 | 435 | 418 | 429 | 441 | 407 | 428 | ] |
| 9:00 PM | 304 | 352 | 304 | 347 | 517 | 365 | 393 | 259 | 354 | $\square$ |
| 10:00 PM | 200 | 216 | 207 | 248 | 380 | 250 | 331 | 206 | 255 | $\square$ |
| 11:00 PM | 170 | 184 | 210 | 203 | 297 | 213 | 280 | 184 | 218 | - |
| Day Total | 10584 | 10851 | 10871 | 10939 | 11775 | 11005 | 9695 | 8229 | 10420 |  |
| \% Weekday Average | 89.6\% | 98.6\% | 98.8\% | 99.4\% | 107.0\% |  |  |  |  |  |
| \% Week Average | 104.5\% | 104.1\% | 104.3\% | 105.0\% | 113.0\% | 105.6\% | 93.0\% | 79.0\% |  |  |
| AM Peak | 7:00 AM | 7:00 AM | 7:00 AM | 7:00 AM | 7:00 AM | 7:00 AM | 11:00 AM | 11:00 AM | 7:00 AM |  |
| Volume | 770 | 827 | 785 | 744 | 735 | 772 | 614 | 475 | 638 |  |
| PM Peak Volume | $\begin{gathered} \text { 5:00 PM } \\ 922 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 913 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 945 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 929 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 919 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 926 \end{gathered}$ | $\begin{gathered} 3: 00 \text { PM } \\ 669 \end{gathered}$ | $\begin{gathered} 3: 00 \text { PM } \\ 637 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 836 \end{gathered}$ |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 10/8/2012 8:02 AM


Report generated on 10/8/2012 8:02 AM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net)


| LOCATION: NW La Center Rd east of Paradise Park Rd SPECIFIC LOCATION: 0 ft from CITY/STATE: La Center, WA |  |  |  |  |  |  |  |  | QC JOB \#: 10797102DIRECTION: EB/WBDATE: $\operatorname{Sep} 10$ 2012 - Sep 162012 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | $\begin{gathered} \text { Mon } \\ 10-\text { Sep-12 } \end{gathered}$ | Tue 11-Sep-12 | Wed 12-Sep-12 | Thu <br> 13-Sep-12 | $\begin{gathered} \text { Fri } \\ \text { 14-Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | Sat 15-Sep-12 | $\begin{gathered} \text { Sun } \\ 16-\text { Sep-12 } \end{gathered}$ | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM | 132 | 112 | 98 | 121 | 137 | 120 | 173 | 191 | 138 |  |
| 1:00 AM | 80 | 71 | 87 | 85 | 91 | 83 | 155 | 124 | 99 | - |
| 2:00 AM | 65 | 57 | 92 | 78 | 89 | 76 | 100 | 89 | 81 | $\square$ |
| 3:00 AM | 88 | 89 | 77 | 80 | 85 | 84 | 88 | 82 | 84 | ] |
| 4:00 AM | 165 | 133 | 149 | 142 | 166 | 151 | 110 | 99 | 138 | $\square$ |
| 5:00 AM | 321 | 308 | 309 | 311 | 277 | 305 | 160 | 100 | 255 |  |
| 6:00 AM | 575 | 583 | 594 | 554 | 536 | 568 | 182 | 158 | 455 | $\square$ |
| 7:00 AM | 770 | 827 | 785 | 744 | 784 | 782 | 308 | 250 | 638 |  |
| 8:00 AM | 592 | 659 | 665 | 624 | 644 | 637 | 417 | 279 | 554 | $\square$ |
| 9:00 AM | 536 | 460 | 443 | 448 | 498 | 477 | 507 | 430 | 475 |  |
| 10:00 AM | 440 | 420 | 463 | 419 | 492 | 447 | 579 | 486 | 471 | $\square$ |
| 11:00 AM | 483 | 503 | 457 | 480 | 568 | 498 | 625 | 464 | 511 |  |
| 12:00 PM | 501 | 448 | 505 | 480 | 574 | 502 | 677 | 583 | 538 |  |
| 1:00 PM | 499 | 506 | 514 | 566 | 619 | 541 | 675 | 580 | 566 |  |
| 2:00 PM | 545 | 640 | 597 | 624 | 674 | 616 | 667 | 546 | 613 | $\square$ |
| 3:00 PM | 764 | 758 | 759 | 817 | 869 | 793 | 690 | 599 | 751 | $\square$ |
| 4:00 PM | 788 | 865 | 886 | 850 | 848 | 847 | 723 | 630 | 799 | $\square$ |
| 5:00 PM | 922 | 913 | 945 | 929 | 895 | 921 | 680 | 586 | 839 | $\square$ |
| 6:00 PM | 745 | 705 | 700 | 776 | 784 | 742 | 599 | 571 | 697 | ] |
| 7:00 PM | 505 | 582 | 587 | 578 | 560 | 562 | 567 | 498 | 554 | $\square$ |
| 8:00 PM | 394 | 460 | 438 | 435 | 470 | 439 | 484 | 384 | 438 | ] |
| 9:00 PM | 304 | 352 | 304 | 347 | 482 | 358 | 410 | 315 | 359 | 」 |
| 10:00 PM | 200 | 216 | 207 | 248 | 383 | 251 | 316 | 188 | 251 |  |
| 11:00 PM | 170 | 184 | 210 | 203 | 281 | 210 | 268 | 180 | 214 | $\square$ |
| Day Total | 10584 | 10851 | 10871 | 10939 | 11806 | 11010 | 10160 | 8412 | 10518 |  |
| \% Weekday Average | 96.1\% | 98.6\% | 98.7\% | 99.4\% | 107.2\% |  |  |  |  |  |
| \% Week Average | 100.6\% | 103.2\% | 103.4\% | 104.0\% | 112.2\% | 104.7\% | 96.6\% | 80.0\% |  |  |
| AM Peak Volume | $\begin{gathered} \text { 7:00 AM } \\ 770 \end{gathered}$ | $\begin{aligned} & 7: 00 \mathrm{AM} \\ & 827 \end{aligned}$ | $\begin{aligned} & 7: 00 \mathrm{AM} \\ & 785 \end{aligned}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 744 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 784 \end{gathered}$ | $\begin{gathered} \text { 7:00 AM } \\ 782 \end{gathered}$ | $\begin{aligned} & 11: 00 \text { AM } \\ & 625 \end{aligned}$ | $\begin{gathered} 10: 00 \text { AM } \\ 486 \end{gathered}$ | $\begin{gathered} \text { 7:00 AM } \\ 638 \end{gathered}$ |  |
| PM Peak Volume | 5:00 PM 922 | $\begin{gathered} \text { 5:00 PM } \\ 913 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 945 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 929 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 895 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 921 \end{gathered}$ | $\begin{gathered} \text { 4:00 PM } \\ 723 \end{gathered}$ | $\begin{gathered} \text { 4:00 PM } \\ 630 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 839 \end{gathered}$ |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 10/8/2012 8:02 AM

| LOCATION: I-5 NB on-ramp at La Center Rd SPECIFIC LOCATION: 0 ft from CITY/STATE: La Center, WA |  |  |  |  |  |  |  |  | QC JOB \#: 10797105DIRECTION: NBDATE: Sep 182012 - Sep 232012 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Mon | Tue 18-Sep-12 | Wed 19-Sep-12 | Thu 20-Sep-12 | $\begin{gathered} \text { Fri } \\ 21-\text { Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | $\begin{gathered} \text { Sat } \\ \text { 22-Sep-12 } \end{gathered}$ | $\begin{gathered} \text { Sun } \\ 23-\text { Sep-12 } \end{gathered}$ | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM |  | 12 | 16 | 10 | 22 | 15 | 14 | 16 | 15 | $\square$ |
| 1:00 AM |  | 11 | 16 | 10 | 9 | 12 | 12 | 14 | 12 | $\square$ |
| 2:00 AM |  | 18 | 15 | 17 | 14 | 16 | 19 | 10 | 16 |  |
| 3:00 AM |  | 29 | 19 | 19 | 21 | 22 | 10 | 10 | 18 | - |
| 4:00 AM |  | 23 | 36 | 32 | 36 | 32 | 10 | 17 | 26 | - |
| 5:00 AM |  | 54 | 70 | 60 | 52 | 59 | 31 | 18 | 48 | $\square$ |
| 6:00 AM |  | 126 | 115 | 116 | 116 | 118 | 45 | 30 | 91 |  |
| 7:00 AM |  | 156 | 153 | 137 | 128 | 144 | 78 | 43 | 116 |  |
| 8:00 AM |  | 137 | 113 | 129 | 121 | 125 | 97 | 75 | 112 |  |
| 9:00 AM |  | 122 | 105 | 96 | 91 | 104 | 91 | 101 | 101 |  |
| 10:00 AM |  | 79 | 109 | 131 | 116 | 109 | 113 | 101 | 108 |  |
| 11:00 AM |  | 124 | 118 | 61 | 129 | 108 | 100 | 86 | 103 |  |
| 12:00 PM |  | 85 | 80 | 105 | 122 | 98 | 122 | 119 | 106 |  |
| 1:00 PM |  | 119 | 113 | 95 | 107 | 109 | 128 | 90 | 109 |  |
| 2:00 PM |  | 101 | 116 | 108 | 114 | 110 | 96 | 127 | 110 | $\square$ |
| 3:00 PM |  | 143 | 151 | 151 | 170 | 154 | 103 | 84 | $134-$ |  |
| 4:00 PM |  | 152 | 136 | 141 | 155 | 146 | 99 | 105 | 131 |  |
| 5:00 PM |  | 118 | 145 | 107 | 137 | 127 | 96 | 86 | 115 | - |
| 6:00 PM |  | 100 | 84 | 100 | 107 | 98 | 87 | 80 | 93 |  |
| 7:00 PM |  | 86 | 58 | 101 | 87 | 83 | 58 | 66 | 76 | , |
| 8:00 PM |  | 35 | 51 | 58 | 46 | 48 | 55 | 48 | 49 | $\square$ |
| 9:00 PM |  | 29 | 49 | 39 | 132 | 62 | 47 | 47 | 57 |  |
| 10:00 PM |  | 24 | 18 | 22 | 42 | 27 | 25 | 20 | 25 | - |
| 11:00 PM |  | 17 | 23 | 14 | 24 | 20 | 26 | 16 | 20 |  |
| Day Total |  | 1900 | 1909 | 1859 | 2098 | 1946 | 1562 | 1409 | 1791 |  |
| \% Weekday Average |  | 97.6\% | 98.1\% | 95.5\% | 107.8\% |  |  |  |  |  |
| \% Week Average |  | 106.1\% | 106.6\% | 103.8\% | 117.1\% | 108.7\% | 87.2\% | 78.7\% |  |  |
| AM Peak Volume |  | $\begin{gathered} 7: 00 \mathrm{AM} \\ 156 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 153 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 137 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 129 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 144 \end{gathered}$ | $\begin{gathered} 10: 00 \mathrm{AM} \\ 113 \end{gathered}$ | $\begin{gathered} 9: 00 \mathrm{AM} \\ 101 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 116 \end{gathered}$ |  |
| PM Peak Volume |  | $\begin{gathered} \text { 4:00 PM } \\ 152 \end{gathered}$ | $\begin{gathered} \text { 3:00 PM } \\ 151 \end{gathered}$ | $\begin{gathered} \hline 3: 00 \text { PM } \\ 151 \\ \hline \end{gathered}$ | $\begin{gathered} \text { 3:00 PM } \\ 170 \end{gathered}$ | $\begin{gathered} \text { 3:00 PM } \\ 154 \end{gathered}$ | $\begin{gathered} 1: 00 \text { PM } \\ 128 \end{gathered}$ | $\begin{gathered} \text { 2:00 PM } \\ 127 \end{gathered}$ | $\begin{gathered} 3: 00 \text { PM } \\ 134 \end{gathered}$ |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 10/8/2012 8:02 AM


Report generated on 10/8/2012 8:02 AM


Report generated on 10/8/2012 8:02 AM


Report generated on 10/8/2012 8:02 AM

| LOCATION: I-5 NB on-ramp at La Center Rd SPECIFIC LOCATION: 0 ft from CITY/STATE: La Center, WA |  |  |  |  |  |  |  |  | QC JOB \#: 10797105 <br> DIRECTION: NB <br> DATE: $\operatorname{Sep} 17$ 2012-Sep 232012 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | $\begin{gathered} \text { Mon } \\ \text { 17-Sep-12 } \end{gathered}$ | Tue 18-Sep-12 | Wed 19-Sep-12 | Thu 20-Sep-12 | $\begin{gathered} \text { Fri } \\ 21-\text { Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | $\begin{gathered} \text { Sat } \\ \text { 22-Sep-12 } \end{gathered}$ | $\begin{gathered} \text { Sun } \\ 23-\text { Sep-12 } \end{gathered}$ | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM | 20 | 12 | 16 | 10 | 22 | 16 | 14 | 16 | 16 | ] |
| 1:00 AM | 9 | 11 | 16 | 10 | 9 | 11 | 12 | 14 | 12 | $\square$ |
| 2:00 AM | 6 | 18 | 15 | 17 | 14 | 14 | 19 | 10 | 14 | - |
| 3:00 AM | 19 | 29 | 19 | 19 | 21 | 21 | 10 | 10 | 18 | $\square$ |
| 4:00 AM | 51 | 23 | 36 | 32 | 36 | 36 | 10 | 17 | 29 |  |
| 5:00 AM | 64 | 54 | 70 | 60 | 52 | 60 | 31 | 18 | 50 |  |
| 6:00 AM | 105 | 126 | 115 | 116 | 116 | 116 | 45 | 30 | 93 |  |
| 7:00 AM | 145 | 156 | 153 | 137 | 128 | 144 | 78 | 43 | 120 |  |
| 8:00 AM | 120 | 137 | 113 | 129 | 121 | 124 | 97 | 75 | 113 |  |
| 9:00 AM | 104 | 122 | 105 | 96 | 91 | 104 | 91 | 101 | 101 | , |
| 10:00 AM | 106 | 79 | 109 | 131 | 116 | 108 | 113 | 101 | 108 | - |
| 11:00 AM | 117 | 124 | 118 | 61 | 129 | 110 | 100 | 86 | 105 | , |
| 12:00 PM | 102 | 85 | 80 | 105 | 122 | 99 | 122 | 119 | 105 | , |
| 1:00 PM | 83 | 119 | 113 | 95 | 107 | 103 | 128 | 90 | 105 | ] |
| 2:00 PM | 0 | 101 | 116 | 108 | 114 | 88 | 96 | 127 | 95 | $\square$ |
| 3:00 PM | 0 | 143 | 151 | 151 | 170 | 123 | 103 | 84 | 115 | - |
| 4:00 PM | 120 | 152 | 136 | 141 | 155 | 141 | 99 | 105 | 130 |  |
| 5:00 PM | 99 | 118 | 145 | 107 | 137 | 121 | 96 | 86 | 113 | 1 |
| 6:00 PM | 89 | 100 | 84 | 100 | 107 | 96 | 87 | 80 | 92 | ] |
| 7:00 PM | 67 | 86 | 58 | 101 | 87 | 80 | 58 | 66 | 75 | 」 |
| 8:00 PM | 33 | 35 | 51 | 58 | 46 | 45 | 55 | 48 | 47 | - |
| 9:00 PM | 27 | 29 | 49 | 39 | 132 | 55 | 47 | 47 | 53 |  |
| 10:00 PM | 23 | 24 | 18 | 22 | 42 | 26 | 25 | 20 | 25 |  |
| 11:00 PM | 19 | 17 | 23 | 14 | 24 | 19 | 26 | 16 | 20 | $\square$ |
| Day Total | 1528 | 1900 | 1909 | 1859 | 2098 | 1860 | 1562 | 1409 | 1754 |  |
| \% Weekday Average | 82.2\% | 102.2\% | 102.6\% | 99.9\% | 112.8\% |  |  |  |  |  |
| \% Week Average | 87.1\% | 108.3\% | 108.8\% | 106.0\% | 119.6\% | 106.0\% | 89.1\% | 80.3\% |  |  |
| AM Peak Volume | $\begin{gathered} 7: 00 \text { AM } \\ 145 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 156 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 153 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 137 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 129 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 144 \end{gathered}$ | $\begin{gathered} \hline 10: 00 \mathrm{AM} \\ 113 \end{gathered}$ | $\begin{gathered} 9: 00 \mathrm{AM} \\ 101 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 120 \end{gathered}$ |  |
| PM Peak Volume | $\begin{gathered} \text { 4:00 PM } \\ 120 \end{gathered}$ | $\begin{gathered} \text { 4:00 PM } \\ 152 \end{gathered}$ | $\begin{gathered} \hline 3: 00 \text { PM } \\ 151 \end{gathered}$ | $\begin{gathered} \hline 3: 00 \text { PM } \\ 151 \end{gathered}$ | $\begin{gathered} \text { 3:00 PM } \\ 170 \end{gathered}$ | $\begin{gathered} 4: 00 \text { PM } \\ 141 \end{gathered}$ | $\begin{gathered} 1: 00 \text { PM } \\ 128 \end{gathered}$ | $\begin{gathered} \text { 2:00 PM } \\ 127 \end{gathered}$ | $\begin{gathered} \text { 4:00 PM } \\ 130 \end{gathered}$ |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 10/8/2012 8:02 AM

| LOCATION: I-5 NB off-ramp at La Center Rd SPECIFIC LOCATION: 0 ft from CITY/STATE: La Center, WA |  |  |  |  |  |  |  |  | QC JOB \#: 10797106DIRECTION: NBDATE: Sep 14 2012 - Sep 162012 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Mon | Tue | Wed | Thu | $\begin{gathered} \text { Fri } \\ \text { 14-Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | Sat 15-Sep-12 | $\underset{16-\text { Sun-12 }}{ }$ | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM |  |  |  |  | 62 | 62 | 89 | 101 | 84 | ] |
| 1:00 AM |  |  |  |  | 33 | 33 | 63 | 56 | 51 | $\square$ |
| 2:00 AM |  |  |  |  | 46 | 46 | 41 | 33 | 40 | $\square$ |
| 3:00 AM |  |  |  |  | 37 | 37 | 35 | 17 | 30 | - |
| 4:00 AM |  |  |  |  | 31 | 31 | 15 | 21 | 22 | $\square$ |
| 5:00 AM |  |  |  |  | 51 | 51 | 36 | 29 | 39 | $\square$ |
| 6:00 AM |  |  |  |  | 85 | 85 | 50 | 43 | 59 | - |
| 7:00 AM |  |  |  |  | 182 | 182 | 105 | 83 | 123 |  |
| 8:00 AM |  |  |  |  | 158 | 158 | 120 | 77 | 118 |  |
| 9:00 AM |  |  |  |  | 210 | 210 | 142 | 99 | 150 | $\square$ |
| 10:00 AM |  |  |  |  | 174 | 174 | 191 | 133 | 166 | $\square$ |
| 11:00 AM |  |  |  |  | 217 | 217 | 228 | 199 | 215 |  |
| 12:00 PM |  |  |  |  | 273 | 273 | 278 | 242 | 264 | $\square$ |
| 1:00 PM |  |  |  |  | 305 | 305 | 285 | 286 | 292 |  |
| 2:00 PM |  |  |  |  | 332 | 332 | 340 | 311 | 328 | $\square$ |
| 3:00 PM |  |  |  |  | 487 | 487 - | 356 | 248 | 364 |  |
| 4:00 PM |  |  |  |  | 471 | 471 | 351 | 257 | 360 |  |
| 5:00 PM |  |  |  |  | 524 | 524 | 365 | 242 | 377 |  |
| 6:00 PM |  |  |  |  | 448 | 448 | 328 | 225 | 334 | ] |
| 7:00 PM |  |  |  |  | 313 | 313 | 297 | 214 | 275 | $\square$ |
| 8:00 PM |  |  |  |  | 323 | 323 | 272 | 168 | 254 | - |
| 9:00 PM |  |  |  |  | 282 | 282 | 252 | 137 | 224 | ] |
| 10:00 PM |  |  |  |  | 218 | 218 | 178 | 128 | 175 | ] |
| 11:00 PM |  |  |  |  | 157 | 157 | 153 | 73 | 128 | 1 |
| Day Total |  |  |  |  | 5419 | 5419 | 4570 | 3422 | 4472 |  |
| \% Weekday Average |  |  |  |  | 100.0\% |  |  |  |  |  |
| \% Week Average |  |  |  |  | 121.2\% | 121.2\% | 102.2\% | 76.5\% |  |  |
| AM Peak Volume |  |  |  |  | $\begin{gathered} 11: 00 \text { AM } \\ 217 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 217 \end{gathered}$ | $\begin{gathered} \hline 11: 00 \text { AM } \\ 228 \end{gathered}$ | $\begin{gathered} \hline 11: 00 \text { AM } \\ 199 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 215 \end{gathered}$ |  |
| PM Peak Volume |  |  |  |  | $\begin{gathered} \text { 5:00 PM } \\ 524 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 524 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 365 \end{gathered}$ | $\begin{gathered} 2: 00 \text { PM } \\ 311 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 377 \end{gathered}$ |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 10/8/2012 8:02 AM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net)

| LOCATION: I-5 NB off-ramp at La Center Rd SPECIFIC LOCATION: 0 ft from CITY/STATE: La Center, WA |  |  |  | QC JOB \#: 10797106DIRECTION: NBDATE:Sep 17 2012-Sep 232012 |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Mon 17-Sep-12 | $\begin{gathered} \text { Tue } \\ 18 \text {-Sep-12 } \end{gathered}$ | Wed 19-Sep-12 | $\begin{gathered} \text { Thu } \\ 20-\text { Sep-12 } \end{gathered}$ | $\begin{gathered} \text { Fri } \\ 21-\text { Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | Sat 22-Sep-12 | $\begin{gathered} \text { Sun } \\ 23-\text { Sep-12 } \end{gathered}$ | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM | 38 | 50 | 56 | 52 | 71 | 53 | 90 | 90 | 64 | ] |
| 1:00 AM | 34 | 32 | 40 | 37 | 45 | 38 | 57 | 44 | 41 | $\square$ |
| 2:00 AM | 19 | 34 | 26 | 31 | 25 | 27 | 29 | 56 | 31 | $\square$ |
| 3:00 AM | 18 | 30 | 21 | 37 | 32 | 28 | 31 | 14 | 26 | $\square$ |
| 4:00 AM | 30 | 21 | 27 | 27 | 21 | 25 | 25 | 17 | 24 | - |
| 5:00 AM | 39 | 49 | 43 | 52 | 42 | 45 | 35 | 26 | 41 | $\square$ |
| 6:00 AM | 72 | 89 | 78 | 67 | 97 | 81 | 53 | 32 | 70 | - |
| 7:00 AM | 137 | 180 | 158 | 171 | 176 | 164 | 112 | 93 | 147 |  |
| 8:00 AM | 141 | 215 | 167 | 221 | 173 | 183 | 91 | 69 | 154 |  |
| 9:00 AM | 154 | 170 | 159 | 173 | 165 | 164 | 129 | 117 | 152 |  |
| 10:00 AM | 163 | 143 | 175 | 202 | 185 | 174 | 174 | 115 | 165 |  |
| 11:00 AM | 195 | 247 | 244 | 230 | 237 | 231 | 265 | 198 | 231 |  |
| 12:00 PM | 216 | 211 | 246 | 222 | 264 | 232 | 264 | 243 | 238 | $\square$ |
| 1:00 PM | 264 | 236 | 260 | 282 | 267 | 262 | 252 | 236 | 257 |  |
| 2:00 PM | 292 | 310 | 299 | 295 | 340 | 307 | 299 | 334 | 310 | $\square$ |
| 3:00 PM | 379 | 379 | 390 | 425 | 417 | 398 | 362 | 333 | 384 | I |
| 4:00 PM | 448 | 456 | 479 | 506 | 470 | 472 | 294 | 281 | 419 | - |
| 5:00 PM | 585 | 553 | 521 | 529 | 562 | 550 | 331 | 281 | 480 |  |
| 6:00 PM | 456 | 410 | 435 | 501 | 484 | 457 | 300 | 256 | 406 | ] |
| 7:00 PM | 310 | 372 | 326 | 309 | 380 | 339 | 250 | 246 | 313 | I |
| 8:00 PM | 195 | 292 | 261 | 285 | 241 | 255 | 253 | 208 | 248 | I |
| 9:00 PM | 178 | 256 | 217 | 220 | 249 | 224 | 215 | 159 | 213 | $\square$ |
| 10:00 PM | 128 | 134 | 152 | 128 | 183 | 145 | 191 | 101 | 145 | ] |
| 11:00 PM | 82 | 78 | 119 | 102 | 144 | 105 | 146 | 103 | 111 |  |
| Day Total | 4573 | 4947 | 4899 | 5104 | 5270 | 4959 | 4248 | 3652 | 4670 |  |
| \% Weekday Average | 84.4\% | 99.8\% | 98.8\% | 102.9\% | 106.3\% |  |  |  |  |  |
| \% Week Average | 102.3\% | 105.9\% | 104.9\% | 109.3\% | 112.8\% | 106.2\% | 91.0\% | 78.2\% |  |  |
| AM Peak Volume | $\begin{gathered} \hline 11: 00 \mathrm{AM} \\ 195 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 247 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 244 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 230 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 237 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 231 \end{gathered}$ | $\begin{gathered} \hline 11: 00 \mathrm{AM} \\ 265 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 198 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 231 \end{gathered}$ |  |
| PM Peak Volume | $\begin{gathered} \text { 5:00 PM } \\ 585 \end{gathered}$ | $\begin{gathered} 5: 00 \mathrm{PM} \\ 553 \end{gathered}$ | $\begin{gathered} 5: 00 \mathrm{PM} \\ 521 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 529 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 562 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 550 \end{gathered}$ | $\begin{gathered} 3: 00 \text { PM } \\ 362 \end{gathered}$ | $\begin{gathered} 2: 00 \mathrm{PM} \\ 334 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 480 \end{gathered}$ |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 10/8/2012 8:02 AM


Report generated on 10/8/2012 8:02 AM


Report generated on 10/8/2012 8:02 AM

| LOCATION: I-5 NB off-ramp at La Center Rd SPECIFIC LOCATION: 0 ft from CITY/STATE: La Center, WA |  |  |  |  |  |  |  |  | QC JOB \#: 10797106DIRECTION: NBDATE: Sep 10 2012 - Sep 162012 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | $\begin{gathered} \text { Mon } \\ 10-\text { Sep-12 } \end{gathered}$ | Tue <br> 11-Sep-12 | Wed 12-Sep-12 | Thu <br> 13-Sep-12 | $\begin{gathered} \hline \text { Fri } \\ \text { 14-Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | Sat 15-Sep-12 | $\begin{gathered} \text { Sun } \\ 16-\text { Sep-12 } \end{gathered}$ | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM | 38 | 50 | 56 | 52 | 62 | 52 | 89 | 101 | 64 | $\square \square$ |
| 1:00 AM | 34 | 32 | 40 | 37 | 33 | 35 | 63 | 56 | 42 | $\square$ |
| 2:00 AM | 19 | 34 | 26 | 31 | 46 | 31 | 41 | 33 | 33 | $\square$ |
| 3:00 AM | 18 | 30 | 21 | 37 | 37 | 29 | 35 | 17 | 28 | $\square$ |
| 4:00 AM | 30 | 21 | 27 | 27 | 31 | 27 | 15 | 21 | 25 | $\square$ |
| 5:00 AM | 39 | 49 | 43 | 52 | 51 | 47 | 36 | 29 | 43 | $\square$ |
| 6:00 AM | 72 | 89 | 78 | 67 | 85 | 78 | 50 | 43 | 69 | - |
| 7:00 AM | 137 | 180 | 158 | 171 | 182 | 166 | 105 | 83 | 145 |  |
| 8:00 AM | 141 | 215 | 167 | 221 | 158 | 180 | 120 | 77 | 157 |  |
| 9:00 AM | 154 | 170 | 159 | 173 | 210 | 173 | 142 | 99 | 158 |  |
| 10:00 AM | 163 | 143 | 175 | 202 | 174 | 171 | 191 | 133 | 169 |  |
| 11:00 AM | 195 | 247 | 244 | 230 | 217 | 227 | 228 | 199 | 223 | - |
| 12:00 PM | 216 | 211 | 246 | 222 | 273 | 234 | 278 | 242 | 241 | - |
| 1:00 PM | 264 | 236 | 260 | 282 | 305 | 269 | 285 | 286 | 274 | $\square$ |
| 2:00 PM | 292 | 310 | 299 | 295 | 332 | 306 | 340 | 311 | 311 | $\square$ |
| 3:00 PM | 379 | 379 | 390 | 425 | 487 | 412 | 356 | 248 | 381 | $\square$ |
| 4:00 PM | 448 | 456 | 479 | 506 | 471 | 472 | 351 | 257 | 424 | $\square$ |
| 5:00 PM | 585 | 553 | 521 | 529 | 524 | 542 | 365 | 242 | 474 |  |
| 6:00 PM | 456 | 410 | 435 | 501 | 448 | 450 | 328 | 225 | 400 |  |
| 7:00 PM | 310 | 372 | 326 | 309 | 313 | 326 | 297 | 214 | 306 | ] |
| 8:00 PM | 195 | 292 | 261 | 285 | 323 | 271 | 272 | 168 | 257 | ] |
| 9:00 PM | 178 | 256 | 217 | 220 | 282 | 231 | 252 | 137 | 220 | , |
| 10:00 PM | 128 | 134 | 152 | 128 | 218 | 152 | 178 | 128 | 152 |  |
| 11:00 PM | 82 | 78 | 119 | 102 | 157 | 108 | 153 | 73 | 109 | $\square$ |
| Day Total | 4573 | 4947 | 4899 | 5104 | 5419 | 4989 | 4570 | 3422 | 4705 |  |
| \% Weekday Average | 91.7\% | 99.2\% | 98.2\% | 102.3\% | 108.6\% |  |  |  |  |  |
| \% Week Average | 97.2\% | 105.1\% | 104.1\% | 108.5\% | 115.2\% | 106.0\% | 97.1\% | 72.7\% |  |  |
| AM Peak Volume | $\begin{array}{\|c} \hline 11: 00 \mathrm{AM} \\ 195 \end{array}$ | $\begin{gathered} \text { 11:00 AM } \\ 247 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 244 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 230 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 217 \end{gathered}$ | $\begin{gathered} \text { 11:00 AM } \\ 227 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 228 \end{gathered}$ | $\begin{gathered} \hline 11: 00 \mathrm{AM} \\ 199 \end{gathered}$ | $\begin{gathered} \text { 11:00 AM } \\ 223 \end{gathered}$ |  |
| PM Peak Volume | $\begin{gathered} \text { 5:00 PM } \\ 585 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 553 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 521 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 529 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 524 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 542 \end{gathered}$ | $\begin{gathered} 5: 00 \text { PM } \\ 365 \end{gathered}$ | $\begin{gathered} \hline \text { 2:00 PM } \\ 311 \end{gathered}$ | $\begin{gathered} 5: 00 \text { PM } \\ 474 \end{gathered}$ |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 10/8/2012 8:02 AM


Report generated on 10/8/2012 8:02 AM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net)

| LOCATION: I-5 SB on-ramp at La Center Rd SPECIFIC LOCATION: 0 ft from CITY/STATE: La Center, WA |  |  |  |  |  |  |  |  | QC JOB \#: 10797107DIRECTION: SBDATE: Sep 17 2012 - Sep 232012 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Mon 17-Sep-12 | Tue 18-Sep-12 | Wed 19-Sep-12 | Thu 20-Sep-12 | $\begin{gathered} \text { Fri } \\ \text { 21-Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | $\begin{gathered} \text { Sat } \\ \text { 22-Sep-12 } \end{gathered}$ | $\begin{gathered} \text { Sun } \\ 23-\text { Sep-12 } \end{gathered}$ | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM | 82 | 58 | 50 | 71 | 69 | 66 | 88 | 81 | 71 | $\square$ |
| 1:00 AM | 52 | 35 | 53 | 51 | 38 | 46 | 61 | 76 | 52 | $\square$ |
| 2:00 AM | 43 | 37 | 52 | 44 | 55 | 46 | 62 | 59 | 50 | $\square$ |
| 3:00 AM | 60 | 58 | 68 | 47 | 61 | 59 | 59 | 54 | 58 | , |
| 4:00 AM | 126 | 115 | 130 | 109 | 110 | 118 | 70 | 56 | 102 |  |
| 5:00 AM | 270 | 273 | 239 | 243 | 218 | 249 | 90 | 58 | 199 |  |
| 6:00 AM | 434 | 421 | 447 | 417 | 431 | 430 | 122 | 83 | 336 |  |
| 7:00 AM | 495 | 544 | 494 | 507 | 484 | 505 | 179 | 126 | 404 |  |
| 8:00 AM | 360 | 361 | 409 | 371 | 358 | 372 | 258 | 187 | 329 | - |
| 9:00 AM | 319 | 257 | 266 | 258 | 319 | 284 | 288 | 219 | 275 |  |
| 10:00 AM | 245 | 240 | 245 | 244 | 259 | 247 | 263 | 231 | 247 | - |
| 11:00 AM | 248 | 231 | 232 | 225 | 235 | 234 | 310 | 219 | 243 |  |
| 12:00 PM | 234 | 202 | 214 | 220 | 250 | 224 | 241 | 239 | 229 |  |
| 1:00 PM | 208 | 222 | 213 | 247 | 233 | 225 | 231 | 215 | 224 |  |
| 2:00 PM | 237 | 224 | 225 | 238 | 280 | 241 | 233 | 219 | 237 | $\square$ |
| 3:00 PM | 245 | 227 | 258 | 274 | 293 | 259 | 236 | 239 | 253 | $\square$ |
| 4:00 PM | 234 | 281 | 267 | 234 | 288 | 261 | 260 | 199 | 252 |  |
| 5:00 PM | 229 | 234 | 252 | 240 | 230 | 237 | 236 | 211 | 233 | - |
| 6:00 PM | 179 | 187 | 195 | 197 | 204 | 192 | 189 | 178 | 190 | - |
| 7:00 PM | 112 | 122 | 174 | 152 | 160 | 144 | 154 | 161 | 148 | ] |
| 8:00 PM | 99 | 115 | 117 | 99 | 114 | 109 | 140 | 137 | 117 | $\square$ |
| 9:00 PM | 96 | 104 | 88 | 97 | 138 | 105 | 108 | 103 | 105 |  |
| 10:00 PM | 73 | 79 | 63 | 98 | 130 | 89 | 130 | 65 | 91 |  |
| 11:00 PM | 80 | 79 | 79 | 85 | 113 | 87 | 105 | 69 | 87 | - |
| Day Total | 4760 | 4706 | 4830 | 4768 | 5070 | 4829 | 4113 | 3484 | 4532 |  |
| \% Weekday Average | 90.8\% | 97.5\% | 100.0\% | 98.7\% | 105.0\% |  |  |  |  |  |
| \% Week <br> Average | 107.8\% | 103.8\% | 106.6\% | 105.2\% | 111.9\% | 106.6\% | 90.8\% | 76.9\% |  |  |
| AM Peak Volume | $\begin{gathered} \text { 7:00 AM } \\ 495 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 544 \end{gathered}$ | $\begin{gathered} 7: 00 \text { AM } \\ 494 \end{gathered}$ | $\begin{gathered} \text { 7:00 AM } \\ 507 \end{gathered}$ | $\begin{gathered} \text { 7:00 AM } \\ 484 \end{gathered}$ | $\begin{aligned} & \text { 7:00 AM } \\ & 505 \end{aligned}$ | $\begin{gathered} \hline 11: 00 \mathrm{AM} \\ 310 \end{gathered}$ | $\begin{gathered} \text { 10:00 AM } \\ 231 \end{gathered}$ | $\begin{gathered} \text { 7:00 AM } \\ 404 \end{gathered}$ |  |
| PM Peak Volume | 3:00 PM 245 | 4:00 PM 281 | 4:00 PM 267 | 3:00 PM 274 | $\begin{gathered} 3: 00 \text { PM } \\ 293 \end{gathered}$ | $\begin{gathered} \text { 4:00 PM } \\ 261 \end{gathered}$ | $\begin{gathered} \text { 4:00 PM } \\ 260 \end{gathered}$ | $\begin{gathered} \text { 12:00 PM } \\ 239 \end{gathered}$ | $\begin{gathered} 3: 00 \text { PM } \\ 253 \end{gathered}$ |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 10/8/2012 8:02 AM


Report generated on 10/8/2012 8:02 AM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net)


Report generated on 10/8/2012 8:02 AM

| Type of report: | ube Count - | Volume Data |  | SUMMARY - Tube Count - Volume Data (Week) |  |  |  |  |  | Page 5 of 5 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LOCATION: I-5 SB on-ramp at La Center Rd SPECIFIC LOCATION: 0 ft from CITY/STATE: La Center, WA |  |  |  |  |  |  |  |  | QC JOB \#: 10797107DIRECTION: SBDATE: Sep 10 2012 - Sep 162012 |  |
| Start Time | $\begin{gathered} \text { Mon } \\ 10-\text { Sep-12 } \end{gathered}$ | $\begin{gathered} \text { Tue } \\ \text { 11-Sep-12 } \end{gathered}$ | Wed 12-Sep-12 | Thu <br> 13-Sep-12 | $\begin{gathered} \text { Fri } \\ \text { 14-Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | $\begin{gathered} \text { Sat } \\ 15-\text { Sep-12 } \end{gathered}$ | $\begin{gathered} \text { Sun } \\ 16-\text { Sep-12 } \end{gathered}$ | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM | 82 | 58 | 50 | 71 | 63 | 65 | 89 | 96 | 73 |  |
| 1:00 AM | 52 | 35 | 53 | 51 | 66 | 51 | 72 | 73 | 57 | - |
| 2:00 AM | 43 | 37 | 52 | 44 | 52 | 46 | 57 | 54 | 48 | $\square$ |
| 3:00 AM | 60 | 58 | 68 | 47 | 56 | 58 | 57 | 53 | 57 | $\square$ |
| 4:00 AM | 126 | 115 | 130 | 109 | 122 | 120 | 85 | 70 | 108 |  |
| 5:00 AM | 270 | 273 | 239 | 243 | 220 | 249 | 97 | 56 | 200 | ] |
| 6:00 AM | 434 | 421 | 447 | 417 | 415 | 427 | 124 | 104 | 337 | $\square$ |
| 7:00 AM | 495 | 544 | 494 | 507 | 497 | 507 | 168 | 123 | 404 |  |
| 8:00 AM | 360 | 361 | 409 | 371 | 413 | 383 | 248 | 168 | 333 | ] |
| 9:00 AM | 319 | 257 | 266 | 258 | 304 | 281 | 290 | 236 | 276 |  |
| 10:00 AM | 245 | 240 | 245 | 244 | 300 | 255 | 311 | 277 | 266 |  |
| 11:00 AM | 248 | 231 | 232 | 225 | 300 | 247 | 295 | 234 | 252 | I |
| 12:00 PM | 234 | 202 | 214 | 220 | 215 | 217 | 316 | 245 | 235 | ] |
| 1:00 PM | 208 | 222 | 213 | 247 | 263 | 231 | 280 | 248 | 240 | I |
| 2:00 PM | 237 | 224 | 225 | 238 | 240 | 233 | 239 | 210 | 230 | $\square$ |
| 3:00 PM | 245 | 227 | 258 | 274 | 323 | 265 | 255 | 233 | 259 | - |
| 4:00 PM | 234 | 281 | 267 | 234 | 292 | 262 | 274 | 224 | 258 | I |
| 5:00 PM | 229 | 234 | 252 | 240 | 263 | 244 | 223 | 198 | 234 | ] |
| 6:00 PM | 179 | 187 | 195 | 197 | 216 | 195 | 218 | 190 | 197 | - |
| 7:00 PM | 112 | 122 | 174 | 152 | 161 | 144 | 167 | 168 | 151 | $\square$ |
| 8:00 PM | 99 | 115 | 117 | 99 | 136 | 113 | 166 | 130 | 123 | ] |
| 9:00 PM | 96 | 104 | 88 | 97 | 107 | 98 | 143 | 110 | 106 | ] |
| 10:00 PM | 73 | 79 | 63 | 98 | 116 | 86 | 104 | 67 | 86 |  |
| 11:00 PM | 80 | 79 | 79 | 85 | 103 | 85 | 87 | 77 | 84 | I |
| Day Total | 4760 | 4706 | 4830 | 4768 | 5243 | 4862 | 4365 | 3644 | 4614 |  |
| \% Weekday Average | 97.9\% | 96.8\% | 99.3\% | 98.1\% | 107.8\% |  |  |  |  |  |
| \% Week Average | 103.2\% | 102.0\% | 104.7\% | 103.3\% | 113.6\% | 105.4\% | 94.6\% | 79.0\% |  |  |
| AM Peak | 7:00 AM | 7:00 AM | 7:00 AM | 7:00 AM | 7:00 AM | 7:00 AM | 10:00 AM | 10:00 AM | 7:00 AM |  |
| Volume | 495 | 544 | 494 | 507 | 497 | 507 | 311 | 277 | 404 |  |
| PM Peak | 3:00 PM | 4:00 PM | 4:00 PM | 3:00 PM | 3:00 PM | 3:00 PM | 12:00 PM | 1:00 PM | 3:00 PM |  |
| Volume | 245 | 281 | 267 | 274 | 323 | 265 | 316 | 248 | 259 |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 10/8/2012 8:02 AM

| LOCATION: I-5 SB off-ramp at La Center Rd SPECIFIC LOCATION: 0 ft from CITY/STATE: La Center, WA |  |  |  |  |  |  |  |  | QC JOB \#: 10797108DIRECTION: SBDATE: Sep 142012 - Sep 162012 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Mon | Tue | Wed | Thu | $\begin{gathered} \text { Fri } \\ \text { 14-Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | $\begin{gathered} \text { Sat } \\ 15-\text { Sep-12 } \end{gathered}$ | $\underset{16-\text { Sun-12 }}{ }$ | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM |  |  |  |  | 12 | 12 | 12 | 15 | 13 | $\square$ |
| 1:00 AM |  |  |  |  | 15 | 15 | 15 | 15 | 15 | $\square$ |
| 2:00 AM |  |  |  |  | 7 | 7 | 10 | 9 | 9 | $\square$ |
| 3:00 AM |  |  |  |  | 19 | 19 | 10 | 8 | 12 | $\square$ |
| 4:00 AM |  |  |  |  | 9 | 9 | 9 | 3 | 7 | $\square$ |
| 5:00 AM |  |  |  |  | 28 | 28 | 10 | 6 | 15 | $\square$ |
| 6:00 AM |  |  |  |  | 50 | 50 | 25 | 13 | 29 | $\square$ |
| 7:00 AM |  |  |  |  | 87 | 87 | 44 | 27 | 53 |  |
| 8:00 AM |  |  |  |  | 66 | 66 | 42 | 30 | 46 | - |
| 9:00 AM |  |  |  |  | 69 | 69 | 97 | 64 | 77 | $\square$ |
| 10:00 AM |  |  |  |  | 79 | 79 | 112 | 92 | 94 | $\square$ |
| 11:00 AM |  |  |  |  | 115 | 115 | 110 | 105 | 110 |  |
| 12:00 PM |  |  |  |  | 106 | 106 | 114 | 115 | 112 | - |
| 1:00 PM |  |  |  |  | 140 | 140 | 126 | 129 | 132 | - |
| 2:00 PM |  |  |  |  | 162 | 162 | 108 | 113 | 128 |  |
| 3:00 PM |  |  |  |  | 143 | 143 | 112 | 116 | 124 - | $\square$ |
| 4:00 PM |  |  |  |  | 167 | 167 | 123 | 115 | 135 | - |
| 5:00 PM |  |  |  |  | 152 | 152 | 128 | 142 | 141 | , |
| 6:00 PM |  |  |  |  | 122 | 122 | 110 | 125 | 119 | - |
| 7:00 PM |  |  |  |  | 94 | 94 | 108 | 115 | 106 | , |
| 8:00 PM |  |  |  |  | 83 | 83 | 92 | 86 | 87 | $\square$ |
| 9:00 PM |  |  |  |  | 128 | 128 | 61 | 54 | 81 | I |
| 10:00 PM |  |  |  |  | 61 | 61 | 43 | 25 | 43 |  |
| 11:00 PM |  |  |  |  | 30 | 30 | 33 | 19 | 27 | 1 |
| Day Total |  |  |  |  | 1944 | 1944 | 1654 | 1541 | 1715 |  |
| \% Weekday Average |  |  |  |  | 100.0\% |  |  |  |  |  |
| \% Week Average |  |  |  |  | 113.4\% | 113.4\% | 96.4\% | 89.9\% |  |  |
| AM Peak Volume |  |  |  |  | $\begin{gathered} 11: 00 \mathrm{AM} \\ 115 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 115 \end{gathered}$ | $\begin{gathered} \hline 10: 00 \mathrm{AM} \\ 112 \end{gathered}$ | $\begin{gathered} \text { 11:00 AM } \\ 105 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 110 \end{gathered}$ |  |
| PM Peak Volume |  |  |  |  | $\begin{gathered} 4: 00 \text { PM } \\ 167 \end{gathered}$ | $\begin{gathered} \text { 4:00 PM } \\ 167 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 128 \end{gathered}$ | $\begin{gathered} 5: 00 \mathrm{PM} \\ 142 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 141 \end{gathered}$ |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 10/8/2012 8:02 AM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net)

| LOCATION: l-5 SB off-ramp at La Center Rd SPECIFIC LOCATION: 0 ft from CITY/STATE: La Center, WA |  |  |  |  |  |  |  |  | QC JOB \#: 10797108DIRECTION:SBDATE:Sep 17 2012-Sep 232012 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Mon 17-Sep-12 | $\begin{gathered} \text { Tue } \\ 18-\text { Sep-12 } \end{gathered}$ | Wed 19-Sep-12 | $\begin{gathered} \text { Thu } \\ 20-\text { Sep-12 } \end{gathered}$ | $\begin{gathered} \text { Fri } \\ \text { 21-Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | Sat 22-Sep-12 | $\begin{gathered} \text { Sun } \\ 23-\text { Sep-12 } \end{gathered}$ | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM | 8 | 12 | 5 | 14 | 11 | 10 | 13 | 11 | 11 | $\square$ |
| 1:00 AM | 7 | 8 | 17 | 7 | 5 | 9 | 17 | 6 | 10 | $\square$ |
| 2:00 AM | 8 | 4 | 10 | 8 | 9 | 8 | 7 | 4 | 7 | - |
| 3:00 AM | 12 | 7 | 12 | 3 | 16 | 10 | 12 | 8 | 10 | $\square$ |
| 4:00 AM | 9 | 10 | 15 | 18 | 16 | 14 | 2 | 9 | 11 | $\square$ |
| 5:00 AM | 21 | 39 | 29 | 25 | 27 | 28 | 12 | 3 | 22 | $\square$ |
| 6:00 AM | 49 | 42 | 53 | 60 | 59 | 53 | 20 | 16 | 43 | $\square$ |
| 7:00 AM | 78 | 101 | 90 | 79 | 81 | 86 | 40 | 26 | 71 |  |
| 8:00 AM | 59 | 60 | 81 | 63 | 68 | 66 | 53 | 43 | 61 |  |
| 9:00 AM | 72 | 76 | 52 | 64 | 58 | 64 | 59 | 54 | 62 |  |
| 10:00 AM | 83 | 71 | 75 | 61 | 79 | 74 | 100 | 82 | 79 |  |
| 11:00 AM | 100 | 85 | 78 | 75 | 97 | 87 | 94 | 89 | 88 | - |
| 12:00 PM | 84 | 91 | 104 | 104 | 108 | 98 | 114 | 106 | 102 |  |
| 1:00 PM | 107 | 113 | 93 | 99 | 135 | 109 | 118 | 159 | 118 |  |
| 2:00 PM | 114 | 139 | 117 | 135 | 137 | 128 | 103 | 111 | 122 | - |
| 3:00 PM | 139 | 142 | 160 | 144 | 149 | 147 - | -117 | 120 | 139 |  |
| 4:00 PM | 160 | 132 | 178 | 170 | 167 | 161 | 109 | 111 | 147 | ] |
| 5:00 PM | 174 | 172 | 173 | 216 | 183 | 184 | 129 | 118 | 166 |  |
| 6:00 PM | 116 | 137 | 101 | 127 | 188 | 134 | 96 | 110 | 125 | ] |
| 7:00 PM | 105 | 102 | 100 | 85 | 95 | 97 | 89 | 96 | 96 | ] |
| 8:00 PM | 74 | 60 | 60 | 54 | 74 | 64 | 67 | 59 | 64 | , |
| 9:00 PM | 52 | 47 | 50 | 47 | 67 | 53 | 71 | 41 | 54 | ] |
| 10:00 PM | 21 | 27 | 23 | 38 | 46 | 31 | 50 | 36 | 34 |  |
| 11:00 PM | 17 | 23 | 13 | 25 | 32 | 22 | 28 | 14 | 22 | $\square$ |
| Day Total | 1669 | 1700 | 1689 | 1721 | 1907 | 1737 | 1520 | 1432 | 1664 |  |
| \% Weekday Average | 85.9\% | 97.9\% | 97.2\% | 99.1\% | 109.8\% |  |  |  |  |  |
| \% Week Average | 97.3\% | 102.2\% | 101.5\% | 103.4\% | 114.6\% | 104.4\% | 91.3\% | 86.1\% |  |  |
| AM Peak Volume | $\begin{gathered} \hline 11: 00 \mathrm{AM} \\ 100 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 101 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 90 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 79 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 97 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 87 \end{gathered}$ | $\begin{gathered} 10: 00 \mathrm{AM} \\ 100 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 89 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 88 \end{gathered}$ |  |
| PM Peak Volume | $\begin{gathered} \text { 5:00 PM } \\ 174 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 172 \end{gathered}$ | $\begin{gathered} 4: 00 \text { PM } \\ 178 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 216 \end{gathered}$ | $\begin{gathered} \text { 6:00 PM } \\ 188 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 184 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 129 \end{gathered}$ | $\begin{gathered} 1: 00 \mathrm{PM} \\ 159 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 166 \end{gathered}$ |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 10/8/2012 8:02 AM


Report generated on 10/8/2012 8:02 AM


Report generated on 10/8/2012 8:02 AM

| Type of report: | be Count - | Volume Data |  | SUMMARY - Tube Count - Volume Data (Week) |  |  |  |  | Page 5 of 5QC JOB \#: 10797108DIRECTION: SBDATE: Sep 10 2012 - Sep 162012 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LOCATION: I-5 SB off-ramp at La Center Rd SPECIFIC LOCATION: 0 ft from CITY/STATE: La Center, WA |  |  |  |  |  |  |  |  |  |  |
| Start Time | $\begin{gathered} \text { Mon } \\ \text { 10-Sep-12 } \end{gathered}$ | Tue 11-Sep-12 | Wed 12-Sep-12 | Thu <br> 13-Sep-12 | $\begin{gathered} \text { Fri } \\ \text { 14-Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | $\begin{gathered} \text { Sat } \\ \text { 15-Sep-12 } \end{gathered}$ | $\begin{gathered} \text { Sun } \\ 16-\text { Sep-12 } \end{gathered}$ | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM | 8 | 12 | 5 | 14 | 12 | 10 | 12 | 15 | 11 | $\square$ |
| 1:00 AM | 7 | 8 | 17 | 7 | 15 | 11 | 15 | 15 | 12 | $\square$ |
| 2:00 AM | 8 | 4 | 10 | 8 | 7 | 7 | 10 | 9 | 8 | - |
| 3:00 AM | 12 | 7 | 12 | 3 | 19 | 11 | 10 | 8 | 10 | $\square$ |
| 4:00 AM | 9 | 10 | 15 | 18 | 9 | 12 | 9 | 3 | 10 | $\square$ |
| 5:00 AM | 21 | 39 | 29 | 25 | 28 | 28 | 10 | 6 | 23 | - |
| 6:00 AM | 49 | 42 | 53 | 60 | 50 | 51 | 25 | 13 | 42 |  |
| 7:00 AM | 78 | 101 | 90 | 79 | 87 | 87 | 44 | 27 | 72 | $\square$ |
| 8:00 AM | 59 | 60 | 81 | 63 | 66 | 66 | 42 | 30 | 57 | ] |
| 9:00 AM | 72 | 76 | 52 | 64 | 69 | 67 | 97 | 64 | 71 | $\square$ |
| 10:00 AM | 83 | 71 | 75 | 61 | 79 | 74 | 112 | 92 | 82 |  |
| 11:00 AM | 100 | 85 | 78 | 75 | 115 | 91 | 110 | 105 | 95 | $\square$ |
| 12:00 PM | 84 | 91 | 104 | 104 | 106 | 98 | 114 | 115 | 103 | - |
| 1:00 PM | 107 | 113 | 93 | 99 | 140 | 110 | 126 | 129 | 115 | I |
| 2:00 PM | 114 | 139 | 117 | 135 | 162 | 133 | 108 | 113 | 127 | I |
| 3:00 PM | 139 | 142 | 160 | 144 | 143 | 146 | 112 | 116 | 137 | $\square$ |
| 4:00 PM | 160 | 132 | 178 | 170 | 167 | 161 | 123 | 115 | 149 | - |
| 5:00 PM | 174 | 172 | 173 | 216 | 152 | 177 | 128 | 142 | 165 |  |
| 6:00 PM | 116 | 137 | 101 | 127 | 122 | 121 | 110 | 125 | 120 | ] |
| 7:00 PM | 105 | 102 | 100 | 85 | 94 | 97 | 108 | 115 | 101 | ] |
| 8:00 PM | 74 | 60 | 60 | 54 | 83 | 66 | 92 | 86 | 73 | - |
| 9:00 PM | 52 | 47 | 50 | 47 | 128 | 65 | 61 | 54 | 63 | ] |
| 10:00 PM | 21 | 27 | 23 | 38 | 61 | 34 | 43 | 25 | 34 | ] |
| 11:00 PM | 17 | 23 | 13 | 25 | 30 | 22 | 33 | 19 | 23 |  |
| Day Total | 1669 | 1700 | 1689 | 1721 | 1944 | 1745 | 1654 | 1541 | 1703 |  |
| \% Weekday Average | 95.6\% | 97.4\% | 96.8\% | 98.6\% | 111.4\% |  |  |  |  |  |
| \% Week Average | 98.0\% | 99.8\% | 99.2\% | 101.1\% | 114.2\% | 102.5\% | 97.1\% | 90.5\% |  |  |
| AM Peak Volume | $\begin{gathered} \hline 11: 00 \mathrm{AM} \\ 100 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 101 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{AM} \\ 90 \end{gathered}$ | $\begin{gathered} \text { 7:00 AM } \\ 79 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 115 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 91 \end{gathered}$ | $\begin{array}{\|c\|} \hline 10: 00 \mathrm{AM} \\ 112 \end{array}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 105 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 95 \end{gathered}$ |  |
| PM Peak Volume | 5:00 PM 174 | $\begin{gathered} \text { 5:00 PM } \\ 172 \end{gathered}$ | $\begin{gathered} \hline 4: 00 \text { PM } \\ 178 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 216 \end{gathered}$ | $\begin{gathered} 4: 00 \text { PM } \\ 167 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 177 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 128 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 142 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 165 \end{gathered}$ |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 10/8/2012 8:02 AM

## Appendix C Tube Count Volume Data Sheets from Snoqualmie

| LOCATION: Combined Volume-Main Driveway to Snoqualmie Casino north of roundabout at SE North Bend Way SPECIFIC LOCATION: 100 ft from North Bend Way CITY/STATE: Snoqualmie, WA |  |  |  |  |  |  |  |  | DIRECTION: NB <br> DATE: Sep 212012 - Sep 232012 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Mon | Tue | Wed | Thu | $\begin{gathered} \text { Fri } \\ 21-\text { Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | Sat 22-Sep-12 | $\begin{gathered} \text { Sun } \\ 23-\text { Sep-12 } \end{gathered}$ | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM |  |  |  |  | 43 | 43 | 77 | 365 | 162 | $\square$ |
| 1:00 AM |  |  |  |  | 43 | 43 | 69 | 276 | 129 | $\square$ |
| 2:00 AM |  |  |  |  | 16 | 16 | 38 | 222 | 92 | $\square$ |
| 3:00 AM |  |  |  |  | 18 | 18 | 21 | 153 | 64 |  |
| 4:00 AM |  |  |  |  | 15 | 15 | 19 | 91 | 42 | $\square$ |
| 5:00 AM |  |  |  |  | 34 | 34 | 51 | 55 | 47 | $\square$ |
| 6:00 AM |  |  |  |  | 47 | 47 | 69 | 60 | 59 | $\square$ |
| 7:00 AM |  |  |  |  | 79 | 79 | 164 | 68 | 104 | - |
| 8:00 AM |  |  |  |  | 101 | 101 | 174 | 124 | 133 |  |
| 9:00 AM |  |  |  |  | 153 | 153 | 260 | 55 | 156 |  |
| 10:00 AM |  |  |  |  | 210 | 210 | 183 | 0 | 131 | $\square$ |
| 11:00 AM |  |  |  |  | 253 | 253 | 192 | 0 | 148 | $\square$ |
| 12:00 PM |  |  |  |  | 261 | 261 | 240 | 0 | 167 |  |
| 1:00 PM |  |  |  |  | 237 | 237 | 271 | 0 | 169 | ] |
| 2:00 PM |  |  |  |  | 248 | 248 | 297 | 0 | 182 | - |
| 3:00 PM |  |  |  |  | 295 | 295 | 470 | 0 | 255 |  |
| 4:00 PM |  |  |  |  | 249 | 249 | 303 | 0 | 184 | $\square$ |
| 5:00 PM |  |  |  |  | 340 | 340 | 304 | 0 | 215 | $\square$ |
| 6:00 PM |  |  |  |  | 449 | 449 | 319 | 0 | 256 | $\square$ |
| 7:00 PM |  |  |  |  | 531 | 531 | 310 | 0 | 280 |  |
| 8:00 PM |  |  |  |  | 301 | 301 | 281 | 0 | 194 | I |
| 9:00 PM |  |  |  |  | 271 | 271 | 314 | 0 | 195 | $\square$ |
| 10:00 PM |  |  |  |  | 205 | 205 | 537 | 0 | 247 |  |
| 11:00 PM |  |  |  |  | 183 | 183 | 382 | 0 | 188 | 1 |
| Day Total |  |  |  |  | 4582 | 4582 | 5345 | 1469 | 3799 |  |
| \% Weekday Average |  |  |  |  | 100.0\% |  |  |  |  |  |
| \% Week Average |  |  |  |  | 120.6\% | 120.6\% | 140.7\% | 38.7\% |  |  |
| AM Peak Volume |  |  |  |  | $\begin{gathered} 11: 00 \text { AM } \\ 253 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 253 \end{gathered}$ | $\begin{gathered} 9: 00 \text { AM } \\ 260 \end{gathered}$ | $\begin{gathered} 12: 00 \mathrm{AM} \\ 365 \end{gathered}$ | $\begin{gathered} 12: 00 \mathrm{AM} \\ 162 \end{gathered}$ |  |
| PM Peak Volume |  |  |  |  | $\begin{gathered} \text { 7:00 PM } \\ 531 \end{gathered}$ | $\begin{gathered} \text { 7:00 PM } \\ 531 \end{gathered}$ | $\begin{gathered} \text { 10:00 PM } \\ 537 \end{gathered}$ | $\begin{gathered} 12: 00 \text { PM } \\ 0 \end{gathered}$ | $\begin{gathered} 7: 00 \text { PM } \\ 280 \end{gathered}$ |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 11/2/2012 1:57 PM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net)


Report generated on 11/2/2012 1:57 PM

| LOCATION: SPECIFIC L CITY/STATE: | Combined OCATION: Snoqualm | olume0 ft fro WA | Drivew orth Be $\qquad$ | Snoqu ay |  | north of roundabout at |  | Way | DATE | QC JOB \#: 10822001 DIRECTION: NB Oct 012012 - Oct 012012 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Mon 01 -Oct-12 | Tue | Wed | Thu | Fri | Average Weekday Hourly Traffic | Sat | Sun | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM | 0 |  |  |  |  | 0 |  |  | 0 | 1 |
| 1:00 AM | 0 |  |  |  |  | 0 |  |  | 0 | 1 |
| 2:00 AM | 0 |  |  |  |  | 0 |  |  | 0 | 1 |
| 3:00 AM | 0 |  |  |  |  | 0 |  |  | 0 | 1 |
| 4:00 AM | 0 |  |  |  |  | 0 |  |  | 0 | 1 |
| 5:00 AM | 0 |  |  |  |  | 0 |  |  | 0 | 1 |
| 6:00 AM | 0 |  |  |  |  | 0 |  |  | 0 | 1 |
| 7:00 AM | 0 |  |  |  |  | 0 |  |  | 0 | 1 |
| 8:00 AM | 0 |  |  |  |  | 0 |  |  | 0 | 1 |
| 9:00 AM | 0 |  |  |  |  | 0 |  |  | 0 | 1 |
| 10:00 AM | 0 |  |  |  |  | 0 |  |  | 0 | 1 |
| 11:00 AM | 2 |  |  |  |  | 2 |  |  | 2 |  |
| 12:00 PM |  |  |  |  |  |  |  |  |  |  |
| 1:00 PM |  |  |  |  |  |  |  | $\bigcirc$ |  |  |
| 2:00 PM |  |  |  |  |  |  |  |  |  |  |
| 3:00 PM |  |  |  |  |  |  |  |  |  |  |
| 4:00 PM |  |  |  |  |  |  |  |  |  |  |
| 5:00 PM |  |  |  |  |  |  |  |  |  |  |
| 6:00 PM |  |  |  |  |  |  |  |  |  |  |
| 7:00 PM |  |  |  |  |  |  |  |  |  |  |
| 8:00 PM |  |  |  |  |  |  |  |  |  |  |
| 9:00 PM |  |  |  |  |  |  |  |  |  |  |
| 10:00 PM |  |  |  |  |  |  |  |  |  |  |
| 11:00 PM |  |  |  |  |  |  |  |  |  |  |
| Day Total | 2 |  |  |  |  | 2 |  |  | 2 |  |
| \% Weekday |  |  |  |  |  |  |  |  |  |  |
| Average |  |  |  |  |  |  |  |  |  |  |
| \% Week Average |  |  |  |  |  | 100.0\% |  |  |  |  |
| AM Peak | 11:00 AM |  |  |  |  | 11:00 AM |  |  |  |  |
| Volume | 2 |  |  |  |  | 2 |  |  | $2$ |  |
| PM Peak |  |  |  |  |  |  |  |  |  |  |
| Volume |  |  |  |  |  |  |  |  |  |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 11/2/2012 1:57 PM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net)

| LOCATION: Combined Volume-Main Driveway to Snoqualmie Casino north of roundabout at SE North Bend Way SPECIFIC LOCATION: 100 ft from North Bend Way CITY/STATE: Snoqualmie, WA |  |  |  |  |  |  |  | QC JOB \#: 10822001DIRECTION: NBDATE:Sep 17 2012-Sep 212012 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | $\begin{gathered} \text { Mon } \\ 17 \text {-Sep-12 } \end{gathered}$ | Tue 18-Sep-12 | Wed 19-Sep-12 | Thu 20-Sep-12 | $\begin{gathered} \text { Fri } \\ \text { 21-Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic |  |  | Average Weekday Profile |
| 12:00 AM | 0 | 0 | 0 | 0 | 43 | 9 |  |  | $\square$ |
| 1:00 AM | 0 | 0 | 0 | 0 | 43 | 9 |  |  | $\square$ |
| 2:00 AM | 0 | 0 | 0 | 0 | 16 | 3 |  |  | - |
| 3:00 AM | 0 | 0 | 0 | 0 | 18 | 4 |  |  | - |
| 4:00 AM | 0 | 0 | 0 | 0 | 15 | 3 |  |  | D |
| 5:00 AM | 0 | 0 | 0 | 0 | 34 | 7 |  |  | $\square$ |
| 6:00 AM | 0 | 0 | 0 | 0 | 47 | 9 |  |  | $\square$ |
| 7:00 AM | 0 | 0 | 0 | 0 | 79 | 16 |  |  | - |
| 8:00 AM | 0 | 0 | 0 | 0 | 101 | 20 |  |  | $\square$ |
| 9:00 AM | 0 | 0 | 0 | 0 | 153 | 31 |  |  |  |
| 10:00 AM | 0 | 0 | 0 | 0 | 210 | 42 |  |  |  |
| 11:00 AM | 0 | 0 | 0 | 0 | 253 | 51 |  |  |  |
| 12:00 PM | 0 | 0 | 0 | 0 | 261 | 52 |  |  |  |
| 1:00 PM | 0 | 0 | 0 | 0 | 237 | 47 |  |  | - |
| 2:00 PM | 0 | 0 | 0 | 0 | 248 | 50 |  |  | $\square$ |
| 3:00 PM | 0 | 0 | 0 | 0 | 295 | 59 |  |  | $\square$ |
| 4:00 PM | 0 | 0 | 0 | 0 | 249 | 50 |  |  | $\square$ |
| 5:00 PM | 0 | 0 | 0 | 0 | 340 | 68 |  |  | $\square$ |
| 6:00 PM | 0 | 0 | 0 | 0 | 449 | 90 |  |  | $\square$ |
| 7:00 PM | 0 | 0 | 0 | 0 | 531 | 106 |  |  |  |
| 8:00 PM | 0 | 0 | 0 | 0 | 301 | 60 |  |  | $\square$ |
| 9:00 PM | 0 | 0 | 0 | 0 | 271 | 54 |  |  |  |
| 10:00 PM | 0 | 0 | 0 | 0 | 205 | 41 |  |  |  |
| 11:00 PM | 0 | 0 | 0 | 0 | 183 | 37 |  |  |  |
| Day Total | 0 | 0 | 0 | 0 | 4582 | 918 |  |  |  |
| \% Weekday Average | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 499.1\% |  |  |  |  |
| \% Week Average |  |  |  |  |  |  |  |  |  |
| AM Peak Volume | $\begin{gathered} 12: 00 \mathrm{AM} \\ 0 \end{gathered}$ | $\begin{gathered} 12: 00 \mathrm{AM} \\ 0 \end{gathered}$ | $\begin{gathered} 12: 00 \mathrm{AM} \\ 0 \end{gathered}$ | $\begin{gathered} 12: 00 \text { AM } \\ 0 \end{gathered}$ | $\begin{gathered} \hline 11: 00 \text { AM } \\ 253 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 51 \end{gathered}$ |  |  |  |
| PM Peak Volume | ${ }_{0}^{12: 00 ~ P M}$ | $\begin{gathered} 12: 00 \text { PM } \\ 0 \end{gathered}$ | $\begin{gathered} 12: 00 \text { PM } \\ 0 \end{gathered}$ | $\begin{gathered} 12: 00 ~ P M \\ 0 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{PM} \\ 531 \end{gathered}$ | $\begin{gathered} 7: 00 \text { PM } \\ 106 \end{gathered}$ |  |  |  |
| Comments: |  |  |  |  |  |  |  |  |  |

Report generated on 11/2/2012 1:57 PM

| LOCATION: SPECIFIC CITY/STAT | SE North | Bend Way | DATE: | QC JOB \#: 10822001 DIRECTION: NB Sep 222012 - Sep 232012 |
| :---: | :---: | :---: | :---: | :---: |
| Start Time | $\begin{gathered} \text { Sat } \\ \text { 22-Sep-12 } \end{gathered}$ | $\begin{gathered} \text { Sun } \\ 23-\text { Sep-12 } \end{gathered}$ | Average Weekend Hourly Traffic | Average Weekend Profile |
| 12:00 AM | 77 | 365 | 221 | , |
| 1:00 AM | 69 | 276 | 173 | $\square$ |
| 2:00 AM | 38 | 222 | 130 |  |
| 3:00 AM | 21 | 153 | 87 |  |
| 4:00 AM | 19 | 91 | 55 | $\square$ |
| 5:00 AM | 51 | 55 | 53 | $\square$ |
| 6:00 AM | 69 | 60 | 65 | $\square$ |
| 7:00 AM | 164 | 68 | 116 | $\square$ |
| 8:00 AM | 174 | 124 | 149 | $\square$ |
| 9:00 AM | 260 | 55 | 158 |  |
| 10:00 AM | 183 | 0 | 92 | $\square$ |
| 11:00 AM | 192 | 0 | 96 | $\square$ |
| 12:00 PM | 240 | 0 | 120 |  |
| 1:00 PM | 271 | 0 | 136 | $\square$ |
| 2:00 PM | 297 | 0 | 149 | - |
| 3:00 PM | 470 | 0 | 235 |  |
| 4:00 PM | 303 | 0 | 152 | $\square$ |
| 5:00 PM | 304 | 0 | 152 | ? |
| 6:00 PM | 319 | 0 | 160 | $\square$ |
| 7:00 PM | 310 | 0 | 155 | , |
| 8:00 PM | 281 | 0 | 141 | $\square$ |
| 9:00 PM | 314 | 0 | 157 | - |
| 10:00 PM | 537 | 0 | 269 | 1 |
| 11:00 PM | 382 | 0 | 191 | 1 |
| Day Total | 5345 | 1469 | 3412 |  |
| \% Weekday Average |  |  |  |  |
| \% Week Average | 156.7\% | 43.1\% |  |  |
| AM Peak Volume | $\begin{gathered} 9: 00 \text { AM } \\ 260 \end{gathered}$ | $\begin{gathered} 12: 00 \mathrm{AM} \\ 365 \end{gathered}$ | $\begin{gathered} 12: 00 \mathrm{AM} \\ 221 \end{gathered}$ |  |
| PM Peak Volume | $\begin{gathered} 10: 00 \text { PM } \\ 537 \end{gathered}$ | $\begin{gathered} 12: 00 ~ P M \\ 0 \end{gathered}$ | $\begin{gathered} 10: 00 \text { PM } \\ 269 \end{gathered}$ |  |
| Comments: |  |  |  |  |

Report generated on 11/2/2012 1:57 PM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net)

| LOCATION: Combined Volume-Main Driveway to Snoqualmie Casino north of roundabout at SE North Bend Way SPECIFIC LOCATION: 100 ft from North Bend Way CITY/STATE: Snoqualmie, WA |  |  |  |  |  |  |  |  | QC JOB \#: 10822001DIRECTION: NBDATE: Sep 17 2012-Sep 232012 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | $\begin{gathered} \text { Mon } \\ \text { 17-Sep-12 } \end{gathered}$ | Tue 18-Sep-12 | Wed 19-Sep-12 | Thu 20-Sep-12 | $\begin{gathered} \text { Fri } \\ \text { 21-Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | Sat 22-Sep-12 | $\begin{gathered} \text { Sun } \\ 23 \text {-Sep-12 } \end{gathered}$ | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM | 0 | 0 | 0 | 0 | 43 | 9 | 77 | 365 | 69 | $\square$ |
| 1:00 AM | 0 | 0 | 0 | 0 | 43 | 9 | 69 | 276 | 55 | - |
| 2:00 AM | 0 | 0 | 0 | 0 | 16 | 3 | 38 | 222 | 39 |  |
| 3:00 AM | 0 | 0 | 0 | 0 | 18 | 4 | 21 | 153 | 27 |  |
| 4:00 AM | 0 | 0 | 0 | 0 | 15 | 3 | 19 | 91 | 18 | $\square$ |
| 5:00 AM | 0 | 0 | 0 | 0 | 34 | 7 | 51 | 55 | 20 | $\square$ |
| 6:00 AM | 0 | 0 | 0 | 0 | 47 | 9 | 69 | 60 | 25 | $\square$ |
| 7:00 AM | 0 | 0 | 0 | 0 | 79 | 16 | 164 | 68 | 44 |  |
| 8:00 AM | 0 | 0 | 0 | 0 | 101 | 20 | 174 | 124 | 57 |  |
| 9:00 AM | 0 | 0 | 0 | 0 | 153 | 31 | 260 | 55 | 67 | - |
| 10:00 AM | 0 | 0 | 0 | 0 | 210 | 42 | 183 | 0 | 56 | $\square$ |
| 11:00 AM | 0 | 0 | 0 | 0 | 253 | 51 | 192 | 0 | 64 |  |
| 12:00 PM | 0 | 0 | 0 | 0 | 261 | 52 | 240 | 0 | 72 |  |
| 1:00 PM | 0 | 0 | 0 | 0 | 237 | 47 | 271 | 0 | 73 | ] |
| 2:00 PM | 0 | 0 | 0 | 0 | 248 | 50 | 297 | 0 | 78 | - |
| 3:00 PM | 0 | 0 | 0 | 0 | 295 | 59 | 470 | 0 | 109 | - |
| 4:00 PM | 0 | 0 | 0 | 0 | 249 | 50 | 303 | 0 | 79 | ] |
| 5:00 PM | 0 | 0 | 0 | 0 | 340 | 68 | 304 | 0 | 92 | - |
| 6:00 PM | 0 | 0 | 0 | 0 | 449 | 90 | 319 | 0 | 110 | - |
| 7:00 PM | 0 | 0 | 0 | 0 | 531 | 106 | 310 | 0 | 120 |  |
| 8:00 PM | 0 | 0 | 0 | 0 | 301 | 60 | 281 | 0 | 83 | - |
| 9:00 PM | 0 | 0 | 0 | 0 | 271 | 54 | 314 | 0 | 84 | ] |
| 10:00 PM | 0 | 0 | 0 | 0 | 205 | 41 | 537 | 0 | 106 |  |
| 11:00 PM | 0 | 0 | 0 | 0 | 183 | 37 | 382 | 0 | 81 | 1 |
| Day Total | 0 | 0 | 0 | 0 | 4582 | 918 | 5345 | 1469 | 1628 |  |
| \% Weekday Average | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 499.1\% |  |  |  |  |  |
| \% Week Average | 0.0\% | 0.0\% | 0.0\% | 0.0\% | 281.4\% | 56.4\% | 328.3\% | 90.2\% |  |  |
| AM Peak Volume | $\begin{gathered} 12: 00 \mathrm{AM} \\ 0 \end{gathered}$ | $\begin{gathered} 12: 00 \mathrm{AM} \\ 0 \end{gathered}$ | $\begin{gathered} 12: 00 \mathrm{AM} \\ 0 \end{gathered}$ | $\begin{gathered} 12: 00 \mathrm{AM} \\ 0 \end{gathered}$ | $\begin{gathered} \hline 11: 00 \mathrm{AM} \\ 253 \\ \hline \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 51 \end{gathered}$ | $\begin{aligned} & 9: 00 \text { AM } \\ & 260 \end{aligned}$ | $\begin{gathered} 12: 00 \text { AM } \\ 365 \end{gathered}$ | $\begin{gathered} 12: 00 \mathrm{AM} \\ 69 \end{gathered}$ |  |
| PM Peak Volume | ${ }_{\text {12:00 PM }}^{0}$ | $\begin{gathered} 12: 00 \text { PM } \\ 0 \end{gathered}$ | $\begin{gathered} 12: 00 ~ P M \\ 0 \end{gathered}$ | $\begin{gathered} 12: 00 \text { PM } \\ 0 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{PM} \\ 531 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{PM} \\ 106 \end{gathered}$ | $\begin{gathered} \hline 10: 00 \mathrm{PM} \\ 537 \end{gathered}$ | $\begin{gathered} 12: 00 \mathrm{PM} \\ 0 \\ \hline \end{gathered}$ | $\begin{gathered} \text { 7:00 PM } \\ 120 \end{gathered}$ |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 11/2/2012 1:57 PM

| LOCATION: Combined Volume-Main Driveway to Snoqualmie Casino north of roundabout at SE North Bend Way SPECIFIC LOCATION: 100 ft from North Bend Way <br> CITY/STATE: Snoqualmie, WA |  |  |  |  |  |  |  |  | DIRECTION: SBDATE: Sep 212012 - Sep 232012 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Mon | Tue | Wed | Thu | $\begin{gathered} \text { Fri } \\ 21-\text { Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | Sat 22-Sep-12 | $\begin{gathered} \text { Sun } \\ 23-\text { Sep-12 } \end{gathered}$ | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM |  |  |  |  | 235 | 235 | 307 | 76 | 206 | $\square$ |
| 1:00 AM |  |  |  |  | 141 | 141 | 251 | 69 | 154 | $\square$ |
| 2:00 AM |  |  |  |  | 117 | 117 | 224 | 31 | 124 | $\square$ |
| 3:00 AM |  |  |  |  | 83 | 83 | 127 | 15 | 75 | $\square$ |
| 4:00 AM |  |  |  |  | 60 | 60 | 68 | 20 | 49 | $\square$ |
| 5:00 AM |  |  |  |  | 40 | 40 | 43 | 37 | 40 | $\square$ |
| 6:00 AM |  |  |  |  | 35 | 35 | 56 | 64 | 52 | $\square$ |
| 7:00 AM |  |  |  |  | 40 | 40 | 89 | 116 | 82 | $\square$ |
| 8:00 AM |  |  |  |  | 71 | 71 | 124 | 134 | 110 | $\square$ |
| 9:00 AM |  |  |  |  | 51 | 51 | 172 | 235 | 153 | $\square$ |
| 10:00 AM |  |  |  |  | 94 | 94 | 318 | 345 | 252 | - |
| 11:00 AM |  |  |  |  | 93 | 93 | 345 | 363 | 267 | $\square$ |
| 12:00 PM |  |  |  |  | 160 | 160 | 317 | 417 | 298 | $\square$ |
| 1:00 PM |  |  |  |  | 216 | 216 | 329 | 459 | 335 | $\square$ |
| 2:00 PM |  |  |  |  | 244 | 244 | 324 | 474 | 347 | - |
| 3:00 PM |  |  |  |  | 222 | 222 | 126 | 443 | 264 | ] |
| 4:00 PM |  |  |  |  | 236 | 236 | 362 | 423 | 340 | ] |
| 5:00 PM |  |  |  |  | 262 | 262 | 387 | 422 | 357 | $\square$ |
| 6:00 PM |  |  |  |  | 238 | 238 | 432 | 448 | 373 | $\square$ |
| 7:00 PM |  |  |  |  | 288 | 288 | 452 | 438 | 393 |  |
| 8:00 PM |  |  |  |  | 316 | 316 | 362 | 393 | 357 | - |
| 9:00 PM |  |  |  |  | 335 | 335 | 288 | 361 | 328 | ] |
| 10:00 PM |  |  |  |  | 475 | 475 | 253 | 293 | 340 | - |
| 11:00 PM |  |  |  |  | 333 | 333 | 216 | 234 | 261 | 1 |
| Day Total |  |  |  |  | 4385 | 4385 | 5972 | 6310 | 5557 |  |
| \% Weekday Average |  |  |  |  | 100.0\% |  |  |  |  |  |
| \% Week Average |  |  |  |  | 78.9\% | 78.9\% | 107.5\% | 113.6\% |  |  |
| AM Peak Volume |  |  |  |  | $\begin{gathered} 12: 00 \text { AM } \\ 235 \end{gathered}$ | $\begin{gathered} 12: 00 \text { AM } \\ 235 \end{gathered}$ | $\begin{gathered} \hline 11: 00 \mathrm{AM} \\ 345 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 363 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 267 \end{gathered}$ |  |
| PM Peak |  |  |  |  | 10:00 PM | 10:00 PM | 7:00 PM | 2:00 PM | 7:00 PM |  |
| Volume |  |  |  |  | 475 | 475 | 452 | 474 | 393 |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 11/2/2012 1:57 PM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net)

| LOCATION: Combined Volume-Main Driveway to Snoqualmie Casino north of roundabout at SE North Bend Way SPECIFIC LOCATION: 100 ft from North Bend Way <br> CITY/STATE: Snoqualmie, WA |  |  |  |  |  |  |  |  | $\begin{gathered} \text { QC JOB \#: } 10822001 \\ \text { DIRECTION: SB } \\ \text { DATE: Sep } 24 \text { 2012 - Sep } 302012 \end{gathered}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | $\begin{gathered} \text { Mon } \\ 24-\text { Sep-12 } \end{gathered}$ | Tue 25-Sep-12 | Wed 26-Sep-12 | Thu 27-Sep-12 | Fri <br> 28-Sep-12 | Average Weekday Hourly Traffic | Sat 29-Sep-12 | Sun 30-Sep-12 | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM | 197 | 158 | 114 | 121 | 220 | 162 | 342 | 339 | 213 | $\square$ |
| 1:00 AM | 131 | 170 | 92 | 92 | 157 | 128 | 286 | 262 | 170 |  |
| 2:00 AM | 93 | 99 | 75 | 89 | 126 | 96 | 219 | 245 | 135 |  |
| 3:00 AM | 73 | 68 | 62 | 49 | 86 | 68 | 130 | 165 | 90 | $\square$ |
| 4:00 AM | 44 | 65 | 42 | 40 | 55 | 49 | 93 | 95 | 62 | $\square$ |
| 5:00 AM | 59 | 59 | 54 | 57 | 76 | 61 | 89 | 103 | 71 |  |
| 6:00 AM | 132 | 70 | 123 | 128 | 83 | 107 | 144 | 116 | 114 | - |
| 7:00 AM | 215 | 99 | 176 | 208 | 128 | 165 | 214 | 146 | 169 |  |
| 8:00 AM | 226 | 125 | 215 | 231 | 160 | 191 | 262 | 209 | 204 |  |
| 9:00 AM | 278 | 128 | 253 | 288 | 214 | 232 | 310 | 255 | 247 | $\square$ |
| 10:00 AM | 329 | 224 | 290 | 354 | 243 | 288 | 387 | 319 | 307 | $\square$ |
| 11:00 AM | 383 | 398 | 300 | 388 | 304 | 355 | 476 | 357 | 372 |  |
| 12:00 PM | 391 | 226 | 339 | 370 | 331 | 331 | 550 | 357 | 366 |  |
| 1:00 PM | 434 | 354 | 450 | 436 | 344 | 404 | 577 | 459 | 436 |  |
| 2:00 PM | 439 | 343 | 387 | 403 | 366 | 388 | 570 | 458 | 424 |  |
| 3:00 PM | 436 | 396 | 418 | 438 | 388 | 415 | 560 | 436 | 439 |  |
| 4:00 PM | 455 | 497 | 488 | 459 | 384 | 457 | 526 | 471 | 469 |  |
| 5:00 PM | 426 | 478 | 489 | 440 | 422 | 451 | 505 | 497 | 465 |  |
| 6:00 PM | 402 | 493 | 479 | 449 | 452 | 455 | 513 | 524 | 473 |  |
| 7:00 PM | 398 | 399 | 389 | 434 | 503 | 425 | 501 | 399 | 432 | - |
| 8:00 PM | 363 | 327 | 316 | 442 | 498 | 389 | 439 | 541 | 418 | $\square$ |
| 9:00 PM | 382 | 275 | 277 | 404 | 474 | 362 | 472 | 445 | 390 |  |
| 10:00 PM | 346 | 218 | 201 | 359 | 417 | 308 | 460 | 336 | 334 | ] |
| 11:00 PM | 237 | 166 | 167 | 302 | 437 | 262 | 452 | 239 | 286 | $\square$ |
| Day Total | 6869 | 5835 | 6196 | 6981 | 6868 | 6549 | 9077 | 7773 | 7086 |  |
| \% Weekday Average | 156.6\% | 89.1\% | 94.6\% | 106.6\% | 104.9\% |  |  |  |  |  |
| \% Week Average | 123.6\% | 82.3\% | 87.4\% | 98.5\% | 96.9\% | 92.4\% | 128.1\% | 109.7\% |  |  |
| AM Peak | 11:00 AM | 11:00 AM | 11:00 AM | 11:00 AM | 11:00 AM | 11:00 AM | 11:00 AM | 11:00 AM | 11:00 AM |  |
| Volume | 383 | 398 | 300 | 388 | 304 | 355 | 476 | 357 | 372 |  |
| PM Peak | 4:00 PM | 4:00 PM | 5:00 PM | 4:00 PM | 7:00 PM | 4:00 PM | 1:00 PM | 8:00 PM | 6:00 PM |  |
| Volume | 455 | 497 | 489 | 459 | 503 | 457 | 577 | 541 | 473 |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 11/2/2012 1:57 PM

| LOCATION: SPECIFIC L CITY/STATE | Combined OCATION: Snoqualm | olume00 ft fro WA | Drivew orth Be | Snoqu ay |  | north of roundabout at | Nort | Way | DATE | QC JOB \#: 10822001 DIRECTION: SB Oct 01 2012-Oct 012012 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Mon 01 -Oct-12 | Tue | Wed | Thu | Fri | Average Weekday Hourly Traffic | Sat | Sun | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM | 213 |  |  |  |  | 213 |  |  | 213 | $\square$ |
| 1:00 AM | 142 |  |  |  |  | 142 |  |  | 142 | $\square$ |
| 2:00 AM | 101 |  |  |  |  | 101 |  |  | 101 |  |
| 3:00 AM | 76 |  |  |  |  | 76 |  |  | 76 | $\square$ |
| 4:00 AM | 44 |  |  |  |  | 44 |  |  | 44 | $\square$ |
| 5:00 AM | 76 |  |  |  |  | 76 |  |  | 76 | $\square$ |
| 6:00 AM | 126 |  |  |  |  | 126 |  |  | 126 | $\square$ |
| 7:00 AM | 205 |  |  |  |  | 205 |  |  | 205 | $\square$ |
| 8:00 AM | 207 |  |  |  |  | 207 |  |  | 207 |  |
| 9:00 AM | 288 |  |  |  |  | 288 |  |  | 288 | $\square$ |
| 10:00 AM | 334 |  |  |  |  | 334 |  |  | 334 |  |
| 11:00 AM | 136 |  |  |  |  | 136 |  |  | 136 |  |
| 12:00 PM |  |  |  |  |  |  |  |  |  |  |
| 1:00 PM |  |  |  |  |  | $\square$ |  | 0 |  |  |
| 2:00 PM |  |  |  |  |  |  |  |  |  |  |
| 3:00 PM |  |  |  |  |  |  |  |  |  |  |
| 4:00 PM |  |  |  |  |  |  |  |  |  |  |
| 5:00 PM |  |  |  |  |  |  |  |  |  |  |
| 6:00 PM |  |  |  |  |  |  |  |  |  |  |
| 7:00 PM |  |  |  |  |  |  |  |  |  |  |
| 8:00 PM |  |  |  |  |  |  |  |  |  |  |
| 9:00 PM |  |  |  |  |  |  |  |  |  |  |
| 10:00 PM |  |  |  |  |  |  |  |  |  |  |
| 11:00 PM |  |  |  |  |  |  |  |  |  |  |
| Day Total | 1948 |  |  |  |  | 1948 |  |  | 1948 |  |
| \% Weekday |  |  |  |  |  |  |  |  |  |  |
| Average | 29.7\% |  |  |  |  |  |  |  |  |  |
| \% Week |  |  |  |  |  |  |  |  |  |  |
| Average | 27.5\% |  |  |  |  | 100.0\% |  |  |  |  |
| AM Peak | 10:00 AM |  |  |  |  | 10:00 AM |  |  | 10:00 AM |  |
| Volume | 334 |  |  |  |  | 334 |  |  | 334 |  |
| PM Peak |  |  |  |  |  |  |  |  |  |  |
| Volume |  |  |  |  |  |  |  |  |  |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 11/2/2012 1:57 PM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net)

| LOCATION SPECIFIC CITY/STAT | Combined OCATION: <br> : Snoqual | Volume-Ma 100 ft from mie, WA | ain Driveway North Bend | y to Snoqual Way | Imie Casino | orth of roundabout at | SE North Bend Way | DATE: | QC JOB \#: 10822001 DIRECTION: SB <br> Sep 172012 - Sep 212012 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Mon 17-Sep-12 | Tue <br> 18-Sep-12 | Wed 19-Sep-12 | Thu 20-Sep-12 | $\begin{gathered} \hline \text { Fri } \\ 21-\text { Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic |  |  | Average Weekday Profile |
| 12:00 AM | 197 | 158 | 114 | 121 | 235 | 165 |  |  | - |
| 1:00 AM | 131 | 170 | 92 | 92 | 141 | 125 |  |  | $\square$ |
| 2:00 AM | 93 | 99 | 75 | 89 | 117 | 95 |  |  |  |
| 3:00 AM | 73 | 68 | 62 | 49 | 83 | 67 |  |  | $\square$ |
| 4:00 AM | 44 | 65 | 42 | 40 | 60 | 50 |  |  | $\square$ |
| 5:00 AM | 59 | 59 | 54 | 57 | 40 | 54 |  |  | - |
| 6:00 AM | 132 | 70 | 123 | 128 | 35 | 98 |  |  |  |
| 7:00 AM | 215 | 99 | 176 | 208 | 40 | 148 |  |  |  |
| 8:00 AM | 226 | 125 | 215 | 231 | 71 | 174 |  |  |  |
| 9:00 AM | 278 | 128 | 253 | 288 | 51 | 200 |  |  |  |
| 10:00 AM | 329 | 224 | 290 | 354 | 94 | 258 |  |  |  |
| 11:00 AM | 383 | 398 | 300 | 388 | 93 | 312 |  |  |  |
| 12:00 PM | 391 | 226 | 339 | 370 | 160 | 297 |  |  | - |
| 1:00 PM | 434 | 354 | 450 | 436 | 216 | 378 | $\square$ |  |  |
| 2:00 PM | 439 | 343 | 387 | 403 | 244 | 363 |  |  |  |
| 3:00 PM | 436 | 396 | 418 | 438 | 222 | 382 |  |  | $\square$ |
| 4:00 PM | 455 | 497 | 488 | 459 | 236 | 427 |  |  |  |
| 5:00 PM | 426 | 478 | 489 | 440 | 262 | 419 |  |  |  |
| 6:00 PM | 402 | 493 | 479 | 449 | 238 | 412 |  |  |  |
| 7:00 PM | 398 | 399 | 389 | 434 | 288 | 382 |  |  | $0$ |
| 8:00 PM | 363 | 327 | 316 | 442 | 316 | 353 |  |  | $\square$ |
| 9:00 PM | 382 | 275 | 277 | 404 | 335 | 335 |  |  |  |
| 10:00 PM | 346 | 218 | 201 | 359 | 475 | 320 |  |  |  |
| 11:00 PM | 237 | 166 | 167 | 302 | 333 | 241 |  |  |  |
| Day Total | 6869 | 5835 | 6196 | 6981 | 4385 | 6055 |  |  |  |
| \% Weekday Average | 113.4\% | 96.4\% | 102.3\% | 115.3\% | 72.4\% |  |  |  |  |
| \% Week Average |  |  |  |  |  |  |  |  |  |
| AM Peak Volume | $\begin{gathered} \hline 11: 00 \mathrm{AM} \\ 383 \\ \hline \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 398 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 300 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 388 \end{gathered}$ | $\begin{gathered} 12: 00 \mathrm{AM} \\ 235 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 312 \end{gathered}$ |  |  |  |
| PM Peak Volume | $\begin{gathered} 4: 00 \text { PM } \\ 455 \\ \hline \end{gathered}$ | $\begin{gathered} 4: 00 \mathrm{PM} \\ 497 \\ \hline \end{gathered}$ | $\begin{gathered} 5: 00 \mathrm{PM} \\ 489 \\ \hline \end{gathered}$ | $\begin{gathered} 4: 00 \mathrm{PM} \\ 459 \\ \hline \end{gathered}$ | $\begin{gathered} 10: 00 \mathrm{PM} \\ 475 \end{gathered}$ | $\begin{gathered} 4: 00 \mathrm{PM} \\ 427 \\ \hline \end{gathered}$ |  |  |  |
| Comments: |  |  |  |  |  |  |  |  |  |

Report generated on 11/2/2012 1:57 PM


Report generated on 11/2/2012 1:57 PM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net)

| LOCATION: Combined Volume-Main Driveway to Snoqualmie Casino north of roundabout at SE North Bend Way SPECIFIC LOCATION: 100 ft from North Bend Way CITY/STATE: Snoqualmie, WA |  |  |  |  |  |  |  |  | QC JOB \#: 10822001DIRECTION: SBDATE:Sep 17 2012-Sep 232012 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | $\begin{gathered} \text { Mon } \\ 17-\text { Sep-12 } \end{gathered}$ | Tue 18-Sep-12 | Wed 19-Sep-12 | Thu 20-Sep-12 | $\begin{gathered} \text { Fri } \\ \text { 21-Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | Sat 22-Sep-12 | $\begin{gathered} \text { Sun } \\ 23 \text {-Sep-12 } \end{gathered}$ | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM | 197 | 158 | 114 | 121 | 235 | 165 | 307 | 76 | 173 | — |
| 1:00 AM | 131 | 170 | 92 | 92 | 141 | 125 | 251 | 69 | 135 |  |
| 2:00 AM | 93 | 99 | 75 | 89 | 117 | 95 | 224 | 31 | 104 |  |
| 3:00 AM | 73 | 68 | 62 | 49 | 83 | 67 | 127 | 15 | 68 |  |
| 4:00 AM | 44 | 65 | 42 | 40 | 60 | 50 | 68 | 20 | 48 | $\square$ |
| 5:00 AM | 59 | 59 | 54 | 57 | 40 | 54 | 43 | 37 | 50 | $\square$ |
| 6:00 AM | 132 | 70 | 123 | 128 | 35 | 98 | 56 | 64 | 87 | - |
| 7:00 AM | 215 | 99 | 176 | 208 | 40 | 148 | 89 | 116 | 135 |  |
| 8:00 AM | 226 | 125 | 215 | 231 | 71 | 174 | 124 | 134 | 161 |  |
| 9:00 AM | 278 | 128 | 253 | 288 | 51 | 200 | 172 | 235 | 201 |  |
| 10:00 AM | 329 | 224 | 290 | 354 | 94 | 258 | 318 | 345 | 279 |  |
| 11:00 AM | 383 | 398 | 300 | 388 | 93 | 312 | 345 | 363 | 324 |  |
| 12:00 PM | 391 | 226 | 339 | 370 | 160 | 297 | 317 | 417 | 317 | $\square$ |
| 1:00 PM | 434 | 354 | 450 | 436 | 216 | 378 | 329 | 459 | 383 |  |
| 2:00 PM | 439 | 343 | 387 | 403 | 244 | 363 | 324 | 474 | 373 |  |
| 3:00 PM | 436 | 396 | 418 | 438 | 222 | 382 | 126 | 443 | 354 |  |
| 4:00 PM | 455 | 497 | 488 | 459 | 236 | 427 | 362 | 423 | 417 |  |
| 5:00 PM | 426 | 478 | 489 | 440 | 262 | 419 | 387 | 422 | 415 |  |
| 6:00 PM | 402 | 493 | 479 | 449 | 238 | 412 | 432 | 448 | 420 |  |
| 7:00 PM | 398 | 399 | 389 | 434 | 288 | 382 | 452 | 438 | 400 |  |
| 8:00 PM | 363 | 327 | 316 | 442 | 316 | 353 | 362 | 393 | 360 | J |
| 9:00 PM | 382 | 275 | 277 | 404 | 335 | 335 | 288 | 361 | 332 | 」 |
| 10:00 PM | 346 | 218 | 201 | 359 | 475 | 320 | 253 | 293 | 306 | ) |
| 11:00 PM | 237 | 166 | 167 | 302 | 333 | 241 | 216 | 234 | 236 | 1 |
| Day Total | 6869 | 5835 | 6196 | 6981 | 4385 | 6055 | 5972 | 6310 | 6078 |  |
| \% Weekday Average | 113.4\% | 96.4\% | 102.3\% | 115.3\% | 72.4\% |  |  |  |  |  |
| \% Week Average | 113.0\% | 96.0\% | 101.9\% | 114.9\% | 72.1\% | 99.6\% | 98.3\% | 103.8\% |  |  |
| AM Peak Volume | $\begin{gathered} \hline 11: 00 \mathrm{AM} \\ 383 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 398 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 300 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 388 \end{gathered}$ | $\begin{gathered} 12: 00 \text { AM } \\ 235 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 312 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 345 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 363 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 324 \end{gathered}$ |  |
| PM Peak Volume | 4:00 PM 455 | $\begin{gathered} 4: 00 \mathrm{PM} \\ 497 \end{gathered}$ | $\begin{gathered} 5: 00 \mathrm{PM} \\ 489 \end{gathered}$ | $\begin{gathered} 4: 00 \text { PM } \\ 459 \end{gathered}$ | $\begin{gathered} 10: 00 \mathrm{PM} \\ 475 \end{gathered}$ | $\begin{gathered} \hline 4: 00 \mathrm{PM} \\ 427 \end{gathered}$ | $\begin{gathered} 7: 00 \text { PM } \\ 452 \end{gathered}$ | $\begin{gathered} \text { 2:00 PM } \\ 474 \end{gathered}$ | $\begin{gathered} \text { 6:00 PM } \\ 420 \end{gathered}$ |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 11/2/2012 1:57 PM

| LOCATION: Combined Volume-Main Driveway to Snoqualmie Casino north of roundabout at SE North Bend Way SPECIFIC LOCATION: 100 ft from North Bend Way CITY/STATE: Snoqualmie, WA |  |  |  |  |  |  |  |  | DIRECTION: NB/SB <br> DATE: Sep 212012 - Sep 232012 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Mon | Tue | Wed | Thu | $\begin{gathered} \text { Fri } \\ 21-\text { Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | Sat 22-Sep-12 | Sun 23-Sep-12 | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM |  |  |  |  | 278 | 278 | 384 | 441 | 368 | $\square$ |
| 1:00 AM |  |  |  |  | 184 | 184 | 320 | 345 | 283 | $\square$ |
| 2:00 AM |  |  |  |  | 133 | 133 | 262 | 253 | 216 | $\square$ |
| 3:00 AM |  |  |  |  | 101 | 101 | 148 | 168 | 139 | $\square$ |
| 4:00 AM |  |  |  |  | 75 | 75 | 87 | 111 | 91 | $\square$ |
| 5:00 AM |  |  |  |  | 74 | 74 | 94 | 92 | 87 | $\square$ |
| 6:00 AM |  |  |  |  | 82 | 82 | 125 | 124 | 110 | $\square$ |
| 7:00 AM |  |  |  |  | 119 | 119 | 253 | 184 | 185 | $\square$ |
| 8:00 AM |  |  |  |  | 172 | 172 | 298 | 258 | 243 | $\square$ |
| 9:00 AM |  |  |  |  | 204 | 204 | 432 | 290 | 309 |  |
| 10:00 AM |  |  |  |  | 304 | 304 | 501 | 345 | 383 | - |
| 11:00 AM |  |  |  |  | 346 | 346 | 537 | 363 | 415 | - |
| 12:00 PM |  |  |  |  | 421 | 421 | 557 | 417 | 465 | $\square$ |
| 1:00 PM |  |  |  |  | 453 | 453 | 600 | 459 | 504 | $\square$ |
| 2:00 PM |  |  |  |  | 492 | 492 | 621 | 474 | 529 | I |
| 3:00 PM |  |  |  |  | 517 | 517 | 596 | 443 | 519 |  |
| 4:00 PM |  |  |  |  | 485 | 485 | 665 | 423 | 524 | - |
| 5:00 PM |  |  |  |  | 602 | 602 | 691 | 422 | 572 | - |
| 6:00 PM |  |  |  |  | 687 | 687 | 751 | 448 | 629 | $\square$ |
| 7:00 PM |  |  |  |  | 819 | 819 | 762 | 438 | 673 |  |
| 8:00 PM |  |  |  |  | 617 | 617 | 643 | 393 | 551 | ? |
| 9:00 PM |  |  |  |  | 606 | 606 | 602 | 361 | 523 | + |
| 10:00 PM |  |  |  |  | 680 | 680 | 790 | 293 | 588 |  |
| 11:00 PM |  |  |  |  | 516 | 516 | 598 | 234 | 449 | 1 |
| Day Total |  |  |  |  | 8967 | 8967 | 11317 | 7779 | 9355 |  |
| \% Weekday Average |  |  |  |  | 100.0\% |  |  |  |  |  |
| \% Week Average |  |  |  |  | 95.9\% | 95.9\% | 121.0\% | 83.2\% |  |  |
| AM Peak Volume |  |  |  |  | $\begin{gathered} 11: 00 \text { AM } \\ 346 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 346 \end{gathered}$ | $\begin{gathered} \hline 11: 00 \mathrm{AM} \\ 537 \end{gathered}$ | $\begin{gathered} 12: 00 \mathrm{AM} \\ 441 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 415 \end{gathered}$ |  |
| PM Peak |  |  |  |  | 7:00 PM | 7:00 PM | 10:00 PM | 2:00 PM | 7:00 PM |  |
| Volume |  |  |  |  | 819 | 819 | 790 | 474 | 673 |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 11/2/2012 1:57 PM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net)

| LOCATION: Combined Volume-Main Driveway to Snoqualmie Casino north of roundabout at SE North Bend Way SPECIFIC LOCATION: 100 ft from North Bend Way CITY/STATE: Snoqualmie, WA |  |  |  |  |  |  |  |  | DIRECTION: NB/SBDATE:Sep 24 2012-Sep 302012 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Mon 24-Sep-12 | Tue 25-Sep-12 | Wed 26-Sep-12 | Thu <br> 27-Sep-12 | $\begin{gathered} \text { Fri } \\ 28-\text { Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | Sat 29-Sep-12 | $\begin{gathered} \text { Sun } \\ 30-\text { Sep-12 } \end{gathered}$ | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM | 197 | 158 | 114 | 121 | 220 | 162 | 342 | 339 | 213 | $\square$ |
| 1:00 AM | 131 | 170 | 92 | 92 | 157 | 128 | 286 | 262 | 170 | - |
| 2:00 AM | 93 | 99 | 75 | 89 | 126 | 96 | 219 | 245 | 135 |  |
| 3:00 AM | 73 | 68 | 62 | 49 | 86 | 68 | 130 | 165 | 90 |  |
| 4:00 AM | 44 | 65 | 42 | 40 | 55 | 49 | 93 | 95 | 62 | $\square$ |
| 5:00 AM | 59 | 59 | 54 | 57 | 76 | 61 | 89 | 103 | 71 | $\square$ |
| 6:00 AM | 132 | 70 | 123 | 128 | 83 | 107 | 144 | 116 | 114 | $\square$ |
| 7:00 AM | 215 | 99 | 176 | 208 | 128 | 165 | 214 | 146 | 169 |  |
| 8:00 AM | 226 | 125 | 215 | 231 | 160 | 191 | 262 | 209 | 204 |  |
| 9:00 AM | 278 | 128 | 253 | 288 | 214 | 232 | 310 | 255 | 247 |  |
| 10:00 AM | 329 | 224 | 290 | 354 | 243 | 288 | 387 | 319 | 307 |  |
| 11:00 AM | 383 | 398 | 300 | 388 | 304 | 355 | 476 | 357 | 372 | - |
| 12:00 PM | 391 | 226 | 339 | 370 | 331 | 331 | 550 | 357 | 366 | ) |
| 1:00 PM | 434 | 354 | 450 | 436 | 344 | 404 | 577 | 459 | 436 | ] |
| 2:00 PM | 439 | 343 | 387 | 403 | 366 | 388 | 570 | 458 | 424 |  |
| 3:00 PM | 436 | 396 | 418 | 438 | 388 | 415 | 560 | 436 | 439 | $\square$ |
| 4:00 PM | 455 | 497 | 488 | 459 | 384 | 457 | 526 | 471 | 469 |  |
| 5:00 PM | 426 | 478 | 489 | 440 | 422 | 451 | 505 | 497 | 465 |  |
| 6:00 PM | 402 | 493 | 479 | 449 | 452 | 455 | 513 | 524 | 473 |  |
| 7:00 PM | 398 | 399 | 389 | 434 | 503 | 425 | 501 | 399 | 432 | $\square$ |
| 8:00 PM | 363 | 327 | 316 | 442 | 498 | 389 | 439 | 541 | 418 |  |
| 9:00 PM | 382 | 275 | 277 | 404 | 474 | 362 | 472 | 445 | 390 |  |
| 10:00 PM | 346 | 218 | 201 | 359 | 417 | 308 | 460 | 336 | 334 | - |
| 11:00 PM | 237 | 166 | 167 | 302 | 437 | 262 | 452 | 239 | 286 | 1 |
| Day Total | 6869 | 5835 | 6196 | 6981 | 6868 | 6549 | 9077 | 7773 | 7086 |  |
| \% Weekday Average | 76.6\% | 89.1\% | 94.6\% | 106.6\% | 104.9\% |  |  |  |  |  |
| \% Week Average | 73.4\% | 82.3\% | 87.4\% | 98.5\% | 96.9\% | 92.4\% | 128.1\% | 109.7\% |  |  |
| AM Peak Volume | $\begin{gathered} \hline 11: 00 \mathrm{AM} \\ 383 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 398 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 300 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 388 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 304 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 355 \end{gathered}$ | $\begin{gathered} \hline 11: 00 \mathrm{AM} \\ 476 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 357 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 372 \end{gathered}$ |  |
| PM Peak | 4:00 PM 455 | 4:00 PM 497 | 5:00 PM | $\begin{gathered} \text { 4:00 PM } \\ 459 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{PM} \\ 503 \end{gathered}$ | $\begin{gathered} \text { 4:00 PM } \\ 457 \end{gathered}$ | $\begin{gathered} 1: 00 \mathrm{PM} \\ 577 \end{gathered}$ | $\begin{gathered} \text { 8:00 PM } \\ 541 \end{gathered}$ | $\begin{gathered} \hline \text { 6:00 PM } \\ 473 \end{gathered}$ |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 11/2/2012 1:57 PM

| LOCATION: SPECIFIC L CITY/STATE | Combined OCATION: Snoqualm | lume0 ft fro WA | Drivew orth Be | Snoqu ay |  | north of roundabout at | $\overline{\mathrm{E} \text { Nort }}$ | Way | DATE | QC JOB \#: 10822001 DIRECTION: NB/SB Oct 012012 - Oct 012012 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | $\begin{gathered} \text { Mon } \\ 01 \text {-Oct-12 } \end{gathered}$ | Tue | Wed | Thu | Fri | Average Weekday Hourly Traffic | Sat | Sun | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM | 213 |  |  |  |  | 213 |  |  | 213 | $\square$ |
| 1:00 AM | 142 |  |  |  |  | 142 |  |  | 142 | $\square$ |
| 2:00 AM | 101 |  |  |  |  | 101 |  |  | 101 |  |
| 3:00 AM | 76 |  |  |  |  | 76 |  |  | 76 | - |
| 4:00 AM | 44 |  |  |  |  | 44 |  |  | 44 | $\square$ |
| 5:00 AM | 76 |  |  |  |  | 76 |  |  | 76 | $\square$ |
| 6:00 AM | 126 |  |  |  |  | 126 |  |  | 126 |  |
| 7:00 AM | 205 |  |  |  |  | 205 |  |  | 205 |  |
| 8:00 AM | 207 |  |  |  |  | 207 |  |  | 207 | I |
| 9:00 AM | 288 |  |  |  |  | 288 |  |  | 288 | - |
| 10:00 AM | 334 |  |  |  |  | 334 |  |  | 334 |  |
| 11:00 AM | 138 |  |  |  |  | 138 |  |  | 138 | $\square$ |
| 12:00 PM |  |  |  |  |  |  |  |  |  |  |
| 1:00 PM |  |  |  |  |  | , |  | 0 |  |  |
| 2:00 PM |  |  |  |  |  | R |  |  | 1-9 |  |
| 3:00 PM |  |  |  |  |  | ded |  |  |  |  |
| 4:00 PM |  |  |  |  |  |  |  |  |  |  |
| 5:00 PM |  |  |  |  |  |  |  |  |  |  |
| 6:00 PM |  |  |  |  |  |  |  |  |  |  |
| 7:00 PM |  |  |  |  |  |  |  |  |  |  |
| 8:00 PM |  |  |  |  |  |  |  |  |  |  |
| 9:00 PM |  |  |  |  |  |  |  |  |  |  |
| 10:00 PM |  |  |  |  |  |  |  |  |  |  |
| 11:00 PM |  |  |  |  |  |  |  |  |  |  |
| Day Total | 1950 |  |  |  |  | 1950 |  |  | 1950 |  |
| \% Weekday |  |  |  |  |  |  |  |  |  |  |
| Average | 29.8\% |  |  |  |  |  |  |  |  |  |
| \% Week Average | 27.5\% |  |  |  |  | 100.0\% |  |  |  |  |
| AM Peak | 10:00 AM |  |  |  |  | 10:00 AM |  |  | 10:00 AM |  |
| Volume | 334 |  |  |  |  | 334 |  |  | 334 |  |
| PM Peak |  |  |  |  |  |  |  |  |  |  |
| Volume |  |  |  |  |  |  |  |  |  |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 11/2/2012 1:57 PM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net)

| LOCATION SPECIFIC CITY/STAT | Combined OCATION: <br> : Snoqualm | Volume-Ma 100 ft from mie, WA | ain Driveway North Bend | y to Snoqual Way | Imie Casino | orth of roundabout at | SE North Bend Way | DATE: | QC JOB \#: 10822001 DIRECTION: NB/SB Sep 172012 - Sep 212012 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Mon 17-Sep-12 | Tue <br> 18-Sep-12 | Wed 19-Sep-12 | Thu 20-Sep-12 | $\begin{gathered} \hline \text { Fri } \\ 21-\text { Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic |  |  | Average Weekday Profile |
| 12:00 AM | 197 | 158 | 114 | 121 | 278 | 174 |  |  | - |
| 1:00 AM | 131 | 170 | 92 | 92 | 184 | 134 |  |  | $\square$ |
| 2:00 AM | 93 | 99 | 75 | 89 | 133 | 98 |  |  |  |
| 3:00 AM | 73 | 68 | 62 | 49 | 101 | 71 |  |  | $\square$ |
| 4:00 AM | 44 | 65 | 42 | 40 | 75 | 53 |  |  | $\square$ |
| 5:00 AM | 59 | 59 | 54 | 57 | 74 | 61 |  |  | $\square$ |
| 6:00 AM | 132 | 70 | 123 | 128 | 82 | 107 |  |  | - |
| 7:00 AM | 215 | 99 | 176 | 208 | 119 | 163 |  |  |  |
| 8:00 AM | 226 | 125 | 215 | 231 | 172 | 194 |  |  |  |
| 9:00 AM | 278 | 128 | 253 | 288 | 204 | 230 |  |  |  |
| 10:00 AM | 329 | 224 | 290 | 354 | 304 | 300 |  |  |  |
| 11:00 AM | 383 | 398 | 300 | 388 | 346 | 363 |  |  |  |
| 12:00 PM | 391 | 226 | 339 | 370 | 421 | 349 |  |  |  |
| 1:00 PM | 434 | 354 | 450 | 436 | 453 | 425 | $\square$ |  |  |
| 2:00 PM | 439 | 343 | 387 | 403 | 492 | 413 |  |  | $\square$ |
| 3:00 PM | 436 | 396 | 418 | 438 | 517 | 441 |  |  | $\square$ |
| 4:00 PM | 455 | 497 | 488 | 459 | 485 | 477 |  |  |  |
| 5:00 PM | 426 | 478 | 489 | 440 | 602 | 487 | - |  | $\square$ |
| 6:00 PM | 402 | 493 | 479 | 449 | 687 | 502 |  |  | - |
| 7:00 PM | 398 | 399 | 389 | 434 | 819 | 488 |  |  |  |
| 8:00 PM | 363 | 327 | 316 | 442 | 617 | 413 |  |  | - |
| 9:00 PM | 382 | 275 | 277 | 404 | 606 | 389 |  |  | $\square$ |
| 10:00 PM | 346 | 218 | 201 | 359 | 680 | 361 |  |  | I |
| 11:00 PM | 237 | 166 | 167 | 302 | 516 | 278 |  |  |  |
| Day Total | 6869 | 5835 | 6196 | 6981 | 8967 | 6971 |  |  |  |
| \% Weekday Average | 98.5\% | 83.7\% | 88.9\% | 100.1\% | 128.6\% |  |  |  |  |
| \% Week Average |  |  |  |  |  |  |  |  |  |
| AM Peak Volume | $\begin{gathered} \hline 11: 00 \mathrm{AM} \\ 383 \\ \hline \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 398 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 300 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 388 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 346 \\ \hline \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 363 \end{gathered}$ |  |  |  |
| PM Peak Volume | $\begin{gathered} 4: 00 \text { PM } \\ 455 \\ \hline \end{gathered}$ | $\begin{gathered} 4: 00 \mathrm{PM} \\ 497 \\ \hline \end{gathered}$ | $\begin{gathered} 5: 00 \mathrm{PM} \\ 489 \\ \hline \end{gathered}$ | $\begin{gathered} 4: 00 \mathrm{PM} \\ 459 \\ \hline \end{gathered}$ | $\begin{gathered} 7: 00 \text { PM } \\ 819 \\ \hline \end{gathered}$ | $\begin{gathered} \text { 6:00 PM } \\ 502 \\ \hline \end{gathered}$ |  |  |  |
| Comments: |  |  |  |  |  |  |  |  |  |

Report generated on 11/2/2012 1:57 PM


Report generated on 11/2/2012 1:57 PM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net)

| LOCATION: Combined Volume-Main Driveway to Snoqualmie Casino north of roundabout at SE North Bend Way SPECIFIC LOCATION: 100 ft from North Bend Way <br> CITY/STATE: Snoqualmie, WA |  |  |  |  |  |  |  |  | QC JOB \#: 10822001DIRECTION: NB/SBDATE: Sep 17 2012-Sep 232012 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | $\begin{gathered} \text { Mon } \\ \text { 17-Sep-12 } \end{gathered}$ | Tue 18-Sep-12 | Wed 19-Sep-12 | Thu 20-Sep-12 | $\begin{gathered} \text { Fri } \\ \text { 21-Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | Sat 22-Sep-12 | $\begin{gathered} \text { Sun } \\ 23 \text {-Sep-12 } \end{gathered}$ | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM | 197 | 158 | 114 | 121 | 278 | 174 | 384 | 441 | 242 | $\square$ |
| 1:00 AM | 131 | 170 | 92 | 92 | 184 | 134 | 320 | 345 | 191 |  |
| 2:00 AM | 93 | 99 | 75 | 89 | 133 | 98 | 262 | 253 | 143 | $\square$ |
| 3:00 AM | 73 | 68 | 62 | 49 | 101 | 71 | 148 | 168 | 96 |  |
| 4:00 AM | 44 | 65 | 42 | 40 | 75 | 53 | 87 | 111 | 66 | $\square$ |
| 5:00 AM | 59 | 59 | 54 | 57 | 74 | 61 | 94 | 92 | 70 | - |
| 6:00 AM | 132 | 70 | 123 | 128 | 82 | 107 | 125 | 124 | 112 | - |
| 7:00 AM | 215 | 99 | 176 | 208 | 119 | 163 | 253 | 184 | 179 |  |
| 8:00 AM | 226 | 125 | 215 | 231 | 172 | 194 | 298 | 258 | 218 |  |
| 9:00 AM | 278 | 128 | 253 | 288 | 204 | 230 | 432 | 290 | 268 |  |
| 10:00 AM | 329 | 224 | 290 | 354 | 304 | 300 | 501 | 345 | 335 |  |
| 11:00 AM | 383 | 398 | 300 | 388 | 346 | 363 | 537 | 363 | 388 | $\square$ |
| 12:00 PM | 391 | 226 | 339 | 370 | 421 | 349 | 557 | 417 | 389 | , |
| 1:00 PM | 434 | 354 | 450 | 436 | 453 | 425 | 600 | 459 | 455 |  |
| 2:00 PM | 439 | 343 | 387 | 403 | 492 | 413 | 621 | 474 | 451 |  |
| 3:00 PM | 436 | 396 | 418 | 438 | 517 | 441 | 596 | 443 | 463 | $\square$ |
| 4:00 PM | 455 | 497 | 488 | 459 | 485 | 477 | 665 | 423 | 496 | I |
| 5:00 PM | 426 | 478 | 489 | 440 | 602 | 487 | 691 | 422 | 507 |  |
| 6:00 PM | 402 | 493 | 479 | 449 | 687 | 502 | 751 | 448 | 530 |  |
| 7:00 PM | 398 | 399 | 389 | 434 | 819 | 488 | 762 | 438 | 520 |  |
| 8:00 PM | 363 | 327 | 316 | 442 | 617 | 413 | 643 | 393 | 443 | ] |
| 9:00 PM | 382 | 275 | 277 | 404 | 606 | 389 | 602 | 361 | 415 | I |
| 10:00 PM | 346 | 218 | 201 | 359 | 680 | 361 | 790 | 293 | 412 | , |
| 11:00 PM | 237 | 166 | 167 | 302 | 516 | 278 | 598 | 234 | 317 | 1 |
| Day Total | 6869 | 5835 | 6196 | 6981 | 8967 | 6971 | 11317 | 7779 | 7706 |  |
| \% Weekday Average | 98.5\% | 83.7\% | 88.9\% | 100.1\% | 128.6\% |  |  |  |  |  |
| \% Week Average | 89.1\% | 75.7\% | 80.4\% | 90.6\% | 116.4\% | 90.5\% | 146.9\% | 100.9\% |  |  |
| AM Peak Volume | $\begin{gathered} 11: 00 \mathrm{AM} \\ 383 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 398 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 300 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 388 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 346 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 363 \end{gathered}$ | $\begin{gathered} \hline 11: 00 \mathrm{AM} \\ 537 \\ \hline \end{gathered}$ | $\begin{gathered} 12: 00 \text { AM } \\ 441 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 388 \end{gathered}$ |  |
| PM Peak Volume | $4: 00 \mathrm{PM}$ 455 | $\begin{gathered} 4: 00 \mathrm{PM} \\ 497 \end{gathered}$ | $\begin{gathered} 5: 00 \mathrm{PM} \\ 489 \end{gathered}$ | $\begin{gathered} 4: 00 \text { PM } \\ 459 \end{gathered}$ | $\begin{gathered} 7: 00 \mathrm{PM} \\ 819 \end{gathered}$ | $\begin{gathered} \text { 6:00 PM } \\ 502 \end{gathered}$ | $\begin{gathered} \hline 10: 00 \text { PM } \\ 790 \end{gathered}$ | $\begin{gathered} \text { 2:00 PM } \\ 474 \end{gathered}$ | $\begin{gathered} \text { 6:00 PM } \\ 530 \end{gathered}$ |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 11/2/2012 1:57 PM

| LOCATION: West Driveway to Snoqualmie Casino SPECIFIC LOCATION: 100 ft from North Bend Way CITY/STATE: Snoqualmie , WA |  |  |  |  |  |  |  |  | QC JOB \#: 10822002DIRECTION: NBDATE: Sep 20 2012 - Sep 232012 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Mon | Tue | Wed | Thu 20-Sep-12 | $\begin{gathered} \text { Fri } \\ 21-\text { Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | $\begin{gathered} \text { Sat } \\ 22-\text { Sep-12 } \end{gathered}$ | Sun 23-Sep-12 | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM |  |  |  |  | 8 | 8 | 5 | 64 | 26 | - |
| 1:00 AM |  |  |  |  | 11 | 11 | 14 | 56 | 27 | - |
| 2:00 AM |  |  |  |  | 1 | 1 | 4 | 80 | 28 | - |
| 3:00 AM |  |  |  |  | 4 | 4 | 2 | 26 | 11 | - |
| 4:00 AM |  |  |  |  | 5 | 5 | 3 | 20 | 9 | - |
| 5:00 AM |  |  |  |  | 20 | 20 | 12 | 16 | 16 | $\square$ |
| 6:00 AM |  |  |  |  | 28 | 28 | 26 | 14 | 23 | - |
| 7:00 AM |  |  |  |  | 54 | 54 | 34 | 14 | 34 |  |
| 8:00 AM |  |  |  |  | 64 | 64 | 59 | 29 | 51 | $\square$ |
| 9:00 AM |  |  |  |  | 73 | 73 | 84 | 24 | 60 |  |
| 10:00 AM |  |  |  |  | 70 | 70 | 62 | 54 | 62 |  |
| 11:00 AM |  |  |  |  | 99 | 99 | 55 | 39 | 64 |  |
| 12:00 PM |  |  |  |  | 93 | 93 | 46 | 41 | 60 | $\square$ |
| 1:00 PM |  |  |  |  | 109 | 109 | 68 | 49 | 75 |  |
| 2:00 PM |  |  |  |  | 103 | 103 | 54 | 59 | 72 |  |
| 3:00 PM |  |  |  | 0 | 120 | - 60 | 68 | 36 | 56 | $\square$ |
| 4:00 PM |  |  |  | 0 | 119 | 60 | 68 | 61 | 62 |  |
| 5:00 PM |  |  |  | 0 | 158 | 79 | 95 | 55 | 77 |  |
| 6:00 PM |  |  |  | 0 | 120 | 60 | 98 | 77 | 74 |  |
| 7:00 PM |  |  |  | 0 | 121 | 61 | 61 | 42 | 56 |  |
| 8:00 PM |  |  |  | 0 | 74 | 37 | 61 | 56 | 48 | $\square$ |
| 9:00 PM |  |  |  | 0 | 63 | 32 | 45 | 26 | 34 |  |
| 10:00 PM |  |  |  | 0 | 28 | 14 | 99 | 49 | 44 |  |
| 11:00 PM |  |  |  | 0 | 18 | 9 | 62 | 45 | 31 |  |
| Day Total |  |  |  | 0 | 1563 | 1154 | 1185 | 1032 | 1100 |  |
| \% Weekday |  |  |  |  |  |  |  |  |  |  |
| Average |  |  |  | 0.0\% | 135.4\% |  |  |  |  |  |
| \% Week <br> Average |  |  |  | 0.0\% | 142.1\% | 104.9\% | 107.7\% | 93.8\% |  |  |
| AM Peak |  |  |  |  | 11:00 AM | 11:00 AM | 9:00 AM | 2:00 AM | 11:00 AM |  |
| Volume |  |  |  |  | 99 | 99 | 84 | 80 | 64 |  |
| PM Peak |  |  |  | 3:00 PM | 5:00 PM | 1:00 PM | 10:00 PM | 6:00 PM | 5:00 PM |  |
| Volume |  |  |  | 0 | 158 | 109 | 99 | 77 | 77 |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 11/2/2012 1:57 PM

| LOCATION: West Driveway to Snoqualmie Casino SPECIFIC LOCATION: 100 ft from North Bend Way CITY/STATE: Snoqualmie , WA |  |  |  |  |  |  |  |  | QC JOB \#: 10822002DIRECTION: NBDATE: Sep 24 2012 - Sep 302012 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | $\begin{gathered} \text { Mon } \\ 24-\text { Sep-12 } \end{gathered}$ | Tue 25-Sep-12 | Wed 26-Sep-12 | $\begin{gathered} \text { Thu } \\ \text { 27-Sep-12 } \end{gathered}$ | Fri 28-Sep-12 | Average Weekday Hourly Traffic | Sat 29-Sep-12 | $\begin{array}{\|c} \text { Sun } \\ 30-\text { Sep-12 } \end{array}$ | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM | 45 | 33 | 25 | 31 | 39 | 35 | 76 | 74 | 46 |  |
| 1:00 AM | 33 | 18 | 13 | 22 | 19 | 21 | 44 | 39 | 27 | $\square$ |
| 2:00 AM | 23 | 30 | 21 | 27 | 28 | 26 | 61 | 69 | 37 | - |
| 3:00 AM | 8 | 16 | 7 | 7 | 18 | 11 | 26 | 41 | 18 | $\square$ |
| 4:00 AM | 16 | 4 | 10 | 7 | 16 | 11 | 19 | 20 | 13 | $\square$ |
| 5:00 AM | 6 | 7 | 8 | 6 | 8 | 7 | 5 | 12 | 7 | - |
| 6:00 AM | 14 | 9 | 13 | 18 | 11 | 13 | 17 | 15 | 14 | $\square$ |
| 7:00 AM | 26 | 21 | 18 | 23 | 8 | 19 | 18 | 20 | 19 | $\square$ |
| 8:00 AM | 48 | 26 | 33 | 38 | 28 | 35 | 34 | 30 | 34 |  |
| 9:00 AM | 32 | 18 | 21 | 27 | 32 | 26 | 27 | 29 | 27 | $\square$ |
| 10:00 AM | 42 | 16 | 35 | 52 | 22 | 33 | 50 | 39 | 37 | - |
| 11:00 AM | 42 | 16 | 37 | 37 | 23 | 31 | 45 | 33 | 33 | $\square$ |
| 12:00 PM | 40 | 20 | 48 | 41 | 32 | 36 | 68 | 38 | 41 | $\square$ |
| 1:00 PM | 47 | 50 | 55 | 51 | 41 | 49 | 94 | 58 | 57 | $\square$ |
| 2:00 PM | 84 | 46 | 45 | 59 | 47 | 56 | 127 | 66 | 68 | - |
| 3:00 PM | 62 | 54 | 67 | 63 | 44 | 58 | 101 | 35 | 61 | $\square$ |
| 4:00 PM | 86 | 82 | 81 | 104 | 63 | 83 | 74 | 66 | 79 | $\square$ |
| 5:00 PM | 65 | 615 | 83 | 79 | 47 | 178 | 86 | 48 | 146 |  |
| 6:00 PM | 85 | 345 | 100 | 98 | 88 | 143 | 100 | 80 | 128 | - |
| 7:00 PM | 55 | 90 | 66 | 69 | 92 | 74 | 68 | 47 | 70 | $\square$ |
| 8:00 PM | 54 | 57 | 50 | 68 | 74 | 61 | 60 | 86 | 64 | $\square$ |
| 9:00 PM | 39 | 48 | 43 | 58 | 46 | 47 | 51 | 36 | 46 |  |
| 10:00 PM | 61 | 45 | 66 | 66 | 61 | 60 | 66 | 38 | 58 |  |
| 11:00 PM | 34 | 26 | 41 | 33 | 53 | 37 | 57 | 56 | 43 | 1 |
| Day Total | 1047 | 1692 | 986 | 1084 | 940 | 1150 | 1374 | 1075 | 1173 |  |
| \% Weekday Average | 90.7\% | 147.1\% | 85.7\% | 94.3\% | 81.7\% |  |  |  |  |  |
| \% Week Average | 95.2\% | 144.2\% | 84.1\% | 92.4\% | 80.1\% | 98.0\% | 117.1\% | 91.6\% |  |  |
| AM Peak Volume | $\begin{gathered} 8: 00 \mathrm{AM} \\ 48 \end{gathered}$ | $\begin{gathered} 12: 00 \mathrm{AM} \\ 33 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 37 \end{gathered}$ | $\begin{gathered} \text { 10:00 AM } \\ 52 \end{gathered}$ | $\begin{gathered} 12: 00 \mathrm{AM} \\ 39 \end{gathered}$ | $\begin{gathered} 12: 00 \mathrm{AM} \\ 35 \end{gathered}$ | $\begin{gathered} 12: 00 \mathrm{AM} \\ 76 \end{gathered}$ | $\begin{gathered} 12: 00 \mathrm{AM} \\ 74 \end{gathered}$ | $\begin{gathered} 12: 00 \mathrm{AM} \\ 46 \end{gathered}$ |  |
| PM Peak Volume | $\begin{gathered} 4: 00 \text { PM } \\ 86 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 615 \end{gathered}$ | $\begin{gathered} 6: 00 \mathrm{PM} \\ 100 \end{gathered}$ | $\begin{gathered} \text { 4:00 PM } \\ 104 \end{gathered}$ | $\begin{gathered} \text { 7:00 PM } \\ 92 \end{gathered}$ | $\begin{gathered} 5: 00 \text { PM } \\ 178 \end{gathered}$ | $\begin{gathered} \text { 2:00 PM } \\ 127 \end{gathered}$ | $\begin{gathered} 8: 00 \text { PM } \\ 86 \end{gathered}$ | $\begin{gathered} 5: 00 \text { PM } \\ 146 \end{gathered}$ |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 11/2/2012 1:57 PM

| LOCATION: SPECIFIC L CITY/STATE | West Drive OCATION: <br> E: Snoqualm | ay to 00 ft fr , WA | ualmie orth Be |  |  |  |  |  | DAT | QC JOB \#: 10822002 DIRECTION: NB Oct 012012 - Oct 012012 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | $\begin{gathered} \text { Mon } \\ 01-O c t-12 \end{gathered}$ | Tue | Wed | Thu | Fri | Average Weekday Hourly Traffic | Sat | Sun | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM | 38 |  |  |  |  | 38 |  |  | 38 | $\square$ |
| 1:00 AM | 30 |  |  |  |  | 30 |  |  | 30 |  |
| 2:00 AM | 29 |  |  |  |  | 29 |  |  | 29 | $\square$ |
| 3:00 AM | 14 |  |  |  |  | 14 |  |  | 14 | $\square$ |
| 4:00 AM | 13 |  |  |  |  | 13 |  |  | 13 | - |
| 5:00 AM | 8 |  |  |  |  | 8 |  |  | 8 | $\square$ |
| 6:00 AM | 12 |  |  |  |  | 12 |  |  | 12 | $\square$ |
| 7:00 AM | 21 |  |  |  |  | 21 |  |  | 21 |  |
| 8:00 AM | 34 |  |  |  |  | 34 |  |  | 34 |  |
| 9:00 AM | 27 |  |  |  |  | 27 |  |  | 27 | $\square$ |
| 10:00 AM | 42 |  |  |  |  | 42 |  |  | 42 |  |
| 11:00 AM | 14 |  |  |  |  | 14 |  |  | 14 | $\square$ |
| 12:00 PM |  |  |  |  |  |  |  |  |  |  |
| 1:00 PM |  |  |  |  |  |  |  | $=$ |  |  |
| 2:00 PM |  |  |  |  |  |  |  |  |  |  |
| 3:00 PM |  |  |  |  |  |  |  |  |  |  |
| 4:00 PM |  |  |  |  |  |  |  |  |  |  |
| 5:00 PM |  |  |  |  |  |  |  |  |  |  |
| 6:00 PM |  |  |  |  |  |  |  |  |  |  |
| 7:00 PM |  |  |  |  |  |  |  |  |  |  |
| 8:00 PM |  |  |  |  |  |  |  |  |  |  |
| 9:00 PM |  |  |  |  |  |  |  |  |  |  |
| 10:00 PM |  |  |  |  |  |  |  |  |  |  |
| 11:00 PM |  |  |  |  |  |  |  |  |  |  |
| Day Total | 282 |  |  |  |  | 282 |  |  | 282 |  |
| \% Weekday |  |  |  |  |  |  |  |  |  |  |
| Average | 24.5\% |  |  |  |  |  |  |  |  |  |
| \% Week |  |  |  |  |  |  |  |  |  |  |
| Average | 24.0\% |  |  |  |  | 100.0\% |  |  |  |  |
| AM Peak | 10:00 AM |  |  |  |  | 10:00 AM |  |  | 10:00 AM |  |
| Volume | 42 |  |  |  |  | 42 |  |  | 42 |  |
| PM Peak |  |  |  |  |  |  |  |  |  |  |
| Volume |  |  |  |  |  |  |  |  |  |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 11/2/2012 1:57 PM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net)

| LOCATION: SPECIFIC L CITY/STATE | West Drive OCATION: <br> E: Snoqualm | eway to Sno 100 ft from mie, WA | qualmie Ca North Bend |  |  |  |  | DATE | QC JOB \#: 10822002 DIRECTION: NB <br> Sep 172012 - Sep 212012 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Mon 17-Sep-12 | Tue 18-Sep-12 | Wed 19-Sep-12 | Thu 20-Sep-12 | $\begin{gathered} \hline \text { Fri } \\ \text { 21-Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic |  |  | Average Weekday Profile |
| 12:00 AM | 45 | 33 | 25 | 31 | 8 | 28 |  |  | - |
| 1:00 AM | 33 | 18 | 13 | 22 | 11 | 19 |  |  | $\square$ |
| 2:00 AM | 23 | 30 | 21 | 27 | 1 | 20 |  |  | $\square$ |
| 3:00 AM | 8 | 16 | 7 | 7 | 4 | 8 |  |  | - |
| 4:00 AM | 16 | 4 | 10 | 7 | 5 | 8 |  |  | - |
| 5:00 AM | 6 | 7 | 8 | 6 | 20 | 9 |  |  | $\square$ |
| 6:00 AM | 14 | 9 | 13 | 18 | 28 | 16 |  |  | $\square$ |
| 7:00 AM | 26 | 21 | 18 | 23 | 54 | 28 |  |  | $\square$ |
| 8:00 AM | 48 | 26 | 33 | 38 | 64 | 42 |  |  |  |
| 9:00 AM | 32 | 18 | 21 | 27 | 73 | 34 |  |  | $\square$ |
| 10:00 AM | 42 | 16 | 35 | 52 | 70 | 43 |  |  | $\square$ |
| 11:00 AM | 42 | 16 | 37 | 37 | 99 | 46 |  |  |  |
| 12:00 PM | 40 | 20 | 48 | 41 | 93 | 48 |  |  | $\square$ |
| 1:00 PM | 47 | 50 | 55 | 51 | 109 | 62 | n |  | $\square$ |
| 2:00 PM | 84 | 46 | 45 | 59 | 103 | 67 |  |  | , |
| 3:00 PM | 62 | 54 | 67 | 0 | 120 | 61 |  |  | $\square$ |
| 4:00 PM | 86 | 82 | 81 | 0 | 119 | 74 |  |  | - |
| 5:00 PM | 65 | 615 | 83 | 0 | 158 | 184 |  |  |  |
| 6:00 PM | 85 | 345 | 100 | 0 | 120 | 130 |  |  |  |
| 7:00 PM | 55 | 90 | 66 | 0 | 121 | 66 |  |  |  |
| 8:00 PM | 54 | 57 | 50 | 0 | 74 | 47 |  |  |  |
| 9:00 PM | 39 | 48 | 43 | 0 | 63 | 39 |  |  | $\square$ |
| 10:00 PM | 61 | 45 | 66 | 0 | 28 | 40 |  |  |  |
| 11:00 PM | 34 | 26 | 41 | 0 | 18 | 24 |  |  | , |
| Day Total | 1047 | 1692 | 986 | 446 | 1563 | 1143 |  |  |  |
| \% Weekday Average | 91.6\% | 148.0\% | 86.3\% | 39.0\% | 136.7\% |  |  |  |  |
| \% Week Average |  |  |  |  |  |  |  |  |  |
| AM Peak Volume | $\begin{gathered} 8: 00 \mathrm{AM} \\ 48 \\ \hline \end{gathered}$ | $\begin{gathered} 12: 00 \mathrm{AM} \\ 33 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 37 \end{gathered}$ | $\begin{gathered} 10: 00 \mathrm{AM} \\ 52 \\ \hline \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 99 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 46 \end{gathered}$ |  |  |  |
| PM Peak Volume | $\begin{gathered} 4: 00 \text { PM } \\ 86 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 5: 00 \mathrm{PM} \\ 615 \\ \hline \end{gathered}$ | $\begin{gathered} 6: 00 \mathrm{PM} \\ 100 \\ \hline \end{gathered}$ | $\begin{gathered} \text { 2:00 PM } \\ 59 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 5: 00 \text { PM } \\ 158 \\ \hline \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 184 \\ \hline \end{gathered}$ |  |  |  |
| Comments: |  |  |  |  |  |  |  |  |  |

Report generated on 11/2/2012 1:57 PM


Report generated on 11/2/2012 1:57 PM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net)

| LOCATION: West Driveway to Snoqualmie Casino SPECIFIC LOCATION: 100 ft from North Bend Way CITY/STATE: Snoqualmie, WA |  |  |  |  |  |  |  |  | QC JOB \#: 10822002DIRECTION: NBDATE: $\operatorname{Sep} 17$ 2012-Sep 232012 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | $\begin{gathered} \text { Mon } \\ \text { 17-Sep-12 } \\ \hline \end{gathered}$ | Tue 18-Sep-12 | Wed 19-Sep-12 | Thu 20-Sep-12 | $\begin{gathered} \text { Fri } \\ 21-\text { Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | Sat 22-Sep-12 | $\begin{gathered} \text { Sun } \\ 23-\text { Sep-12 } \end{gathered}$ | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM | 45 | 33 | 25 | 31 | 8 | 28 | 5 | 64 | 30 | - |
| 1:00 AM | 33 | 18 | 13 | 22 | 11 | 19 | 14 | 56 | 24 | $\square$ |
| 2:00 AM | 23 | 30 | 21 | 27 | 1 | 20 | 4 | 80 | 27 | $\square$ |
| 3:00 AM | 8 | 16 | 7 | 7 | 4 | 8 | 2 | 26 | 10 | $\square$ |
| 4:00 AM | 16 | 4 | 10 | 7 | 5 | 8 | 3 | 20 | 9 | $\square$ |
| 5:00 AM | 6 | 7 | 8 | 6 | 20 | 9 | 12 | 16 | 11 | $\square$ |
| 6:00 AM | 14 | 9 | 13 | 18 | 28 | 16 | 26 | 14 | 17 | $\square$ |
| 7:00 AM | 26 | 21 | 18 | 23 | 54 | 28 | 34 | 14 | 27 | $\square$ |
| 8:00 AM | 48 | 26 | 33 | 38 | 64 | 42 | 59 | 29 | 42 |  |
| 9:00 AM | 32 | 18 | 21 | 27 | 73 | 34 | 84 | 24 | 40 |  |
| 10:00 AM | 42 | 16 | 35 | 52 | 70 | 43 | 62 | 54 | 47 |  |
| 11:00 AM | 42 | 16 | 37 | 37 | 99 | 46 | 55 | 39 | 46 |  |
| 12:00 PM | 40 | 20 | 48 | 41 | 93 | 48 | 46 | 41 | 47 | $\square$ |
| 1:00 PM | 47 | 50 | 55 | 51 | 109 | 62 | 68 | 49 | 61 | I |
| 2:00 PM | 84 | 46 | 45 | 59 | 103 | 67 | 54 | 59 | 64 |  |
| 3:00 PM | 62 | 54 | 67 | 0 | 120 | 61 | 68 | 36 | 58 | $\square$ |
| 4:00 PM | 86 | 82 | 81 | 0 | 119 | 74 | 68 | 61 | 71 | $\square$ |
| 5:00 PM | 65 | 615 | 83 | 0 | 158 | 184 | 95 | 55 | 153 |  |
| 6:00 PM | 85 | 345 | 100 | 0 | 120 | 130 | 98 | 77 | 118 | 」 |
| 7:00 PM | 55 | 90 | 66 | 0 | 121 | 66 | 61 | 42 | 62 | - |
| 8:00 PM | 54 | 57 | 50 | 0 | 74 | 47 | 61 | 56 | 50 | $\square$ |
| 9:00 PM | 39 | 48 | 43 | 0 | 63 | 39 | 45 | 26 | 38 | $\square$ |
| 10:00 PM | 61 | 45 | 66 | 0 | 28 | 40 | 99 | 49 | 50 | - |
| 11:00 PM | 34 | 26 | 41 | 0 | 18 | 24 | 62 | 45 | 32 |  |
| Day Total | 1047 | 1692 | 986 | 446 | 1563 | 1143 | 1185 | 1032 | 1134 |  |
| \% Weekday Average | 91.6\% | 148.0\% | 86.3\% | 39.0\% | 136.7\% |  |  |  |  |  |
| \% Week <br> Average | 92.3\% | 149.2\% | 86.9\% | 39.3\% | 137.8\% | 100.8\% | 104.5\% | 91.0\% |  |  |
| AM Peak Volume | $\begin{gathered} 8: 00 \mathrm{AM} \\ 48 \end{gathered}$ | $\begin{gathered} 12: 00 \mathrm{AM} \\ 33 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 37 \end{gathered}$ | $\begin{gathered} 10: 00 \mathrm{AM} \\ 52 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 99 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 46 \end{gathered}$ | $\begin{gathered} 9: 00 \mathrm{AM} \\ 84 \end{gathered}$ | $\begin{gathered} 2: 00 \mathrm{AM} \\ 80 \end{gathered}$ | $\begin{gathered} 10: 00 \mathrm{AM} \\ 47 \end{gathered}$ |  |
| PM Peak Volume | $\begin{gathered} \text { 4:00 PM } \\ 86 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 615 \\ \hline \end{gathered}$ | $\begin{gathered} \text { 6:00 PM } \\ 100 \\ \hline \end{gathered}$ | $\begin{gathered} 2: 00 \mathrm{PM} \\ 59 \\ \hline \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 158 \\ \hline \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 184 \end{gathered}$ | $\begin{gathered} 10: 00 \text { PM } \\ 99 \\ \hline \end{gathered}$ | $\begin{gathered} \text { 6:00 PM } \\ \quad 77 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 5: 00 \mathrm{PM} \\ 153 \\ \hline \end{gathered}$ |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 11/2/2012 1:57 PM


Report generated on 11/2/2012 1:57 PM

| LOCATION: West Driveway to Snoqualmie Casino SPECIFIC LOCATION: 100 ft from North Bend Way CITY/STATE: Snoqualmie , WA |  |  |  |  |  |  |  |  | QC JOB \#: 10822002DIRECTION:SBDATE: 24 2012 - Sep 302012 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Mon 24-Sep-12 | Tue 25-Sep-12 | Wed 26-Sep-12 | $\begin{gathered} \text { Thu } \\ \text { 27-Sep-12 } \end{gathered}$ | $\begin{gathered} \text { Fri } \\ 28-\text { Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | Sat 29-Sep-12 | $\begin{array}{\|c} \text { Sun } \\ 30-\text { Sep-12 } \end{array}$ | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM | 3 | 5 | 3 | 7 | 3 | 4 | 13 | 7 | 6 | $\square$ |
| 1:00 AM | 14 | 13 | 15 | 13 | 14 | 14 | 13 | 15 | 14 | $\square$ |
| 2:00 AM | 2 | 1 | 2 | 1 | 2 | 2 | 2 | 1 | 2 | , |
| 3:00 AM | 3 | 2 | 3 | 0 | 4 | 2 | 3 | 2 | 2 | , |
| 4:00 AM | 4 | 4 | 1 | 0 | 2 | 2 | 2 | 3 | 2 | , |
| 5:00 AM | 12 | 12 | 13 | 15 | 18 | 14 | 13 | 13 | 14 | $\square$ |
| 6:00 AM | 22 | 19 | 25 | 23 | 17 | 21 | 26 | 14 | 21 | $\square$ |
| 7:00 AM | 42 | 38 | 39 | 44 | 35 | 40 | 25 | 25 | 35 | $\square$ |
| 8:00 AM | 44 | 34 | 36 | 47 | 50 | 42 | 43 | 31 | 41 |  |
| 9:00 AM | 75 | 45 | 67 | 66 | 61 | 63 | 81 | 59 | 65 |  |
| 10:00 AM | 67 | 55 | 65 | 63 | 54 | 61 | 76 | 45 | 61 | - |
| 11:00 AM | 65 | 89 | 64 | 58 | 71 | 69 | 100 | 67 | 73 |  |
| 12:00 PM | 56 | 25 | 67 | 57 | 53 | 52 | 116 | 58 | 62 | $\square$ |
| 1:00 PM | 84 | 60 | 111 | 70 | 75 | 80 | 132 | 83 | 88 | - |
| 2:00 PM | 84 | 76 | 74 | 78 | 73 | 77 | 134 | 69 | 84 | $\square$ |
| 3:00 PM | 96 | 98 | 78 | 108 | 90 | 94 | 85 | 76 | 90 | - |
| 4:00 PM | 102 | 101 | 98 | 98 | 70 | 94 | 79 | 83 | 90 | - |
| 5:00 PM | 99 | 134 | 126 | 117 | 117 | 119 | 90 | 90 | 110 |  |
| 6:00 PM | 58 | 99 | 94 | 62 | 96 | 82 | 74 | 45 | 75 | $\square$ |
| 7:00 PM | 60 | 51 | 47 | 83 | 88 | 66 | 70 | 45 | 63 | - |
| 8:00 PM | 34 | 17 | 26 | 51 | 64 | 38 | 50 | 27 | 38 | $\square$ |
| 9:00 PM | 45 | 33 | 23 | 49 | 50 | 40 | 68 | 32 | 43 |  |
| 10:00 PM | 21 | 11 | 9 | 26 | 28 | 19 | 24 | 9 | 18 | $\square$ |
| 11:00 PM | 16 | 15 | 13 | 21 | 23 | 18 | 25 | 9 | 17 | $\square$ |
| Day Total | 1108 | 1037 | 1099 | 1157 | 1158 | 1113 | 1344 | 908 | 1114 |  |
| \% Weekday Average | 114.0\% | 93.2\% | 98.7\% | 104.0\% | 104.0\% |  |  |  |  |  |
| \% Week Average | 101.8\% | 93.1\% | 98.7\% | 103.9\% | 103.9\% | 99.9\% | 120.6\% | 81.5\% |  |  |
| AM Peak Volume | $\begin{gathered} 9: 00 \mathrm{AM} \\ 75 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 89 \end{gathered}$ | $\begin{gathered} 9: 00 \mathrm{AM} \\ 67 \end{gathered}$ | $\begin{gathered} 9: 00 \mathrm{AM} \\ 66 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 71 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 69 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 100 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 67 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 73 \end{gathered}$ |  |
| PM Peak | 4:00 PM 102 | 5:00 PM 134 | 5:00 PM 126 | 5:00 PM 117 | 5:00 PM | $\begin{gathered} \text { 5:00 PM } \\ 119 \end{gathered}$ | $\begin{gathered} \text { 2:00 PM } \\ 134 \end{gathered}$ | $\begin{gathered} 5: 00 \mathrm{PM} \\ 90 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 110 \end{gathered}$ |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 11/2/2012 1:57 PM

| LOCATION: SPECIFIC L CITY/STATE | West Drive OCATION: <br> : Snoqualm | ay to 00 ft fr , WA | ualmie orth Be |  |  |  |  |  | DATE | QC JOB \#: 10822002 DIRECTION: SB Oct 012012 - Oct 012012 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | $\begin{gathered} \text { Mon } \\ 01-\text { Oct-12 } \end{gathered}$ | Tue | Wed | Thu | Fri | Average Weekday Hourly Traffic | Sat | Sun | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM | 0 |  |  |  |  | 0 |  |  | 0 | 1 |
| 1:00 AM | 15 |  |  |  |  | 15 |  |  | 15 | $\square$ |
| 2:00 AM | 4 |  |  |  |  | 4 |  |  | 4 | $\square$ |
| 3:00 AM | 0 |  |  |  |  | 0 |  |  | 0 |  |
| 4:00 AM | 6 |  |  |  |  | 6 |  |  | 6 | $\square$ |
| 5:00 AM | 11 |  |  |  |  | 11 |  |  | 11 | $\square$ |
| 6:00 AM | 16 |  |  |  |  | 16 |  |  | 16 | $\square$ |
| 7:00 AM | 46 |  |  |  |  | 46 |  |  | 46 |  |
| 8:00 AM | 35 |  |  |  |  | 35 |  |  | 35 | $\square$ |
| 9:00 AM | 78 |  |  |  |  | 78 |  |  | 78 |  |
| 10:00 AM | 66 |  |  |  |  | 66 |  |  | 66 | ] |
| 11:00 AM | 17 |  |  |  |  | 17 |  |  | 17 | $\square$ |
| 12:00 PM |  |  |  |  |  |  |  |  |  |  |
| 1:00 PM |  |  |  |  |  |  |  | 0 |  |  |
| 2:00 PM |  |  |  |  |  |  |  |  |  |  |
| 3:00 PM |  |  |  |  |  |  |  |  |  |  |
| 4:00 PM |  |  |  |  |  |  |  |  |  |  |
| 5:00 PM |  |  |  |  |  |  |  |  |  |  |
| 6:00 PM |  |  |  |  |  |  |  |  |  |  |
| 7:00 PM |  |  |  |  |  |  |  |  |  |  |
| 8:00 PM |  |  |  |  |  |  |  |  |  |  |
| 9:00 PM |  |  |  |  |  |  |  |  |  |  |
| 10:00 PM |  |  |  |  |  |  |  |  |  |  |
| 11:00 PM |  |  |  |  |  |  |  |  |  |  |
| Day Total | 294 |  |  |  |  | 294 |  |  | 294 |  |
| \% Weekday |  |  |  |  |  |  |  |  |  |  |
| Average | 26.4\% |  |  |  |  |  |  |  |  |  |
| \% Week |  |  |  |  |  |  |  |  |  |  |
| Average | 26.4\% |  |  |  |  | 100.0\% |  |  |  |  |
| AM Peak | 9:00 AM |  |  |  |  | 9:00 AM |  |  | 9:00 AM |  |
| Volume | 78 |  |  |  |  | 78 |  |  | 78 |  |
| PM Peak |  |  |  |  |  |  |  |  |  |  |
| Volume |  |  |  |  |  |  |  |  |  |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 11/2/2012 1:57 PM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net)

| LOCATION: West Driveway to Snoqualmie Casino SPECIFIC LOCATION: 100 ft from North Bend Way CITY/STATE: Snoqualmie, WA |  |  |  |  |  |  | QC JOB \#: 10822002DIRECTION: SBDATE: $\operatorname{Sep} 172012$ - Sep 212012 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | $\begin{gathered} \text { Mon } \\ \text { 17-Sep-12 } \end{gathered}$ | Tue 18-Sep-12 | Wed 19-Sep-12 | Thu <br> 20-Sep-12 | $\begin{gathered} \text { Fri } \\ 21-\text { Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic |  |  | Average Weekday Profile |
| 12:00 AM | 3 | 5 | 3 | 7 | 41 | 12 |  |  | - |
| 1:00 AM | 14 | 13 | 15 | 13 | 22 | 15 |  |  | - |
| 2:00 AM | 2 | 1 | 2 | 1 | 40 | 9 |  |  | $\square$ |
| 3:00 AM | 3 | 2 | 3 | 0 | 14 | 4 |  |  |  |
| 4:00 AM | 4 | 4 | 1 | 0 | 17 | 5 |  |  |  |
| 5:00 AM | 12 | 12 | 13 | 15 | 8 | 12 |  |  | $\square$ |
| 6:00 AM | 22 | 19 | 25 | 23 | 14 | 21 |  |  |  |
| 7:00 AM | 42 | 38 | 39 | 44 | 26 | 38 |  |  |  |
| 8:00 AM | 44 | 34 | 36 | 47 | 50 | 42 |  |  |  |
| 9:00 AM | 75 | 45 | 67 | 66 | 51 | 61 |  |  |  |
| 10:00 AM | 67 | 55 | 65 | 63 | 38 | 58 |  |  | - |
| 11:00 AM | 65 | 89 | 64 | 58 | 59 | 67 |  |  |  |
| 12:00 PM | 56 | 25 | 67 | 57 | 54 | 52 |  |  | $\square$ |
| 1:00 PM | 84 | 60 | 111 | 70 | 70 | 79 | 0 |  |  |
| 2:00 PM | 84 | 76 | 74 | 78 | 69 | 76 |  |  | $\square$ |
| 3:00 PM | 96 | 98 | 78 | 0 | 90 | 72 |  |  | , |
| 4:00 PM | 102 | 101 | 98 | 0 | 98 | 80 |  |  | $\square$ |
| 5:00 PM | 99 | 134 | 126 | 0 | 102 | 92 |  |  |  |
| 6:00 PM | 58 | 99 | 94 | 0 | 100 | 70 |  |  | $\square$ |
| 7:00 PM | 60 | 51 | 47 | 0 | 111 | 54 |  |  | ] |
| 8:00 PM | 34 | 17 | 26 | 0 | 77 | 31 |  |  | $\square$ |
| 9:00 PM | 45 | 33 | 23 | 0 | 60 | 32 |  |  |  |
| 10:00 PM | 21 | 11 | 9 | 0 | 97 | 28 |  |  |  |
| 11:00 PM | 16 | 15 | 13 | 0 | 59 | 21 |  |  |  |
| Day Total | 1108 | 1037 | 1099 | 542 | 1367 | 1031 |  |  |  |
| \% Weekday Average | 107.5\% | 100.6\% | 106.6\% | 52.6\% | 132.6\% |  |  |  |  |
| \% Week Average |  |  |  |  |  |  |  |  |  |
| AM Peak Volume | $\begin{gathered} 9: 00 \mathrm{AM} \\ 75 \\ \hline \end{gathered}$ | $\begin{gathered} \text { 11:00 AM } \\ 89 \end{gathered}$ | $\begin{gathered} 9: 00 \mathrm{AM} \\ 67 \\ \hline \end{gathered}$ | $\begin{gathered} 9: 00 \mathrm{AM} \\ 66 \end{gathered}$ | $\begin{gathered} \text { 11:00 AM } \\ 59 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 67 \\ \hline \end{gathered}$ |  |  |  |
| PM Peak Volume | $\begin{gathered} \hline 4: 00 \text { PM } \\ 102 \\ \hline \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 134 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 5: 00 \text { PM } \\ 126 \\ \hline \end{gathered}$ | $\begin{gathered} 2: 00 \text { PM } \\ 78 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 7: 00 \mathrm{PM} \\ 111 \\ \hline \end{gathered}$ | $\begin{gathered} 5: 00 \text { PM } \\ 92 \\ \hline \end{gathered}$ |  |  |  |
| Comments: |  |  |  |  |  |  |  |  |  |

Report generated on 11/2/2012 1:57 PM


Report generated on 11/2/2012 1:57 PM

| LOCATION: West Driveway to Snoqualmie Casino SPECIFIC LOCATION: 100 ft from North Bend Way CITY/STATE: Snoqualmie , WA |  |  |  |  |  |  |  |  | QC JOB \#: 10822002DIRECTION: SBDATE: Sep 172012 - Sep 232012 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | $\begin{gathered} \text { Mon } \\ \text { 17-Sep-12 } \end{gathered}$ | Tue 18-Sep-12 | Wed 19-Sep-12 | Thu $20-\text { Sep-12 }$ | $\begin{gathered} \text { Fri } \\ 21-\text { Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | $\begin{gathered} \text { Sat } \\ \text { 22-Sep-12 } \end{gathered}$ | Sun 23-Sep-12 | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM | 3 | 5 | 3 | 7 | 41 | 12 | 58 | 9 | 18 | - |
| 1:00 AM | 14 | 13 | 15 | 13 | 22 | 15 | 36 | 15 | 18 | $\square$ |
| 2:00 AM | 2 | 1 | 2 | 1 | 40 | 9 | 66 | 1 | 16 | $\square$ |
| 3:00 AM | 3 | 2 | 3 | 0 | 14 | 4 | 38 | 4 | 9 | $\square$ |
| 4:00 AM | 4 | 4 | 1 | 0 | 17 | 5 | 17 | 3 | 7 | $\square$ |
| 5:00 AM | 12 | 12 | 13 | 15 | 8 | 12 | 9 | 12 | 12 | - |
| 6:00 AM | 22 | 19 | 25 | 23 | 14 | 21 | 14 | 15 | 19 |  |
| 7:00 AM | 42 | 38 | 39 | 44 | 26 | 38 | 35 | 24 | 35 |  |
| 8:00 AM | 44 | 34 | 36 | 47 | 50 | 42 | 58 | 34 | 43 |  |
| 9:00 AM | 75 | 45 | 67 | 66 | 51 | 61 | 52 | 66 | 60 |  |
| 10:00 AM | 67 | 55 | 65 | 63 | 38 | 58 | 57 | 62 | 58 |  |
| 11:00 AM | 65 | 89 | 64 | 58 | 59 | 67 | 66 | 85 | 69 |  |
| 12:00 PM | 56 | 25 | 67 | 57 | 54 | 52 | 65 | 59 | 55 | $\square$ |
| 1:00 PM | 84 | 60 | 111 | 70 | 70 | 79 | 93 | 75 | 80 | - |
| 2:00 PM | 84 | 76 | 74 | 78 | 69 | 76 | 89 | 69 | 77 | I |
| 3:00 PM | 96 | 98 | 78 | 0 | 90 | 72 | 100 | 75 | 77 | $\square$ |
| 4:00 PM | 102 | 101 | 98 | 0 | 98 | 80 | 100 | 72 | 82 | $\square$ |
| 5:00 PM | 99 | 134 | 126 | 0 | 102 | 92 | 129 | 87 | 97 |  |
| 6:00 PM | 58 | 99 | 94 | 0 | 100 | 70 | 104 | 36 | 70 | ] |
| 7:00 PM | 60 | 51 | 47 | 0 | 111 | 54 | 84 | 50 | 58 | 」 |
| 8:00 PM | 34 | 17 | 26 | 0 | 77 | 31 | 53 | 28 | 34 | $\square$ |
| 9:00 PM | 45 | 33 | 23 | 0 | 60 | 32 | 70 | 38 | 38 |  |
| 10:00 PM | 21 | 11 | 9 | 0 | 97 | 28 | 15 | 9 | 23 |  |
| 11:00 PM | 16 | 15 | 13 | 0 | 59 | 21 | 21 | 12 | 19 |  |
| Day Total | 1108 | 1037 | 1099 | 542 | 1367 | 1031 | 1429 | 940 | 1074 |  |
| \% Weekday Average | 107.5\% | 100.6\% | 106.6\% | 52.6\% | 132.6\% |  |  |  |  |  |
| \% Week <br> Average | 103.2\% | 96.6\% | 102.3\% | 50.5\% | 127.3\% | 96.0\% | 133.1\% | 87.5\% |  |  |
| AM Peak Volume | $\begin{gathered} 9: 00 \mathrm{AM} \\ 75 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 89 \end{gathered}$ | 9:00 AM | $\begin{gathered} 9: 00 \mathrm{AM} \\ 66 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 59 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 67 \end{gathered}$ | $\begin{gathered} 2: 00 \mathrm{AM} \\ 66 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 85 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 69 \end{gathered}$ |  |
| PM Peak Volume | $\begin{gathered} \hline 4: 00 \mathrm{PM} \\ 102 \\ \hline \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 134 \\ \hline \end{gathered}$ | $\begin{gathered} 5: 00 \mathrm{PM} \\ 126 \\ \hline \end{gathered}$ | $\begin{gathered} 2: 00 \mathrm{PM} \\ 78 \\ \hline \end{gathered}$ | $\begin{gathered} 7: 00 \text { PM } \\ 111 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 92 \\ \hline \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 129 \\ \hline \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 87 \end{gathered}$ | $\begin{gathered} 5: 00 \mathrm{PM} \\ 97 \\ \hline \end{gathered}$ |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 11/2/2012 1:57 PM

| LOCATION: West Driveway to Snoqualmie Casino SPECIFIC LOCATION: 100 ft from North Bend Way CITY/STATE: Snoqualmie , WA |  |  |  |  |  |  |  |  | QC JOB \#: 10822002DIRECTION: NB/SBDATE: Sep 20 2012 - Sep 232012 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Mon | Tue | Wed | Thu 20-Sep-12 | $\begin{gathered} \text { Fri } \\ 21-\text { Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | $\begin{gathered} \text { Sat } \\ 22-\text { Sep-12 } \end{gathered}$ | $\begin{gathered} \text { Sun } \\ 23-\text { Sep-12 } \end{gathered}$ | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM |  |  |  |  | 49 | 49 | 63 | 73 | 62 | $\square$ |
| 1:00 AM |  |  |  |  | 33 | 33 | 50 | 71 | 51 | $\square$ |
| 2:00 AM |  |  |  |  | 41 | 41 | 70 | 81 | 64 | $\square$ |
| 3:00 AM |  |  |  |  | 18 | 18 | 40 | 30 | 29 | $\square$ |
| 4:00 AM |  |  |  |  | 22 | 22 | 20 | 23 | 22 | $\square$ |
| 5:00 AM |  |  |  |  | 28 | 28 | 21 | 28 | 26 | $\square$ |
| 6:00 AM |  |  |  |  | 42 | 42 | 40 | 29 | 37 | $\square$ |
| 7:00 AM |  |  |  |  | 80 | 80 | 69 | 38 | 62 |  |
| 8:00 AM |  |  |  |  | 114 | 114 | 117 | 63 | 98 | $\square$ |
| 9:00 AM |  |  |  |  | 124 | 124 | 136 | 90 | 117 | - |
| 10:00 AM |  |  |  |  | 108 | 108 | 119 | 116 | 114 | $\square$ |
| 11:00 AM |  |  |  |  | 158 | 158 | 121 | 124 | 134 |  |
| 12:00 PM |  |  |  |  | 147 | 147 | 111 | 100 | 119 | $\square$ |
| 1:00 PM |  |  |  |  | 179 | 179 | 161 | 124 | 155 |  |
| 2:00 PM |  |  |  |  | 172 | 172 | 143 | 128 | 148 |  |
| 3:00 PM |  |  |  | 0 | 210 | 105 | 168 | 111 | 122 - | ] |
| 4:00 PM |  |  |  | 0 | 217 | 109 | 168 | 133 | 130 | I |
| 5:00 PM |  |  |  | 0 | 260 | 130 | 224 | 142 | 157 |  |
| 6:00 PM |  |  |  | 0 | 220 | 110 | 202 | 113 | 134 | $\square$ |
| 7:00 PM |  |  |  | 0 | 232 | 116 | 145 | 92 | 117 | ] |
| 8:00 PM |  |  |  | 0 | 151 | 76 | 114 | 84 | 87 | - |
| 9:00 PM |  |  |  | 0 | 123 | 62 | 115 | 64 | 76 | $\square$ |
| 10:00 PM |  |  |  | 0 | 125 | 63 | 114 | 58 | 74 | $\square$ |
| 11:00 PM |  |  |  | 0 | 77 | 39 | 83 | 57 | 54 |  |
| Day Total |  |  |  | 0 | 2930 | 2125 | 2614 | 1972 | 2189 |  |
| \% Weekday Average |  |  |  | 0.0\% | 137.9\% |  |  |  |  |  |
| \% Week Average |  |  |  | 0.0\% | 133.9\% | 97.1\% | 119.4\% | 90.1\% |  |  |
| AM Peak Volume |  |  |  |  | $\begin{gathered} 11: 00 \text { AM } \\ 158 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 158 \end{gathered}$ | $\begin{gathered} 9: 00 \mathrm{AM} \\ 136 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 124 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 134 \end{gathered}$ |  |
| PM Peak Volume |  |  |  | $\begin{gathered} 3: 00 \text { PM } \\ 0 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 260 \end{gathered}$ | $\begin{gathered} 1: 00 \text { PM } \\ 179 \end{gathered}$ | $\begin{gathered} 5: 00 \text { PM } \\ 224 \end{gathered}$ | $\begin{gathered} 5: 00 \mathrm{PM} \\ 142 \end{gathered}$ | $\begin{gathered} 5: 00 \text { PM } \\ 157 \end{gathered}$ |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 11/2/2012 1:57 PM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net)

| LOCATION: West Driveway to Snoqualmie Casino SPECIFIC LOCATION: 100 ft from North Bend Way CITY/STATE: Snoqualmie, WA |  |  |  |  |  |  |  |  | QC JOB \#: 10822002DIRECTION: NB/SBDATE: Sep 242012 - Sep 302012 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Mon 24-Sep-12 | Tue 25-Sep-12 | Wed 26-Sep-12 | Thu <br> 27-Sep-12 | Fri 28-Sep-12 | Average Weekday Hourly Traffic | Sat 29-Sep-12 | $\begin{gathered} \text { Sun } \\ 30-\text { Sep-12 } \end{gathered}$ | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM | 48 | 38 | 28 | 38 | 42 | 39 | 89 | 81 | 52 | ] |
| 1:00 AM | 47 | 31 | 28 | 35 | 33 | 35 | 57 | 54 | 41 | $\square$ |
| 2:00 AM | 25 | 31 | 23 | 28 | 30 | 27 | 63 | 70 | 39 | - |
| 3:00 AM | 11 | 18 | 10 | 7 | 22 | 14 | 29 | 43 | 20 | $\square$ |
| 4:00 AM | 20 | 8 | 11 | 7 | 18 | 13 | 21 | 23 | 15 | $\square$ |
| 5:00 AM | 18 | 19 | 21 | 21 | 26 | 21 | 18 | 25 | 21 | $\square$ |
| 6:00 AM | 36 | 28 | 38 | 41 | 28 | 34 | 43 | 29 | 35 | $\square$ |
| 7:00 AM | 68 | 59 | 57 | 67 | 43 | 59 | 43 | 45 | 55 |  |
| 8:00 AM | 92 | 60 | 69 | 85 | 78 | 77 | 77 | 61 | 75 |  |
| 9:00 AM | 107 | 63 | 88 | 93 | 93 | 89 | 108 | 88 | 91 |  |
| 10:00 AM | 109 | 71 | 100 | 115 | 76 | 94 | 126 | 84 | 97 |  |
| 11:00 AM | 107 | 105 | 101 | 95 | 94 | 100 | 145 | 100 | 107 |  |
| 12:00 PM | 96 | 45 | 115 | 98 | 85 | 88 | 184 | 96 | 103 | $\square$ |
| 1:00 PM | 131 | 110 | 166 | 121 | 116 | 129 | 226 | 141 | 144 |  |
| 2:00 PM | 168 | 122 | 119 | 137 | 120 | 133 | 261 | 135 | 152 | - |
| 3:00 PM | 158 | 152 | 145 | 171 | 134 | 152 | 186 | 111 | 151 | $\square$ |
| 4:00 PM | 188 | 183 | 179 | 202 | 133 | 177 | 153 | 149 | 170 | - |
| 5:00 PM | 164 | 749 | 209 | 196 | 164 | 296 | 176 | 138 | 257 |  |
| 6:00 PM | 143 | 444 | 194 | 160 | 184 | 225 | 174 | 125 | 203 | 」 |
| 7:00 PM | 115 | 141 | 113 | 152 | 180 | 140 | 138 | 92 | 133 | $\square$ |
| 8:00 PM | 88 | 74 | 76 | 119 | 138 | 99 | 110 | 113 | 103 | - |
| 9:00 PM | 84 | 81 | 66 | 107 | 96 | 87 | 119 | 68 | 89 | - |
| 10:00 PM | 82 | 56 | 75 | 92 | 89 | 79 | 90 | 47 | 76 |  |
| 11:00 PM | 50 | 41 | 54 | 54 | 76 | 55 | 82 | 65 | 60 | 1 |
| Day Total | 2155 | 2729 | 2085 | 2241 | 2098 | 2262 | 2718 | 1983 | 2289 |  |
| \% Weekday Average | 101.4\% | 120.6\% | 92.2\% | 99.1\% | 92.7\% |  |  |  |  |  |
| \% Week Average | 98.4\% | 119.2\% | 91.1\% | 97.9\% | 91.7\% | 98.8\% | 118.7\% | 86.6\% |  |  |
| AM Peak Volume | $\begin{gathered} 10: 00 \mathrm{AM} \\ 109 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 105 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 101 \end{gathered}$ | $\begin{gathered} 10: 00 \mathrm{AM} \\ 115 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 94 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 100 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 145 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 100 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 107 \end{gathered}$ |  |
| PM Peak Volume | $\begin{gathered} \text { 4:00 PM } \\ 188 \end{gathered}$ | $\begin{gathered} 5: 00 \mathrm{PM} \\ 749 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 209 \end{gathered}$ | $\begin{gathered} \text { 4:00 PM } \\ 202 \end{gathered}$ | $\begin{gathered} \text { 6:00 PM } \\ 184 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 296 \end{gathered}$ | $\begin{gathered} 2: 00 \text { PM } \\ 261 \end{gathered}$ | $\begin{gathered} \text { 4:00 PM } \\ 149 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 257 \end{gathered}$ |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 11/2/2012 1:57 PM

| LOCATION: SPECIFIC L CITY/STATE | West Drive OCATION: <br> E: Snoqualm | ay to 00 ft fr , WA | ualmie orth Be |  |  |  |  |  | DAT | QC JOB \#: 10822002 DIRECTION: NB/SB Oct 012012 - Oct 012012 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | $\begin{gathered} \text { Mon } \\ 01-O c t-12 \end{gathered}$ | Tue | Wed | Thu | Fri | Average Weekday Hourly Traffic | Sat | Sun | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM | 38 |  |  |  |  | 38 |  |  | 38 | $\square$ |
| 1:00 AM | 45 |  |  |  |  | 45 |  |  | 45 | $\square$ |
| 2:00 AM | 33 |  |  |  |  | 33 |  |  | 33 | $\square$ |
| 3:00 AM | 14 |  |  |  |  | 14 |  |  | 14 | $\square$ |
| 4:00 AM | 19 |  |  |  |  | 19 |  |  | 19 | - |
| 5:00 AM | 19 |  |  |  |  | 19 |  |  | 19 | $\square$ |
| 6:00 AM | 28 |  |  |  |  | 28 |  |  | 28 | _ |
| 7:00 AM | 67 |  |  |  |  | 67 |  |  | 67 |  |
| 8:00 AM | 69 |  |  |  |  | 69 |  |  | 69 | $\square$ |
| 9:00 AM | 105 |  |  |  |  | 105 |  |  | 105 |  |
| 10:00 AM | 108 |  |  |  |  | 108 |  |  | 108 |  |
| 11:00 AM | 31 |  |  |  |  | 31 |  |  | 31 |  |
| 12:00 PM |  |  |  |  |  |  |  |  |  |  |
| 1:00 PM |  |  |  |  |  |  |  | $=$ |  |  |
| 2:00 PM |  |  |  |  |  |  |  |  |  |  |
| 3:00 PM |  |  |  |  |  |  |  |  |  |  |
| 4:00 PM |  |  |  |  |  |  |  |  |  |  |
| 5:00 PM |  |  |  |  |  |  |  |  |  |  |
| 6:00 PM |  |  |  |  |  |  |  |  |  |  |
| 7:00 PM |  |  |  |  |  |  |  |  |  |  |
| 8:00 PM |  |  |  |  |  |  |  |  |  |  |
| 9:00 PM |  |  |  |  |  |  |  |  |  |  |
| 10:00 PM |  |  |  |  |  |  |  |  |  |  |
| 11:00 PM |  |  |  |  |  |  |  |  |  |  |
| Day Total | 576 |  |  |  |  | 576 |  |  | 576 |  |
| \% Weekday |  |  |  |  |  |  |  |  |  |  |
| Average | 25.5\% |  |  |  |  |  |  |  |  |  |
| \% Week |  |  |  |  |  |  |  |  |  |  |
| Average | 25.2\% |  |  |  |  | 100.0\% |  |  |  |  |
| AM Peak | 10:00 AM |  |  |  |  | 10:00 AM |  |  | 10:00 AM |  |
| Volume | 108 |  |  |  |  | 108 |  |  | 108 |  |
| PM Peak |  |  |  |  |  |  |  |  |  |  |
| Volume |  |  |  |  |  |  |  |  |  |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 11/2/2012 1:57 PM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net)

| LOCATION: SPECIFIC L CITY/STATE | West Drive OCATION: Snoqualm | eway to Sno 100 ft from nie, WA | qualmie Cas North Bend $\qquad$ | sino Way |  |  |  | DATE | $\begin{array}{\|c\|} \hline \text { QC JOB \#: } 10822002 \\ \text { DIRECTION: } \\ \text { NB/SB } \\ \text { Sep } 17 \text { 2012 - Sep } 212012 \\ \hline \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Mon 17-Sep-12 | Tue 18-Sep-12 | Wed 19-Sep-12 | Thu 20-Sep-12 | $\begin{gathered} \text { Fri } \\ 21-\text { Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic |  | DATE | Average Weekday Profile |
| 12:00 AM | 48 | 38 | 28 | 38 | 49 | 40 |  |  | ] |
| 1:00 AM | 47 | 31 | 28 | 35 | 33 | 35 |  |  | $\square$ |
| 2:00 AM | 25 | 31 | 23 | 28 | 41 | 30 |  |  |  |
| 3:00 AM | 11 | 18 | 10 | 7 | 18 | 13 |  |  | $\square$ |
| 4:00 AM | 20 | 8 | 11 | 7 | 22 | 14 |  |  | $\square$ |
| 5:00 AM | 18 | 19 | 21 | 21 | 28 | 21 |  |  | $\square$ |
| 6:00 AM | 36 | 28 | 38 | 41 | 42 | 37 |  |  | $\square$ |
| 7:00 AM | 68 | 59 | 57 | 67 | 80 | 66 |  |  |  |
| 8:00 AM | 92 | 60 | 69 | 85 | 114 | 84 |  |  |  |
| 9:00 AM | 107 | 63 | 88 | 93 | 124 | 95 |  |  | $\square$ |
| 10:00 AM | 109 | 71 | 100 | 115 | 108 | 101 |  |  |  |
| 11:00 AM | 107 | 105 | 101 | 95 | 158 | 113 |  |  |  |
| 12:00 PM | 96 | 45 | 115 | 98 | 147 | 100 |  |  |  |
| 1:00 PM | 131 | 110 | 166 | 121 | 179 | 141 |  |  |  |
| 2:00 PM | 168 | 122 | 119 | 137 | 172 | 144 |  |  | - |
| 3:00 PM | 158 | 152 | 145 | 0 | 210 | 133 |  | ¢ |  |
| 4:00 PM | 188 | 183 | 179 | 0 | 217 | 153 |  |  | $\square$ |
| 5:00 PM | 164 | 749 | 209 | 0 | 260 | 276 |  |  |  |
| 6:00 PM | 143 | 444 | 194 | 0 | 220 | 200 |  |  | - |
| 7:00 PM | 115 | 141 | 113 | 0 | 232 | 120 |  |  |  |
| 8:00 PM | 88 | 74 | 76 | 0 | 151 | 78 |  |  |  |
| 9:00 PM | 84 | 81 | 66 | 0 | 123 | 71 |  |  |  |
| 10:00 PM | 82 | 56 | 75 | 0 | 125 | 68 |  |  |  |
| 11:00 PM | 50 | 41 | 54 | 0 | 77 | 44 |  |  |  |
| Day Total | 2155 | 2729 | 2085 | 988 | 2930 | 2177 |  |  |  |
| \% Weekday Average | 99.0\% | 125.4\% | 95.8\% | 45.4\% | 134.6\% |  |  |  |  |
| \% Week Average |  |  |  |  |  |  |  |  |  |
| AM Peak Volume | $\begin{gathered} \hline 10: 00 \mathrm{AM} \\ 109 \end{gathered}$ | $\begin{gathered} \hline 11: 00 \mathrm{AM} \\ 105 \end{gathered}$ | $\begin{gathered} \hline 11: 00 \text { AM } \\ 101 \end{gathered}$ | $\begin{gathered} 10: 00 \text { AM } \\ 115 \end{gathered}$ | $\begin{gathered} \hline 11: 00 \mathrm{AM} \\ 158 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 113 \end{gathered}$ |  |  |  |
| PM Peak Volume | $\begin{gathered} \text { 4:00 PM } \\ 188 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 749 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 209 \end{gathered}$ | $\begin{gathered} \text { 2:00 PM } \\ 137 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 260 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 276 \end{gathered}$ |  |  |  |
| Comments: |  |  |  |  |  |  |  |  |  |

Report generated on 11/2/2012 1:57 PM


Report generated on 11/2/2012 1:57 PM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net)

| LOCATION: West Driveway to Snoqualmie Casino SPECIFIC LOCATION: 100 ft from North Bend Way CITY/STATE: Snoqualmie, WA |  |  |  |  |  |  |  |  | QC JOB \#: 10822002 DIRECTION: NB/SB <br> DATE: Sep 172012 - Sep 232012 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | $\begin{gathered} \text { Mon } \\ \text { 17-Sep-12 } \\ \hline \end{gathered}$ | Tue 18-Sep-12 | $\begin{gathered} \text { Wed } \\ \text { 19-Sep-12 } \end{gathered}$ | Thu 20-Sep-12 | $\begin{gathered} \text { Fri } \\ 21-\text { Sep-12 } \end{gathered}$ | Average Weekday Hourly Traffic | $\begin{gathered} \text { Sat } \\ \text { 22-Sep-12 } \end{gathered}$ | Sun 23-Sep-12 | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM | 48 | 38 | 28 | 38 | 49 | 40 | 63 | 73 | 48 | $\square$ |
| 1:00 AM | 47 | 31 | 28 | 35 | 33 | 35 | 50 | 71 | 42 | $\square$ |
| 2:00 AM | 25 | 31 | 23 | 28 | 41 | 30 | 70 | 81 | 43 | $\square$ |
| 3:00 AM | 11 | 18 | 10 | 7 | 18 | 13 | 40 | 30 | 19 | $\square$ |
| 4:00 AM | 20 | 8 | 11 | 7 | 22 | 14 | 20 | 23 | 16 | $\square$ |
| 5:00 AM | 18 | 19 | 21 | 21 | 28 | 21 | 21 | 28 | 22 | $\square$ |
| 6:00 AM | 36 | 28 | 38 | 41 | 42 | 37 | 40 | 29 | 36 | - |
| 7:00 AM | 68 | 59 | 57 | 67 | 80 | 66 | 69 | 38 | 63 | $\square$ |
| 8:00 AM | 92 | 60 | 69 | 85 | 114 | 84 | 117 | 63 | 86 |  |
| 9:00 AM | 107 | 63 | 88 | 93 | 124 | 95 | 136 | 90 | 100 |  |
| 10:00 AM | 109 | 71 | 100 | 115 | 108 | 101 | 119 | 116 | 105 | - |
| 11:00 AM | 107 | 105 | 101 | 95 | 158 | 113 | 121 | 124 | 116 | ] |
| 12:00 PM | 96 | 45 | 115 | 98 | 147 | 100 | 111 | 100 | 102 | $\square$ |
| 1:00 PM | 131 | 110 | 166 | 121 | 179 | 141 | 161 | 124 | 142 |  |
| 2:00 PM | 168 | 122 | 119 | 137 | 172 | 144 | 143 | 128 | 141 | , |
| 3:00 PM | 158 | 152 | 145 | 0 | 210 | 133 | 168 | 111 | 135 | - |
| 4:00 PM | 188 | 183 | 179 | 0 | 217 | 153 | 168 | 133 | 153 |  |
| 5:00 PM | 164 | 749 | 209 | 0 | 260 | 276 | 224 | 142 | 250 |  |
| 6:00 PM | 143 | 444 | 194 | 0 | 220 | 200 | 202 | 113 | 188 | 」 |
| 7:00 PM | 115 | 141 | 113 | 0 | 232 | 120 | 145 | 92 | 120 | 1 |
| 8:00 PM | 88 | 74 | 76 | 0 | 151 | 78 | 114 | 84 | 84 | - |
| 9:00 PM | 84 | 81 | 66 | 0 | 123 | 71 | 115 | 64 | 76 |  |
| 10:00 PM | 82 | 56 | 75 | 0 | 125 | 68 | 114 | 58 | 73 |  |
| 11:00 PM | 50 | 41 | 54 | 0 | 77 | 44 | 83 | 57 | 52 | - |
| Day Total | 2155 | 2729 | 2085 | 988 | 2930 | 2177 | 2614 | 1972 | 2212 |  |
| \% Weekday Average | 99.0\% | 125.4\% | 95.8\% | 45.4\% | 134.6\% |  |  |  |  |  |
| \% Week <br> Average | 97.4\% | 123.4\% | 94.3\% | 44.7\% | 132.5\% | 98.4\% | 118.2\% | 89.2\% |  |  |
| AM Peak Volume | $\begin{gathered} \hline 10: 00 \mathrm{AM} \\ 109 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 105 \end{gathered}$ | $\begin{gathered} \hline 11: 00 \mathrm{AM} \\ 101 \end{gathered}$ | $\begin{gathered} 10: 00 \mathrm{AM} \\ 115 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 158 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 113 \end{gathered}$ | $\begin{gathered} 9: 00 \mathrm{AM} \\ 136 \end{gathered}$ | $\begin{gathered} 11: 00 \text { AM } \\ 124 \end{gathered}$ | $\begin{gathered} 11: 00 \mathrm{AM} \\ 116 \end{gathered}$ |  |
| PM Peak Volume | $\begin{gathered} 4: 00 \mathrm{PM} \\ 188 \\ \hline \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 749 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 5: 00 \text { PM } \\ 209 \\ \hline \end{gathered}$ | $\begin{gathered} 2: 00 \mathrm{PM} \\ 137 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 260 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { 5:00 PM } \\ 276 \\ \hline \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 224 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 142 \\ \hline \end{gathered}$ | $\begin{gathered} \hline 5: 00 \mathrm{PM} \\ 250 \\ \hline \end{gathered}$ |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 11/2/2012 1:57 PM

Type of peak hour being reported: Intersection Peak
Method for determining peak hour: Total Entering Volume




QC JOB \#: 12598926 DATE: Tue, May 202014




Type of report: Tube Count - Volume Data

| LOCATION: I-5 Mainline Counts South of La Center Rd Friday SPECIFIC LOCATION: 0 ft from CITY/STATE: La Center, WA |  |  |  |  |  |  |  |  | QC JOB \#: 12598966DIRECTION: NBDATE: May 16 2014 - May 162014 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Mon | Tue | Wed | Thu | Fri <br> 16-May-14 | Average Weekday Hourly Traffic | Sat | Sun | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM |  |  |  |  | 404 | 404 |  |  | 404 | $\square$ |
| 1:00 AM |  |  |  |  | 328 | 328 |  |  | 328 | $\square$ |
| 2:00 AM |  |  |  |  | 293 | 293 |  |  | 293 |  |
| 3:00 AM |  |  |  |  | 330 | 330 |  |  | 330 | $\square$ |
| 4:00 AM |  |  |  |  | 508 | 508 |  |  | 508 | $\square$ |
| 5:00 AM |  |  |  |  | 1017 | 1017 |  |  | 1017 | $\square$ |
| 6:00 AM |  |  |  |  | 1579 | 1579 |  |  | 1579 | - |
| 7:00 AM |  |  |  |  | 2032 | 2032 |  |  | 2032 |  |
| 8:00 AM |  |  |  |  | 1842 | 1842 |  |  | 1842 | $\square$ |
| 9:00 AM |  |  |  |  | 2070 | 2070 |  |  | 2070 | $\square$ |
| 10:00 AM |  |  |  |  | 2279 | 2279 |  |  | 2279 | $\square$ |
| 11:00 AM |  |  |  |  | 2511 | 2511 |  |  | 2511 | $\square$ |
| 12:00 PM |  |  |  |  | 2744 | 2744 |  |  | 2744 |  |
| 1:00 PM |  |  |  |  | 2748 | 2748 |  | $\square$ | 2748 | - |
| 2:00 PM |  |  |  |  | 2857 | 2857 |  |  | 2857 | - |
| 3:00 PM |  |  |  |  | 3124 | 3124 |  |  | 3124 | - |
| 4:00 PM |  |  |  |  | 3080 | 3080 |  |  | 3080 | $\square$ |
| 5:00 PM |  |  |  |  | 3374 | 3374 |  |  | 3374 |  |
| 6:00 PM |  |  |  |  | 2794 | 2794 |  |  | 2794 | - |
| 7:00 PM |  |  |  |  | 2276 | 2276 |  |  | 2276 | - |
| 8:00 PM |  |  |  |  | 1726 | 1726 |  |  | 1726 | $\square$ |
| 9:00 PM |  |  |  |  | 1286 | 1286 |  |  | 1286 | ] |
| 10:00 PM |  |  |  |  | 1000 | 1000 |  |  | 1000 | ] |
| 11:00 PM |  |  |  |  | 758 | 758 |  |  | 758 | $\square$ |
| Day Total |  |  |  |  | 42960 | 42960 |  |  | 42960 |  |
| \% Weekday Average |  |  |  |  | 100.0\% |  |  |  |  |  |
| \% Week Average |  |  |  |  | 100.0\% | 100.0\% |  |  |  |  |
| AM Peak Volume |  |  |  |  | $\begin{gathered} \hline 11: 00 \text { AM } \\ 2511 \end{gathered}$ | $\begin{gathered} \hline 11: 00 \text { AM } \\ 2511 \\ \hline \end{gathered}$ |  |  | $\begin{gathered} \hline 11: 00 \text { AM } \\ 2511 \\ \hline \end{gathered}$ |  |
| PM Peak Volume |  |  |  |  | $\begin{gathered} 5: 00 \text { PM } \\ 3374 \end{gathered}$ | $\begin{gathered} \text { 5:00 PM } \\ 3374 \end{gathered}$ |  |  | $\begin{gathered} \text { 5:00 PM } \\ 3374 \end{gathered}$ |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 6/4/2014 8:32 AM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net)

| LOCATION: SPECIFIC L CITY/STATE | 5 Main LaTION La Cen | counts ft from WA | h of La | er Rd | iday |  |  |  | DAT | QC JOB \#: 12598966 DIRECTION: SB May 162014 - May 162014 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Mon | Tue | Wed | Thu | Fri <br> 16-May-14 | Average Weekday Hourly Traffic | Sat | Sun | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM |  |  |  |  | 423 | 423 |  |  | 423 | $\square$ |
| 1:00 AM |  |  |  |  | 314 | 314 |  |  | 314 | $\square$ |
| 2:00 AM |  |  |  |  | 252 | 252 |  |  | 252 | $\square$ |
| 3:00 AM |  |  |  |  | 347 | 347 |  |  | 347 | $\square$ |
| 4:00 AM |  |  |  |  | 625 | 625 |  |  | 625 | $\square$ |
| 5:00 AM |  |  |  |  | 1245 | 1245 |  |  | 1245 | $\square$ |
| 6:00 AM |  |  |  |  | 2020 | 2020 |  |  | 2020 | $\square$ |
| 7:00 AM |  |  |  |  | 2285 | 2285 |  |  | 2285 |  |
| 8:00 AM |  |  |  |  | 2251 | 2251 |  |  | 2251 |  |
| 9:00 AM |  |  |  |  | 2172 | 2172 |  |  | 2172 |  |
| 10:00 AM |  |  |  |  | 2267 | 2267 |  |  | 2267 | $\square$ |
| 11:00 AM |  |  |  |  | 2607 | 2607 |  |  | 2607 | $\square$ |
| 12:00 PM |  |  |  |  | 2803 | 2803 |  |  | 2803 | $\square$ |
| 1:00 PM |  |  |  |  | 2756 | 2756 |  |  | 2756 | - |
| 2:00 PM |  |  |  |  | 3061 | 3061 |  |  | 3061 |  |
| 3:00 PM |  |  |  |  | 3312 | 3312 |  |  | 3312 |  |
| 4:00 PM |  |  |  |  | 3255 | 3255 |  |  | 3255 |  |
| 5:00 PM |  |  |  |  | 2945 | 2945 |  |  | 2945 |  |
| 6:00 PM |  |  |  |  | 2417 | 2417 |  |  | 2417 | - |
| 7:00 PM |  |  |  |  | 2190 | 2190 |  |  | 2190 | ] |
| 8:00 PM |  |  |  |  | 1962 | 1962 |  |  | 1962 | $\square$ |
| 9:00 PM |  |  |  |  | 1680 | 1680 |  |  | 1680 | ] |
| 10:00 PM |  |  |  |  | 1183 | 1183 |  |  | 1183 | - |
| 11:00 PM |  |  |  |  | 734 | 734 |  |  | 734 | 1 |
| Day Total |  |  |  |  | 45106 | 45106 |  |  | 45106 |  |
| \% Weekday Average |  |  |  |  | 100.0\% |  |  |  |  |  |
| \% Week Average |  |  |  |  | 100.0\% | 100.0\% |  |  |  |  |
| AM Peak Volume |  |  |  |  | $\begin{gathered} \hline \text { 11:00 AM } \\ 2607 \\ \hline \end{gathered}$ | $\begin{gathered} \text { 11:00 AM } \\ 2607 \end{gathered}$ |  |  | $\begin{gathered} \text { 11:00 AM } \\ 2607 \\ \hline \end{gathered}$ |  |
| PM Peak Volume |  |  |  |  | $\begin{gathered} \text { 3:00 PM } \\ 3312 \end{gathered}$ | $\begin{gathered} \text { 3:00 PM } \\ 3312 \end{gathered}$ |  |  | $\begin{gathered} \text { 3:00 PM } \\ 3312 \end{gathered}$ |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |


| LOCATION: SPECIFIC L CITY/STATE | 5 Main LaTION La Cen | e Counts So 0 ft from <br> , WA | h of La | er Rd |  |  |  |  | DAT | QC JOB \#: 12598967 <br> DIRECTION: NB <br> May 202014 - May 202014 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Mon | Tue 20-May-14 | Wed | Thu | Fri | Average Weekday Hourly Traffic | Sat | Sun | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM |  | 347 |  |  |  | 347 |  |  | 347 | $\square$ |
| 1:00 AM |  | 258 |  |  |  | 258 |  |  | 258 | $\square$ |
| 2:00 AM |  | 285 |  |  |  | 285 |  |  | 285 | $\square$ |
| 3:00 AM |  | 324 |  |  |  | 324 |  |  | 324 | $\square$ |
| 4:00 AM |  | 459 |  |  |  | 459 |  |  | 459 | $\square$ |
| 5:00 AM |  | 997 |  |  |  | 997 |  |  | 997 | $\square$ |
| 6:00 AM |  | 1645 |  |  |  | 1645 |  |  | 1645 | $\square$ |
| 7:00 AM |  | 2020 |  |  |  | 2020 |  |  | 2020 |  |
| 8:00 AM |  | 1847 |  |  |  | 1847 |  |  | 1847 | - |
| 9:00 AM |  | 1783 |  |  |  | 1783 |  |  | 1783 |  |
| 10:00 AM |  | 1877 |  |  |  | 1877 |  |  | 1877 |  |
| 11:00 AM |  | 1958 |  |  |  | 1958 |  |  | 1958 | $\square$ |
| 12:00 PM |  | 2100 |  |  |  | 2100 |  |  | 2100 | $\square$ |
| 1:00 PM |  | 2045 |  |  |  | 2045 |  | $\sim$ | 2045 | + |
| 2:00 PM |  | 2247 |  |  |  | 2247 |  |  | 2247 | - |
| 3:00 PM |  | 2274 |  |  |  | 2274 |  |  | 2274 - |  |
| 4:00 PM |  | 2577 |  |  |  | 2577 |  |  | 2577 | $\square$ |
| 5:00 PM |  | 2835 |  |  |  | 2835 |  |  | 2835 |  |
| 6:00 PM |  | 2199 |  |  |  | 2199 |  |  | 2199 | ] |
| 7:00 PM |  | 1824 |  |  |  | 1824 |  |  | 1824 | ] |
| 8:00 PM |  | 1386 |  |  |  | 1386 |  |  | 1386 | $\square$ |
| 9:00 PM |  | 1027 |  |  |  | 1027 |  |  | 1027 | $\square$ |
| 10:00 PM |  | 745 |  |  |  | 745 |  |  | 745 |  |
| 11:00 PM |  | 572 |  |  |  | 572 |  |  | 572 |  |
| Day Total |  | 35631 |  |  |  | 35631 |  |  | 35631 |  |
| \% Weekday Average |  | 100.0\% |  |  |  |  |  |  |  |  |
| \% Week Average |  | 100.0\% |  |  |  | 100.0\% |  |  |  |  |
| AM Peak Volume |  | $\begin{gathered} \text { 7:00 AM } \\ 2020 \end{gathered}$ |  |  |  | $\begin{aligned} & \text { 7:00 AM } \\ & 2020 \end{aligned}$ |  |  | $\begin{aligned} & \text { 7:00 AM } \\ & 2020 \end{aligned}$ |  |
| PM Peak Volume |  | $\begin{gathered} \text { 5:00 PM } \\ 2835 \end{gathered}$ |  |  |  | $\begin{gathered} \hline \text { 5:00 PM } \\ 2835 \end{gathered}$ |  |  | $\begin{gathered} \text { 5:00 PM } \\ 2835 \end{gathered}$ |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 6/4/2014 8:32 AM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net)

| LOCATION: SPECIFIC L CITY/STATE | 5 Main LaTION La Cen | e Counts So 0 ft from <br> , WA | h of La | er Rd |  |  |  |  | DAT | QC JOB \#: 12598967 DIRECTION: SB <br> May 202014 - May 202014 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Mon | Tue 20-May-14 | Wed | Thu | Fri | Average Weekday Hourly Traffic | Sat | Sun | Average Week Hourly Traffic | Average Week Profile |
| 12:00 AM |  | 323 |  |  |  | 323 |  |  | 323 | $\square$ |
| 1:00 AM |  | 267 |  |  |  | 267 |  |  | 267 | $\square$ |
| 2:00 AM |  | 262 |  |  |  | 262 |  |  | 262 | $\square$ |
| 3:00 AM |  | 344 |  |  |  | 344 |  |  | 344 | $\square$ |
| 4:00 AM |  | 624 |  |  |  | 624 |  |  | 624 | $\square$ |
| 5:00 AM |  | 1390 |  |  |  | 1390 |  |  | 1390 | $\square$ |
| 6:00 AM |  | 2069 |  |  |  | 2069 |  |  | 2069 |  |
| 7:00 AM |  | 2370 |  |  |  | 2370 |  |  | 2370 |  |
| 8:00 AM |  | 2240 |  |  |  | 2240 |  |  | 2240 |  |
| 9:00 AM |  | 1924 |  |  |  | 1924 |  |  | 1924 | ] |
| 10:00 AM |  | 1951 |  |  |  | 1951 |  |  | 1951 | $\square$ |
| 11:00 AM |  | 1942 |  |  |  | 1942 |  |  | 1942 |  |
| 12:00 PM |  | 2014 |  |  |  | 2014 |  |  | 2014 | $\square$ |
| 1:00 PM |  | 2077 |  |  |  | 2077 |  | $\sim$ | 2077 | $\square$ |
| 2:00 PM |  | 2235 |  |  |  | 2235 |  |  | 2235 | $\square$ |
| 3:00 PM |  | 2503 |  |  |  | 2503 - |  |  | 2503 - |  |
| 4:00 PM |  | 2582 |  |  |  | 2582 |  |  | 2582 |  |
| 5:00 PM |  | 2521 |  |  |  | 2521 |  |  | 2521 |  |
| 6:00 PM |  | 1704 |  |  |  | 1704 |  |  | 1704 | ] |
| 7:00 PM |  | 1247 |  |  |  | 1247 |  |  | 1247 | $\square$ |
| 8:00 PM |  | 1144 |  |  |  | 1144 |  |  | 1144 | $\square$ |
| 9:00 PM |  | 813 |  |  |  | 813 |  |  | 813 | ] |
| 10:00 PM |  | 582 |  |  |  | 582 |  |  | 582 |  |
| 11:00 PM |  | 453 |  |  |  | 453 |  |  | 453 | $\square$ |
| Day Total |  | 35581 |  |  |  | 35581 |  |  | 35581 |  |
| \% Weekday Average |  | 100.0\% |  |  |  |  |  |  |  |  |
| \% Week Average |  | 100.0\% |  |  |  | 100.0\% |  |  |  |  |
| AM Peak Volume |  | $\begin{gathered} 7: 00 \mathrm{AM} \\ 2370 \end{gathered}$ |  |  |  | $\begin{gathered} \text { 7:00 AM } \\ 2370 \end{gathered}$ |  |  | $\begin{gathered} \text { 7:00 AM } \\ 2370 \end{gathered}$ |  |
| PM Peak |  | 4:00 PM |  |  |  | 4:00 PM |  |  | 4:00 PM |  |
| Volume |  | 2582 |  |  |  | 2582 |  |  | 2582 |  |
| Comments: |  |  |  |  |  |  |  |  |  |  |

Report generated on 6/4/2014 8:32 AM
SOURCE: Quality Counts, LLC (http://www.qualitycounts.net)

## Attachment E: Weigh Station Data from June 2014

I-5/Ridgefield Weigh Station Data
Source: WSDOT Commercial Vehicle Services

| dayStrBgn | dayStrEnd | Day of the Week (KAI) | Time Period <br> (KAI) | Day and Time (KAI) | lane | vehicle <br> Count |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20140613 15:00:00 | 20140613 18:00:00 | Friday | 3:00-6:00 PM | Friday 3:00-6:00 PM | Mainline 1 Bypass | 27 |
| 20140613 15:00:00 | 20140613 18:00:00 | Friday | 3:00-6:00 PM | Friday 3:00-6:00 PM | Mainline 2 Bypass | 330 |
| 20140613 15:00:00 | 20140613 18:00:00 | Friday | 3:00-6:00 PM | Friday 3:00-6:00 PM | Unknown Lane | 48 |
| 20140613 15:00:00 | 20140613 18:00:00 | Friday | 3:00-6:00 PM | Friday 3:00-6:00 PM | Weigh Station East Lane | 164 |
| 20140613 15:00:00 | 20140613 18:00:00 | Friday | 3:00-6:00 PM | Friday 3:00-6:00 PM | Weigh Station West Lane | 8 |
| 20140614 15:00:00 | 20140614 18:00:00 | Saturday | 3:00-6:00 PM | Saturday 3:00-6:00 PM | Mainline 1 Bypass | 10 |
| 20140614 15:00:00 | 20140614 18:00:00 | Saturday | 3:00-6:00 PM | Saturday 3:00-6:00 PM | Mainline 2 Bypass | 145 |
| 20140614 15:00:00 | 20140614 18:00:00 | Saturday | 3:00-6:00 PM | Saturday 3:00-6:00 PM | Unknown Lane | 34 |
| 20140614 15:00:00 | 20140614 18:00:00 | Saturday | 3:00-6:00 PM | Saturday 3:00-6:00 PM | Weigh Station East Lane | 139 |
| 20140614 15:00:00 | 20140614 18:00:00 | Saturday | 3:00-6:00 PM | Saturday 3:00-6:00 PM | Weigh Station West Lane | 18 |
| 20140615 15:00:00 | 20140615 18:00:00 | Sunday | 3:00-6:00 PM | Sunday 3:00-6:00 PM | Mainline 1 Bypass | 21 |
| 20140615 15:00:00 | 20140615 18:00:00 | Sunday | 3:00-6:00 PM | Sunday 3:00-6:00 PM | Mainline 2 Bypass | 183 |
| 20140615 15:00:00 | 20140615 18:00:00 | Sunday | 3:00-6:00 PM | Sunday 3:00-6:00 PM | Unknown Lane | 5 |
| 20140615 15:00:00 | 20140615 18:00:00 | Sunday | 3:00-6:00 PM | Sunday 3:00-6:00 PM | Weigh Station East Lane | 177 |
| 20140615 15:00:00 | 20140615 18:00:00 | Sunday | 3:00-6:00 PM | Sunday 3:00-6:00 PM | Weigh Station West Lane | 99 |
| 20140620 15:00:00 | 20140620 18:00:00 | Friday | 3:00-6:00 PM | Friday 3:00-6:00 PM | Mainline 1 Bypass | 39 |
| 20140620 15:00:00 | 20140620 18:00:00 | Friday | 3:00-6:00 PM | Friday 3:00-6:00 PM | Mainline 2 Bypass | 348 |
| 20140620 15:00:00 | 20140620 18:00:00 | Friday | 3:00-6:00 PM | Friday 3:00-6:00 PM | Unknown Lane | 55 |
| 20140620 15:00:00 | 20140620 18:00:00 | Friday | 3:00-6:00 PM | Friday 3:00-6:00 PM | Weigh Station East Lane | 3 |
| 20140620 15:00:00 | 20140620 18:00:00 | Friday | 3:00-6:00 PM | Friday 3:00-6:00 PM | Weigh Station West Lane | 84 |
| 20140621 15:00:00 | 20140621 18:00:00 | Saturday | 3:00-6:00 PM | Saturday 3:00-6:00 PM | Mainline 1 Bypass | 9 |
| 20140621 15:00:00 | 20140621 18:00:00 | Saturday | 3:00-6:00 PM | Saturday 3:00-6:00 PM | Mainline 2 Bypass | 174 |
| 20140621 15:00:00 | 20140621 18:00:00 | Saturday | 3:00-6:00 PM | Saturday 3:00-6:00 PM | Unknown Lane | 32 |
| 20140621 15:00:00 | 20140621 18:00:00 | Saturday | 3:00-6:00 PM | Saturday 3:00-6:00 PM | Weigh Station East Lane | 102 |
| 20140621 15:00:00 | 20140621 18:00:00 | Saturday | 3:00-6:00 PM | Saturday 3:00-6:00 PM | Weigh Station West Lane | 31 |
| 20140622 15:00:00 | 20140622 18:00:00 | Sunday | 3:00-6:00 PM | Sunday 3:00-6:00 PM | Mainline 1 Bypass | 37 |
| 20140622 15:00:00 | 20140622 18:00:00 | Sunday | 3:00-6:00 PM | Sunday 3:00-6:00 PM | Mainline 2 Bypass | 304 |
| 20140622 15:00:00 | 20140622 18:00:00 | Sunday | 3:00-6:00 PM | Sunday 3:00-6:00 PM | Unknown Lane | 59 |
| 20140622 15:00:00 | 20140622 18:00:00 | Sunday | 3:00-6:00 PM | Sunday 3:00-6:00 PM | Weigh Station East Lane | 143 |
| 20140622 15:00:00 | 20140622 18:00:00 | Sunday | 3:00-6:00 PM | Sunday 3:00-6:00 PM | Weigh Station West Lane | 41 |
| 20140627 15:00:00 | 20140627 18:00:00 | Friday | 3:00-6:00 PM | Friday 3:00-6:00 PM | Mainline 1 Bypass | 295 |
| 20140627 15:00:00 | 20140627 18:00:00 | Friday | 3:00-6:00 PM | Friday 3:00-6:00 PM | Mainline 2 Bypass | 38 |
| 20140627 15:00:00 | 20140627 18:00:00 | Friday | 3:00-6:00 PM | Friday 3:00-6:00 PM | Unknown Lane | 35 |
| 20140627 15:00:00 | 20140627 18:00:00 | Friday | 3:00-6:00 PM | Friday 3:00-6:00 PM | Weigh Station East Lane | 113 |
| 20140627 15:00:00 | 20140627 18:00:00 | Friday | 3:00-6:00 PM | Friday 3:00-6:00 PM | Weigh Station West Lane | 88 |
| 20140628 15:00:00 | 20140628 18:00:00 | Saturday | 3:00-6:00 PM | Saturday 3:00-6:00 PM | Mainline 1 Bypass | 147 |
| 20140628 15:00:00 | 20140628 18:00:00 | Saturday | 3:00-6:00 PM | Saturday 3:00-6:00 PM | Mainline 2 Bypass | 25 |
| 20140628 15:00:00 | 20140628 18:00:00 | Saturday | 3:00-6:00 PM | Saturday 3:00-6:00 PM | Unknown Lane | 37 |
| 20140628 15:00:00 | 20140628 18:00:00 | Saturday | 3:00-6:00 PM | Saturday 3:00-6:00 PM | Weigh Station East Lane | 129 |
| 20140628 15:00:00 | 20140628 18:00:00 | Sunday | 3:00-6:00 PM | Sunday 3:00-6:00 PM | Weigh Station West Lane | 53 |
| 20140629 15:00:00 | 20140629 18:00:00 | Sunday | 3:00-6:00 PM | Sunday 3:00-6:00 PM | Mainline 1 Bypass | 207 |
| 20140629 15:00:00 | 20140629 18:00:00 | Sunday | 3:00-6:00 PM | Sunday 3:00-6:00 PM | Mainline 2 Bypass | 41 |
| 20140629 15:00:00 | 20140629 18:00:00 | Sunday | 3:00-6:00 PM | Sunday 3:00-6:00 PM | Unknown Lane | 63 |
| 20140629 15:00:00 | 20140629 18:00:00 | Sunday | 3:00-6:00 PM | Sunday 3:00-6:00 PM | Weigh Station East Lane | 132 |
| 20140629 15:00:00 | 20140629 18:00:00 | Sunday | 3:00-6:00 PM | Sunday 3:00-6:00 PM | Weigh Station West Lane | 131 |

Ridgefield North Bound Traffic Flow





Piezo

Weigh-in-Motion (WIM)

Static Scale

| AVI Reader |  |
| ---: | :--- |
| In Cab Notification |  |
| (ICN) |  |
| IRD Lane |  |
| Designation | $\#-\#$ |



I-5/Ridgefield Weigh Station Data Assessment
Source: WSDOT Commercial Vehicle Services

| Average of vehicleCount <br> Row Labels | Column Labels <br> Mainline 1 | Mainline 2 |  | Unknown Lane | Weigh Station | Weigh Station | Grand Total |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Monday 7:00-9:00 AM | 117 | 297 | 38 | 85 | 97 | 127 |  |
| Monday 4:00-6:00 PM | 160 | 141 | 24 | 80 | 84 | 98 |  |
| Tuesday 7:00-9:00 AM | 126 | 311 | 44 | 76 | 94 | 130 |  |
| Tuesday 4:00-6:00 PM | 179 | 183 | 18 | 86 | 73 | 108 |  |
| Wednesday 7:00-9:00 AM | 115 | 336 | 30 | 94 | 81 | 131 |  |
| Wednesday 4:00-6:00 PM | 179 | 191 | 13 | 69 | 73 | 105 |  |
| Thursday 7:00-9:00 AM | 97 | 309 | 44 | 128 | 113 | 138 |  |
| Thursday 4:00-6:00 PM | 143 | 166 | 25 | 98 | 94 | 107 |  |
| Friday 7:00-9:00 AM | 75 | 288 | 40 | 100 | 96 | 120 |  |
| Friday 3:00-6:00 PM | 120 | 239 | 46 | 123 | 63 | 118 |  |
| Friday 4:00-6:00 PM | 24 | 228 | 36 | 84 | 53 | 80 |  |
| Saturday 3:00-6:00 PM | 55 | 115 | 34 | 123 | 25 | 74 |  |
| Sunday 3:00-6:00 PM | 88 | 176 | 56 | 151 | 81 | 109 |  |
| Grand Total | $\mathbf{1 1 6}$ | $\mathbf{2 2 9}$ | $\mathbf{3 5}$ | $\mathbf{1 0 0}$ | $\mathbf{7 9}$ | $\mathbf{1 1 2}$ |  |


| Period | Average \# of <br> Trucks to Weigh | \% trucks in <br> peak hour* | Peak Hour <br> Truck Volume |
| :--- | :---: | :---: | :---: |
| Friday 3:00-6:00 PM | 181 | $38 \%$ | 69 |
| Weekday 7:00-9:00 AM | 192 | $51 \%$ | 98 |
| Weekday 4:00-6:00PM | 164 | $53 \%$ | 87 |

*Based on I-5 mainline data from 2013, see sheet labled "R045 2013 Data - Vehicle Classification by Hour"

## R045 2013 Data - Vehicle Classification by Hour

Pivot tables based on data provided by WSDOT
Calculations to determine \% of trucks in peak hour (out of trucks in peak p

| Row Labels | Average of Hour 7 | Average of Hour 8 | Average of Hour 16 | Average of Hour 17 |
| :---: | :---: | :---: | :---: | :---: |
| Monday | 529 | 612 | 793 | 801 |
| Double-unit Truck | 230 | 244 | 304 | 268 |
| Motorcycle, Car, Van and Pickup | 1743 | 2054 | 2717 | 2800 |
| Single-unit Truck | 107 | 119 | 124 | 112 |
| Triple-unit Truck | 36 | 31 | 27 | 23 |
| Tuesday | 524 | 616 | 769 | 793 |
| Double-unit Truck | 255 | 258 | 297 | 266 |
| Motorcycle, Car, Van and Pickup | 1687 | 2046 | 2624 | 2769 |
| Single-unit Truck | 113 | 127 | 131 | 116 |
| Triple-unit Truck | 42 | 34 | 25 | 22 |
| Wednesday | 527 | 620 | 790 | 813 |
| Double-unit Truck | 272 | 271 | 310 | 278 |
| Motorcycle, Car, Van and Pickup | 1686 | 2046 | 2695 | 2834 |
| Single-unit Truck | 107 | 128 | 127 | 114 |
| Triple-unit Truck | 45 | 37 | 29 | 25 |
| Thursday | 518 | 622 | 825 | 840 |
| Double-unit Truck | 265 | 267 | 303 | 267 |
| Motorcycle, Car, Van and Pickup | 1655 | 2061 | 2836 | 2948 |
| Single-unit Truck | 107 | 121 | 135 | 121 |
| Triple-unit Truck | 44 | 38 | 25 | 24 |
| Grand Total | 524 | 618 | 794 | 812 |

Weekday Totals:

| Double-unit Truck | 1022 | 1040 | 1216 | 1079 |
| :--- | ---: | ---: | ---: | ---: |
| Motorcycle, Car, Van and Pickup | 6771 | 8207 | 10872 | 11350 |
| Single-unit Truck | 435 | 495 | 517 | 464 |
| Triple-unit Truck | 166 | 139 | 106 | 95 |


| Total Trucks | 1622 | 1675 | 1838 | 1638 |
| :---: | :---: | :---: | :---: | :---: |
|  | 51\% | 53\% |  |  |
|  | weekday AM peak hour | Weekday PM peak hour |  |  |


| Row Labels | Average of Hour 16 | Average of Hour 17 | Average of Hour 18 |
| :---: | :---: | :---: | :---: |
| Friday | 956 | 968 | 912 |
| Double-unit Truck | 256 | 229 | 189 |
| Motorcycle, Car, Van and Pickup | 3412 | 3505 | 3345 |
| Single-unit Truck | 136 | 122 | 101 |
| Triple-unit Truck | 22 | 19 | 15 |
| Grand Total | 956 | 968 | 912 |
| Total Trucks | 413 | 369 | 305 |
|  | 38\% |  |  |
|  | Friday peak hour |  |  |

# STATE OF WASHINGTON - DEPARTMENT OF TRANSPORTATION <br> T R I P S S Y S T E M 

PERMANENT TRAFFIC RECORDERS*
CONVERSION FACTORS: AVERAGE WEEKDAY TRAFFIC (AWDT) TO ANNUAL AVERAGE DAILY TRAFFIC (AADT)
URBAN STATIONS

| MONTH | AWDT FACTOR |  | AWDT FACTOR |  | AWDT FACTOR |  | AWDT FACTOR |  | AWDT FACTOR |  | AWDT FACTOR |  | AWDT FACTOR |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | R021 |  | R036 |  | R039 |  | R044 |  | R045 |  | R046 |  | R050 |  |
| JANUARY | 38033 | 1.06 | 108001 | 1.04 | 23239 | 1.46 | 74545 | 1.04 | 56055 | 1.21 | 197444 | 1.04 | 42807 | 1.01 |
| FEBRUARY | 42002 | . 96 | 118361 | . 95 | 23383 | 1.45 | 78393 | . 99 | 58999 | 1.15 | 207554 | . 99 | 45810 | . 94 |
| MARCH | 41959 | . 96 | 120273 | . 93 | 23639 | 1.43 | 79150 | . 98 | 62917 | 1.08 | 209104 | . 98 | 45557 | . 94 |
| APRIL | 42740 | . 94 | 124406 | . 90 | 25450 | 1.33 | 80803 | . 96 | 64488 | 1.05 | 211599 | . 97 | 45462 | . 95 |
| MAY | 42791 | . 94 | 126935 | . 88 | 28790 | 1.18 | 83185 | . 93 | 65426 | 1.04 | 213648 | . 96 | 47930 | . 90 |
| JUNE | 44429 | . 91 | 126943 | . 88 | 31384 | 1.08 | 85417 | . 91 | 69713 | . 97 | 214990 | . 95 | 48629 | . 89 |
| JULY | 42765 | . 94 | 127329 | . 88 | 35182 | . 96 | 85823 | . 90 | 73437 | . 92 | 212771 | . 96 | 48469 | . 89 |
| AUGUST | 44104 | . 91 | 130313 | . 86 | 36347 | . 93 | 86461 | . 90 | 75460 | . 90 | 213631 | . 96 | 49468 | . 87 |
| SEPTEMBER | 43506 | . 93 | 126887 | . 88 | 29869 | 1.14 | 84322 | . 92 | 69104 | . 98 | 210406 | . 97 | 48260 | . 89 |
| OCTOBER | 42683 | . 94 | 124859 | . 90 | 26741 | 1.27 | 81759 | . 95 | 64634 | 1.05 | 206650 | . 99 | 47156 | . 91 |
| NOVEMBER | 40155 | 1.00 | 116789 | . 96 | 26197 | 1.29 | 80918 | . 96 | 68070 | 1.00 | 201126 | 1.02 | 45899 | . 94 |
| DECEMBER | 40151 | 1.00 | 120480 | . 93 | 23347 | 1.45 | 79799 | . 97 | 62072 | 1.09 | 199120 | 1.03 | 43735 | . 98 |
| AADT | 40316 |  | 112060 |  | 33917 |  | 77396 |  | 67911 |  | 204459 |  | 43040 |  |
|  | R051 |  | R052 |  | R053 |  | R059 |  | R062 |  | R069 |  | R081 |  |
| JANUARY | 107795 | 1.04 | 75221 | 1.01 | 18063 | 1.20 | 4462 | 1.51 | 69158 | 1.00 | 19782 | 1.08 | 55375 | 1.04 |
| FEBRUARY | 115115 | . 98 | 80417 | . 94 | 20082 | 1.08 | 4937 | 1.36 | 75796 | . 91 | 21226 | 1.01 | 60538 | . 95 |
| MARCH | 117814 | . 96 | 80733 | . 94 | 20957 | 1.03 | 5389 | 1.25 | 76830 | . 90 | 21878 | . 98 | 61460 | . 94 |
| APRIL | 119448 | . 94 | 82362 | . 92 | 22392 | . 97 | 6201 | 1.08 | 76114 | . 91 | 22744 | . 94 | 62399 | . 92 |
| MAY | 120400 | . 94 | 83166 | . 91 | 24153 | . 90 | 6837 | . 98 | 78936 | . 88 | 23396 | . 91 | 65040 | . 88 |
| JUNE | 123441 | . 91 | 83293 | . 91 | 24986 | . 87 | 7418 | . 91 | 78412 | . 88 | 23678 | . 90 | 63692 | . 90 |
| JULY | 122843 | . 92 | 83958 | . 90 | 25809 | . 84 | 8896 | . 76 | 75021 | . 92 | 25277 | . 85 | 60347 | . 95 |
| AUGUST | 125159 | . 90 | 84168 | . 90 | 25408 | . 85 | 8493 | . 79 | 77546 | . 89 | 25316 | . 84 | 62055 | . 93 |
| SEPTEMBER | 121693 | . 93 | 82181 | . 92 | 24821 | . 87 | 7314 | . 92 | 77420 | . 89 | 24206 | . 88 | 63564 | . 90 |
| OCTOBER | 119692 | . 94 | 82237 | . 92 | 23805 | . 91 | 6614 | 1.02 | 76812 | . 90 | 22628 | . 94 | 63772 | . 90 |
| NOVEMBER | 116367 | . 97 | 78868 | . 96 | 21420 | 1.01 | 5496 | 1.22 | 72861 | . 95 | 21359 | 1.00 | 61459 | . 94 |
| DECEMBER | 111575 | 1.01 | 76448 | . 99 | 20543 | 1.05 | 5011 | 1.34 | 71270 | . 97 | 20327 | 1.05 | 57223 | 1.00 |
| AADT | 112581 |  | 75598 |  | 21659 |  | 6726 |  | 69115 |  | 21373 |  | 57494 |  |
|  | R082 |  | R087 |  | R089 |  | R091 |  | R097 |  | R098 |  | R101 |  |
| JANUARY | 165073 | 1.06 | 55585 | 1.06 | 15021 | 1.08 | 112547 | 1.07 | 59847 | 1.15 | 96089 | . 99 | 61352 | . 98 |
| FEBRUARY | 174879 | 1.00 | 61566 | . 96 | 15841 | 1.03 | 119677 | 1.00 | 63228 | 1.09 | 99024 | . 96 | 65725 | . 91 |
| MARCH | 177823 | . 99 | 62222 | . 95 | 16102 | 1.01 | 121801 | . 98 | 65900 | 1.05 | 98654 | . 96 | 66309 | . 90 |
| APRIL | 182417 | . 96 | 63648 | . 93 | 16750 | . 97 | 122949 | . 98 | 67149 | 1.03 | 101309 | . 94 | 66728 | . 90 |
| MAY | 182008 | . 96 | 64355 | . 92 | 17271 | . 94 | 124707 | . 96 | 68301 | 1.01 | 102634 | . 93 | 68650 | . 87 |
| JUNE | 184680 | . 95 | 64264 | . 92 | 17766 | . 92 | 129858 | . 92 | 72437 | . 95 | 103019 | . 92 | 70596 | . 85 |
| JULY | 187429 | . 94 | 63766 | . 92 | 18687 | . 87 | 131249 | . 91 | 75022 | . 92 | 103347 | . 92 | 68058 | . 88 |
| AUGUST | 192942 | . 91 | 64254 | . 92 | 18479 | . 88 | 132850 | . 90 | 76633 | . 90 | 104119 | . 91 | 70643 | . 85 |
| SEPTEMBER | 185953 | . 94 | 62274 | . 95 | 17691 | . 92 | 125768 | . 95 | 69119 | 1.00 | 102414 | . 93 | 67168 | . 89 |
| OCTOBER | 181470 | . 97 | 63722 | . 93 | 17118 | . 95 | 120776 | . 99 | 65664 | 1.05 | 103310 | . 92 | 66098 | . 91 |
| NOVEMBER | 177641 | . 99 | 60521 | . 97 | 16331 | 1.00 | 120652 | . 99 | 68033 | 1.01 | 98433 | . 97 | 62567 | . 96 |
| DECEMBER | 174756 | 1.00 | 56323 | 1.05 | 15493 | 1.05 | 114148 | 1.05 | 64629 | 1.07 | 95597 | 1.00 | 59322 | 1.01 |
| AADT | 1755 |  | 589 |  | 162 |  | 1199 |  | 690 |  | 951 |  | 599 |  |
| * OREGON-O | ED RECOR | DERS | ERRY TER | RMINAL | UUDED |  |  |  |  |  |  |  |  |  |

* OREGON-OWNED RECORDERS AND FERRY TERMINALS EXCLUDED


## Attachment G: Truck Percentages for I-5

## Washington State Department of Transportation

2012 4-BIN CLASSIFICATION by Hour Report for Woodland
Permanent Traffic Recorder R045 on I-5 @ mile post 20.14

Statewide Travel \& Collision Data Office
Travel Data \& Analysis Branch
Automated Data Collection \& Processing Section
360-570-2392 or 360-570-2394

Pivot tables below created by KAI from data provided by WSDOT, contact above

Weekday AM Peak Hour

| Average of Truck Percentage | Column Labels |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | 700 |  | 700 Total | Grand Total |
| Row Labels | NORTH | SOUTH |  |  |
| Monday | 0.177326416 | 0.145665153 | 0.163133436 | 0.163133436 |
| Tuesday | 0.180604721 | 0.159704461 | 0.171235639 | 0.171235639 |
| Wednesday | 0.186982354 | 0.17125927 | 0.179934075 | 0.179934075 |
| Thursday | 0.186770075 | 0.16687609 | 0.177166082 | 0.177166082 |
| Grand Total | 18\% | 16\% | 0.172867308 | 0.172867308 |

Weekday PM Peak Hour

| Average of Truck Percentage | Column Labels |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | 1700 |  | 1700 Total | Grand Total |
| Row Labels | NORTH | SOUTH |  |  |
| Monday | 0.104518881 | 0.136570675 | 0.118886927 | 0.118886927 |
| Tuesday | 0.106122381 | 0.136227937 | 0.119617975 | 0.119617975 |
| Wednesday | 0.112648119 | 0.136050345 | 0.123138772 | 0.123138772 |
| Thursday | 0.108674719 | 0.128221009 | 0.118110859 | 0.118110859 |
| Grand Total | 11\% | 13\% | 0.119938633 | 0.119938633 |

Friday Peak Hour

| Average of Truck Percentage | Column Labels |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1700 |  |  | 1700 Total | Grand Total |
| Row Labels | NORTH |  |  |  |  |
| Friday |  | 0.083186501 | 0.105737658 | 0.094073267 | 0.094073267 |
| Grand Total |  | 8\% | 11\% | 0.094073267 | 0.094073267 |

## Appendix K Existing Conditions Worksheets <br> - Freeway Mainline



| BASIC FREEWAY SEGMENTS WORKSHEET |  |  |  |
| :---: | :---: | :---: | :---: |
| General Information |  | \|Site Information |  |
| Analyst <br> Agency or Company <br> Date Performed <br> Analysis Time Period | ```KML KAI 6/24/2014 Weekday AM Peak Period``` | Highway/Direction of Travel l-5 SB  <br> From/To SR 501 to La Center <br> Jurisdiction WSDOT <br> Analysis Year Existing |  |
| Project Description 12393 |  |  |  |
| $\checkmark$ Oper.(LOS) $\square$ |  | Des.(N) $\square$ | $\square$ Planning Data |
| Flow Inputs |  |  |  |
| Volume, V <br> AADT <br> Peak-Hr Prop. of AADT, K <br> Peak-Hr Direction Prop, D <br> DDHV $=$ AADT $\times K \times D$ | 2733 veh/h veh/day <br> veh/h | Peak-Hour Factor, PHF 1.00 <br> \%Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ 16 <br> \%RVs, $\mathrm{P}_{\mathrm{R}}$ 0 <br> General Terrain: Level <br> GradeLength   <br> Up/Down \%  mi  <br>   |  |
| Calculate Flow Adjustments |  |  |  |
| $\begin{array}{\|l\|} \hline \mathrm{f}_{\mathrm{p}} \\ \mathrm{E}_{\mathrm{T}} \end{array}$ | 1.00 | $\begin{aligned} & E_{R} \quad 1.2 \\ & f_{H V}=1 /\left[1+P_{T}\left(E_{T}-1\right)+P_{R}\left(E_{R}-1\right)\right] 0.926 \end{aligned}$ |  |
| Speed Inputs |  | Calc Speed Adj and FFS |  |
| Lane Width <br> Rt-Side Lat. Clearance <br> Number of Lanes, N <br> Total Ramp Density, TRD <br> FFS (measured) <br> Base free-flow Speed, BFFS | 12.0 ft <br> 6.0 ft <br> 3  <br> 1.33 $\mathrm{ramps} / \mathrm{mi}$ <br> mph <br> 75.4 mph | $\mathrm{f}_{\mathrm{Lw}}$ 0.0 <br> $\mathrm{f}_{\mathrm{LC}}$ 0.0 <br> TRD Adjustment 4.1 <br> FFS 71.3 | mph <br> mph <br> mph <br> mph |
| LOS and Performance Measures |  | Design (N) |  |
| Operational (LOS) |  | Design $(\mathrm{N})$  <br> Design LOS  <br> $\mathrm{v}_{\mathrm{p}}=\left(\mathrm{V}\right.$ or DDHV) $/\left(\mathrm{PHF} \times N \times \mathrm{f}_{\mathrm{HV}}\right.$ $\mathrm{pc} / \mathrm{h} / \mathrm{ln}$ <br> $\left.\times f_{\mathrm{p}}\right)$ mph <br> $S$ $\mathrm{pc} / \mathrm{mi} / \mathrm{ln}$ <br> Required Number of Lanes, N |  |
| Glossary |  | Factor Location |  |
| N - Number of lanes <br> V - Hourly volume <br> $\mathrm{v}_{\mathrm{p}}$ - Flow rate <br> LOS - Level of service <br> speed <br> DDHV - Directional design | S - Speed <br> D - Density <br> FFS - Free-flow speed <br> BFFS - Base free-flow <br> hour volume | $\mathrm{E}_{\mathrm{R}}$ - Exhibits 11-10, 11-12 $\mathrm{f}_{\mathrm{LW}}-$ Exhibit 11-8 <br> $\mathrm{E}_{\mathrm{T}}$ - Exhibits 11-10, 11-11, 11-13 $\mathrm{f}_{\mathrm{LC}}-$ Exhibit 11-9 <br> $\mathrm{f}_{\mathrm{p}}$ - Page 11-18 TRD - Page 11-11 <br> LOS, S, FFS, $\mathrm{v}_{\mathrm{p}}$ - Exhibits 11-2,  <br> $11-3$  |  |












## Appendix L Existing Conditions Worksheets - Merge/Diverge Locations









| RAMPS AND RAMP JUNCTIONS WORKSHEET |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| General Information |  |  |  | Site Information |  |  |  |  |  |  |  |
| Analyst <br> Agency or Company Date Performed Analysis Time Period | KML <br> KAI <br> 6/24/2014 <br> Weekday PM Peak Period |  |  | Freeway/Dir of Travel Junction Jurisdiction Analysis Year |  | I-5 NB Off Ramp <br> La Center WSDOT Existing |  |  |  |  |  |
| Project Description 12393 |  |  |  |  |  |  |  |  |  |  |  |
| Inputs |  |  |  |  |  |  |  |  |  |  |  |
| Upstream Adj R Yes No $\begin{aligned} & \mathrm{L}_{\mathrm{up}}= \\ & \mathrm{V}_{\mathrm{u}}= \end{aligned}$ |  | Freeway <br> Ramp N <br> Accelera <br> Decelera <br> Freeway <br> Ramp Vo <br> Freeway <br> Ramp F | of Lanes, N Lanes, N <br> Length, $L_{A}$ <br> Length $L_{D}$ <br> $V_{F}$ <br> $w$ Speed, $\mathrm{S}_{\mathrm{FF}}$ <br> Speed, $\mathrm{S}_{\text {FR }}$ | $\begin{aligned} & \hline 3 \\ & 1 \\ & 250 \\ & 3074 \\ & 579 \\ & 70.0 \\ & 35.0 \\ & \hline \end{aligned}$ |  |  |  |  |  | Downstrea Ramp Yes No $\mathrm{L}_{\text {down }}=$ $V_{D}=$ | m Adj On Off <br> 2500 ft <br> 133 veh/h |
| Conversion to pc/h Under Base Conditions |  |  |  |  |  |  |  |  |  |  |  |
| (pc/h) | $\begin{gathered} \mathrm{V} \\ (\mathrm{Veh} / \mathrm{hr}) \end{gathered}$ | PHF | Terrain | \%Truck | \%Rv |  | $\mathrm{f}_{\mathrm{HV}}$ |  | $\mathrm{f}_{\mathrm{p}}$ | $\mathrm{v}=\mathrm{V} / \mathrm{PHF} \times \mathrm{f}_{\mathrm{HV}} \times \mathrm{f}_{\mathrm{p}}$ |  |
| Freeway | 3074 | 1.00 | Level | 11 | 0 |  | 0.948 |  | 1.00 | 3243 |  |
| Ramp | 579 | 1.00 | Level | 4 | 0 |  | 0.980 |  | 1.00 | 591 |  |
| UpStream |  |  |  |  |  |  |  |  |  |  |  |
| DownStream | 133 | 1.00 | Level | 8 | 0 |  | 0.962 |  | 1.00 |  |  |
| Merge Areas |  |  |  |  | Diverge Areas |  |  |  |  |  |  |
| Estimation of $\boldsymbol{v}_{12}$ |  |  |  |  | Estimation of $\mathbf{v}_{12}$ |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
| Capacity Checks |  |  |  |  | Capacity Checks |  |  |  |  |  |  |
| $\mathrm{V}_{\mathrm{FO}}$ | Actual | Capacity |  | LOS F? |  |  | Actual |  | Capacity |  | LOS F? |
|  |  | Exhibit 13 |  |  | $\mathrm{V}_{\text {F }}$ |  |  | 3243 | Exhibit 13-8 | 枯 7200 | No |
|  |  |  |  |  | $V_{\text {FO }}=V^{\prime}$ | $V_{F}-V_{R}$ |  | 2652 | Exhibit 13-8 | 7200 | No |
|  |  |  |  |  | $\mathrm{V}_{\mathrm{R}}$ | R |  | 591 | Exhibit 13-10 | 0 2000 | No |
| Flow Entering Merge Influence Area |  |  |  |  | Flow Entering Diverge Influence Area |  |  |  |  |  |  |
|  | Actual | Max Desirable |  | Violation? |  |  | Actua |  | Max Desirabl |  | Violation? |
| $\mathrm{V}_{\mathrm{R} 12}$ |  | Exhibit |  |  | $\mathrm{V}_{12}$ |  | 2319 |  |  | 4400:All | No |
| Level of Service Determination (if not F) |  |  |  |  | Level of Service Determination (if not F) |  |  |  |  |  |  |
| $\begin{aligned} & \mathrm{D}_{\mathrm{R}}=5.475+0.00734 \mathrm{v}_{\mathrm{R}}+0.0078 \mathrm{~V}_{12}-0.00627 \mathrm{~L}_{\mathrm{A}} \\ & \mathrm{D}_{\mathrm{R}}=\quad(\mathrm{pc} / \mathrm{mi} / \mathrm{ln}) \\ & \mathrm{LO}= \\ & \quad \text { (Exhibit 13-2) } \end{aligned}$ |  |  |  |  | $\begin{array}{ll}  & D_{R}=4.252+0.0086 \mathrm{~V}_{12}-0.009 \mathrm{~L}_{\mathrm{D}} \\ \mathrm{D}_{\mathrm{R}}= & 21.9 \text { (pc/mi/ln) } \\ \text { LOS }= & C \text { (Exhibit 13-2) } \end{array}$ |  |  |  |  |  |  |
| Speed Determination |  |  |  |  | Speed Determination |  |  |  |  |  |  |
| $\begin{array}{ll} \hline \mathrm{M}_{\mathrm{S}}= & \text { (Exibit 13-11) } \\ \mathrm{S}_{\mathrm{R}}= & \text { mph (Exhibit 13-11) } \\ \mathrm{S}_{0}= & \text { mph (Exhibit 13-11) } \\ \mathrm{S}= & \text { mph (Exhibit 13-13) } \end{array}$ |  |  |  |  | $\begin{array}{ll} \mathrm{D}_{\mathrm{S}}= & 0.481(\text { Exhibit } 13-12) \\ \mathrm{S}_{\mathrm{R}}= & 56.5 \mathrm{mph}(\text { Exhibit } 13-12) \\ \mathrm{S}_{0}= & 76.8 \mathrm{mph} \text { (Exhibit 13-12) } \\ \mathrm{S}= & 61.1 \mathrm{mph} \text { (Exhibit 13-13) } \end{array}$ |  |  |  |  |  |  |











| RAMPS AND RAMP JUNCTIONS WORKSHEET |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| General Information |  |  |  | Site Information |  |  |  |  |  |  |
| Analyst KML |  |  |  | Freeway/Dir of TravelJunction |  | NB Off Weigh Station |  |  |  |  |
| Agency or Company KAl |  |  |  |  |  | Canter |  |  |  |  |
|  |  |  |  | Jurisdiction |  | DO |  |  |  |  |
| Analysis Time Period Friday PM Peak Period | Friday PM Peak Period |  |  | Analysis Year |  | Existing |  |  |  |  |
| Project Description 12393 |  |  |  |  |  |  |  |  |  |  |
| Inputs |  |  |  |  |  |  |  |  |  |  |
| UnstremAdi R |  | Freeway Number of Lanes, N |  | 3 |  |  |  |  | Downstream Adj |  |
|  |  | Ramp Number of Lanes, N |  |  |  |  |  |  |
| $\square \mathrm{Yes} \square$ On |  |  |  |  |  |  |  |  |  |  | $\checkmark$ Yes $\triangle$ On |  |
| VNo |  | Deceleration Lane Length $L_{D}$ |  |  |  |  |  |  |  |  |
|  |  |  |  | 3711 |  |  |  |  | $\square$ No $\square$ Off |  |
|  |  | Ramp Volume, $\mathrm{V}_{\mathrm{R}}$ |  | 69 |  |  |  |  | $L_{\text {down }}=2525 \mathrm{ft}$ |  |
|  | W/h | Freeway Free-Flow Speed, $\mathrm{S}_{\text {FF }}$ |  | 70.0 |  |  |  |  | $\mathrm{V}_{\mathrm{D}}=$ | $69 \mathrm{veh} / \mathrm{h}$ |
|  |  | Ramp Free | Speed, $\mathrm{S}_{\text {FR }}$ | 35.0 |  |  |  |  |  |  |
| Conversion to pc/h Under Base Conditions |  |  |  |  |  |  |  |  |  |  |
| (poch) | $\begin{aligned} & \text { V } \\ & (\text { Veh/hr) } \end{aligned}$ | PHF | Terrain | \%Truck | \%Rv | $\mathrm{f}_{\mathrm{HV}}$ |  | $\mathrm{f}_{\mathrm{p}}$ | $\mathrm{v}=\mathrm{V} / \mathrm{PHF} \times \mathrm{f}_{\mathrm{HV}} \times \mathrm{f}_{\mathrm{p}}$ |  |
| Freeway | 3711 | 1.00 | Level | 8 | 0 |  |  | 1.00 | 38 |  |
| Ramp | 69 | 1.00 | Level | 100 | 0 |  | 67 | 1.00 | 10 |  |
| UpStream |  |  |  |  |  |  |  |  |  |  |
| DownStream | 69 | 1.00 | Level | 100 | 0 |  |  | 1.00 | 10 |  |
| Merge Areas |  |  |  |  | Diverge Areas |  |  |  |  |  |
| Estimation of $\mathrm{v}_{12}$ |  |  |  |  | Estimation of $\mathbf{v}_{12}$ |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Capacity Checks |  |  |  |  | Capacity Checks |  |  |  |  |  |
| $\mathrm{V}_{\mathrm{FO}}$ | Actual | Capacity |  | LOS F? |  | Actual |  | Capacity |  | LOS F? |
|  |  | Exhibit 13-8 |  |  | $\mathrm{V}_{\mathrm{F}}$ |  | 3859 | Exhibit 13-8 | 7200 | No |
|  |  |  |  |  | $\mathrm{V}_{\mathrm{FO}}=\mathrm{V}_{\mathrm{F}}$ |  | 3756 | Exhibit 13-8 | 7200 | No |
|  |  |  |  |  | $\mathrm{V}_{\mathrm{R}}$ |  | 103 | Exhibit 13-10 | 10200 | No |
| Flow Entering Merge Influence Area |  |  |  |  | Flow Entering Diverge Influence Area |  |  |  |  |  |
|  | Actual | Max Desirable |  | Violation? |  |  | ctual | Max Desirable |  | Violation? |
| $\mathrm{V}_{\text {R12 }}$ |  | Exhibit 13-8 |  |  | $\mathrm{V}_{12}$ |  | 577 | Exhibit 13-8 | 4400:All | No |
| Level of Service Determination (if not F) |  |  |  |  | Level of Service Determination (if not F) |  |  |  |  |  |
| $\begin{array}{ll} \mathrm{D}_{\mathrm{R}}=5.475+0.00734 \mathrm{v}_{\mathrm{R}}+0.0078 \mathrm{~V}_{12}-0.00627 \mathrm{~L}_{\mathrm{A}} \\ \mathrm{D}_{\mathrm{R}}= & (\text { (pc/mi/ln }) \\ \text { LOS }= & \text { (Exhibit } 13-2) \end{array}$ |  |  |  |  | $\begin{array}{ll} \hline & D_{R}=4.252+0.0086 \mathrm{~V}_{12}-0.009 \mathrm{~L}_{\mathrm{D}} \\ \mathrm{D}_{\mathrm{R}}= & 17.6(\text { pc/mil/n) }) \\ \text { LOS }= & B \text { (Exhibit 13-2) } \end{array}$ |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Speed Determination |  |  |  |  | Speed Determination |  |  |  |  |  |
| $M_{\mathrm{S}}=$ (Exibit 13-11) <br> $\mathrm{S}_{\mathrm{R}}=$ mph (Exhibit 13-11) <br> $\mathrm{S}_{0}=$ mph (Exhibit 13-11) <br> $\mathrm{S}=$ mph (Exhibit 13-13) |  |  |  |  | $\begin{array}{ll} \hline \mathrm{D}_{\mathrm{S}}= & 0.437(\text { Exhibit 13-12) } \\ \mathrm{S}_{\mathrm{R}}= & 57.8 \mathrm{mph}(\text { Exhibit 13-12) } \\ \mathrm{S}_{0}= & 75.7 \mathrm{mph} \text { (Exhibit 13-12) } \\ \mathrm{S}^{2}= & 62.7 \mathrm{mph}(\text { Exhibit 13-13) } \end{array}$ |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Appendix M Existing Conditions Worksheets <br> - Study Intersections



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 4.7 |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Movement | 44 | 16 | EBT | EBR | WBT | NBL |


| Major/Minor | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 60 | 0 | 164 | 52 |
| Stage 1 | - | - | - | - | 52 | - |
| Stage 2 | - | - | - | - | 112 | - |
| Critical Hdwy | - | - | 4.21 | - | 6.4 | 6.43 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 | - |
| Follow-up Hdwy | - | - | 2.299 | - | 3.5 | 3.507 |
| Pot Cap-1 Maneuver | - | - | 1488 | - | 831 | 959 |
| Stage 1 | - | - | - | - | 976 | - |
| Stage 2 | - | - | - | - | 918 |  |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1488 | - | 809 | 959 |
| Mov Cap-2 Maneuver | - | - | - | - | 809 | - |
| Stage 1 | - | - | - | - | 976 | - |
| Stage 2 | - | - | - | - | 893 | - |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0 | 4.2 | 9.1 |
| HCM LOS |  |  | A |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 949 | - | - | 1488 | - |
| HCM Lane V/C Ratio | 0.076 | - | - | 0.027 | - |
| HCM Control Delay (s) | 9.1 | - | - | 7.5 | 0 |
| HCM Lane LOS | A | - | - | A | A |
| HCM 95th \%tile Q(veh) | 0.2 | - | - | 0.1 | - |


|  | $\Rightarrow$ | $\rightarrow$ | $\geqslant$ | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | F |  |  | $\uparrow$ |  |  |  |  |  | $\uparrow$ | F |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 25 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 1 |
| Taper Length (tt) | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  | 0.964 |  |  |  |  |  |  |  |  |  | 0.850 |
| Flt Protected |  |  |  |  | 0.958 |  |  |  |  |  | 0.954 |  |
| Satd. Flow (prot) | 0 | 1567 | 0 | 0 | 1746 | 0 | 0 | 0 | 0 | 0 | 1584 | 1442 |
| Flt Permitted |  |  |  |  | 0.958 |  |  |  |  |  | 0.954 |  |
| Satd. Flow (perm) | 0 | 1567 | 0 | 0 | 1746 | 0 | 0 | 0 | 0 | 0 | 1584 | 1442 |
| Link Speed (mph) |  | 40 |  |  | 40 |  |  | 50 |  |  | 50 |  |
| Link Distance (ft) |  | 144 |  |  | 502 |  |  | 626 |  |  | 699 |  |
| Travel Time (s) |  | 2.5 |  |  | 8.6 |  |  | 8.5 |  |  | 9.5 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 13.7 |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 0 | 82 | 30 | 448 | 64 | 0 | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 0 | 22 | 3 | 4 | 6 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 0 | 82 | 30 | 448 | 64 | 0 | 0 | 0 | 0 |
| Major/Minor | Major1 |  |  | Major2 |  |  |  |  |  |
| Conflicting Flow All | 64 | 0 | 0 | 112 | 0 | 0 |  |  |  |
| Stage 1 | - | - | - | - | - | - |  |  |  |
| Stage 2 | - | - | - | - | - | - |  |  |  |
| Critical Hdwy | 4.1 | - | - | 4.14 | - | - |  |  |  |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |  |  |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |  |  |  |
| Follow-up Hdwy | 2.2 | - | - | 2.236 | - | - |  |  |  |
| Pot Cap-1 Maneuver | 1551 | - | - | 1465 | - | - |  |  |  |
| Stage 1 | - | - | - | - | - | - |  |  |  |
| Stage 2 | - | - | - | - | - | - |  |  |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1551 | - | - | 1465 | - | - |  |  |  |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |  |  |  |
| Stage 1 | - | - | - | - | - | - |  |  |  |
| Stage 2 | - | - | - | - | - | - |  |  |  |


| Approach | EB | WB |
| :--- | :---: | :---: |
| HCM Control Delay, s | 0 | 7.5 |
| HCM LOS |  |  |


| Minor Lane/Major Mvmt | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 | SBLn2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1551 | - | - | 1465 | - | - | 163 | 973 |
| HCM Lane V/C Ratio | - | - | - | 0.306 | - | - | 0.638 | 0.008 |
| HCM Control Delay (s) | 0 | - | - | 8.5 | 0 | - | 59.5 | 8.7 |
| HCM Lane LOS | A | - | - | A | A | - | F | A |
| HCM 95th \%tile Q(veh) | 0 | - | - | 1.3 | - | - | 3.6 | 0 |


| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | SBL | SBT | SBR |
| Vol, veh/h | 0 | 4 | 8 |
| Conflicting Peds, \#/hr | Stop | Stop | Stop |
| Sign Control | - | - | None |
| RT Channelized | - | - | 25 |
| Storage Length | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | 100 | 100 | 100 |
| Peak Hour Factor | 13 | 50 | 12 |
| Heavy Vehicles, \% | 100 | 4 | 8 |
| Mvmt Flow |  |  |  |


| Major/Minor | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Conflicting Flow All | 1057 | 1072 | 64 |
| Stage 1 | 960 | 960 | - |
| $\quad$ Stage 2 | 97 | 112 | - |
| Critical Hdwy | 6.53 | 7 | 6.32 |
| Critical Hdwy Stg 1 | 5.53 | 6 | - |
| Critical Hdwy Stg 2 | 5.53 | 6 | - |
| Follow-up Hdwy | 3.617 | 4.45 | 3.408 |
| Pot Cap-1 Maneuver | 238 | 182 | 973 |
| $\quad$ Stage 1 | 355 | 279 | - |
| $\quad 900$ | 719 | - |  |
| Stage 2 |  |  |  |
| Platoon blocked, \% | 163 | 0 | 973 |
| Mov Cap-1 Maneuver | 163 | 0 | - |
| Mov Cap-2 Maneuver | 242 | 0 | - |
| Stage 1 | 900 | 0 | - |
| Stage 2 |  |  |  |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | 55.9 |
| HCM LOS | F |

[^14]|  | * | $\rightarrow$ | $\rangle$ | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | F |  |  | $\uparrow$ | 7 |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 50 | 0 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 0 |  | 1 | 0 |  | 0 |
| Taper Length (tt) | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  |  |  |  | 0.976 |  |  |  | 0.850 |  |  |  |
| FIt Protected |  | 0.984 |  |  |  |  |  | 0.959 |  |  |  |  |
| Satd. Flow (prot) | 0 | 1598 | 0 | 0 | 1744 | 0 | 0 | 1692 | 1509 | 0 | 0 | 0 |
| Flt Permitted |  | 0.984 |  |  |  |  |  | 0.959 |  |  |  |  |
| Satd. Flow (perm) | 0 | 1598 | 0 | 0 | 1744 | 0 | 0 | 1692 | 1509 | 0 | 0 | 0 |
| Link Speed (mph) |  | 40 |  |  | 40 |  |  | 50 |  |  | 50 |  |
| Link Distance (ft) |  | 502 |  |  | 143 |  |  | 542 |  |  | 648 |  |
| Travel Time (s) |  | 8.6 |  |  | 2.4 |  |  | 7.4 |  |  | 8.8 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 3.7 |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 60 | 122 | 0 | 0 | 490 | 108 | 22 | 4 | 286 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | 50 |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, $\%$ | 17 | 17 | 0 | 0 | 4 | 17 | 0 | 50 | 7 |
| Mvmt Flow | 60 | 122 | 0 | 0 | 490 | 108 | 22 | 4 | 286 |


| Major/Minor | Major1 |  | Major2 |  |  | Minor1 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 598 | 0 | 0 | 122 | 0 | 0 | 786 | 840 | 122 |
| Stage 1 | - | - | - | - | - | - | 242 | 242 |  |
| Stage 2 | - | - | - |  | - | - | 544 | 598 |  |
| Critical Hdwy | 4.27 | - | - | 4.1 | - | - | 6.4 | 7 | 6.27 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 5.4 | 6 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 5.4 | 6 |  |
| Follow-up Hdwy | 2.353 | - | - | 2.2 | - | - | 3.5 | 4.45 | 3.363 |
| Pot Cap-1 Maneuver | 909 | - | - | 1478 | - | - | 364 | 254 | 916 |
| Stage 1 | - | - | - | - | - | - | 803 | 625 |  |
| Stage 2 | - | - | - | - | - | - | 586 | 422 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 909 | - | - | 1478 | - | - | 338 | 0 | 916 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 338 | 0 |  |
| Stage 1 | - | - | - | - | - | - | 746 | 0 |  |
| Stage 2 | - | - | - | - | - | - | 586 | 0 |  |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 3 | 0 | 11.2 |
| HCM LOS |  |  | B |


| Minor Lane/Major Mvmt | NBLn1 | NBLn2 | EBL | EBT | EBR | WBL | WBT | WBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 338 | 916 | 909 | - | - | 1478 | - | - |
| HCM Lane V/C Ratio | 0.077 | 0.312 | 0.066 | - | - | - | - | - |
| HCM Control Delay (s) | 16.5 | 10.7 | 9.2 | 0 | - | 0 | - | - |
| HCM Lane LOS | C | B | A | A | - | A | - | - |
| HCM 95th \%tile Q(veh) | 0.2 | 1.3 | 0.2 | - | - | 0 | - | - |


| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | SBL | SBT | SBR |
| Vol, veh/h | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | - | - | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 |
| Heavy Vehicles, \% | 0 | 0 | 0 |
| Mvmt Flow | 0 | 0 | 0 |


| Major/Minor |
| :--- |
| Conflicting Flow All |
| $\quad$ Stage 1 |
| $\quad$ Stage 2 |
| Critical Hdwy |
| Critical Hdwy Stg 1 |
| Critical Hdwy Stg 2 |
| Follow-up Hdwy |
| Pot Cap-1 Maneuver |
| $\quad$ Stage 1 |
| $\quad$ Stage 2 |
| Platoon blocked, \% |
| Mov Cap-1 Maneuver |
| Mov Cap-2 Maneuver |
| Stage 1 |
| Stage 2 |

## Approach

HCM Control Delay, s
HCMLOS

## Minor Lane/Major Mvmt

|  | $\rangle$ | $\rightarrow$ | 7 | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | F |  |  | ${ }_{\dagger}$ |  |  | ${ }_{\dagger}$ |  |  | ¢ |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  | 0.998 |  |  | 0.999 |  |  | 0.955 |  |  | 0.890 |  |
| Flt Protected | 0.950 |  |  |  | 0.999 |  |  | 0.968 |  |  | 0.994 |  |
| Satd. Flow (prot) | 1150 | 1725 | 0 | 0 | 1827 | 0 | 0 | 1493 | 0 | 0 | 1137 | 0 |
| Flt Permitted | 0.950 |  |  |  | 0.999 |  |  | 0.968 |  |  | 0.994 |  |
| Satd. Flow (perm) | 1150 | 1725 | 0 | 0 | 1827 | 0 | 0 | 1493 | 0 | 0 | 1137 | 0 |
| Link Speed (mph) |  | 40 |  |  | 50 |  |  | 40 |  |  | 40 |  |
| Link Distance (ft) |  | 143 |  |  | 173 |  |  | 583 |  |  | 174 |  |
| Travel Time (s) |  | 2.4 |  |  | 2.4 |  |  | 9.9 |  |  | 3.0 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type:

Other

| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 1.5 |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 12 | 392 | 4 | 8 | 538 | 4 | 8 | 0 | 4 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | 0 | - | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 57 | 10 | 0 | 25 | 3 | 67 | 14 | 0 | 25 |
| Mvmt Flow | 12 | 392 | 4 | 8 | 538 | 4 | 8 | 0 | 4 |
| Major/Minor | Major1 |  |  | Major2 |  |  | Minor1 |  |  |
| Conflicting Flow All | 542 | 0 | 0 | 396 | 0 | 0 | 1002 | 976 | 394 |
| Stage 1 | - | - | - | - | - | - | 418 | 418 |  |
| Stage 2 | - | - | - | - | - | - | 584 | 558 |  |
| Critical Hdwy | 4.67 | - | - | 4.35 | - | - | 7.24 | 6.5 | 6.45 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.24 | 5.5 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.24 | 5.5 |  |
| Follow-up Hdwy | 2.713 | - | - | 2.425 | - | - | 3.626 | 4 | 3.525 |
| Pot Cap-1 Maneuver | 800 | - | - | 1048 | - | - | 210 | 253 | 608 |
| Stage 1 | - | - | - | - | - | - | 589 | 594 |  |
| Stage 2 | - | - | - | - | - | - | 477 | 515 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 800 | - | - | 1048 | - | - | 180 | 246 | 608 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 180 | 246 | - |
| Stage 1 | - | - | - | - | - | - | 580 | 585 |  |
| Stage 2 | - | - | - | - | - | - | 416 | 509 |  |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0.3 | 0.1 | 21.1 |
| HCM LOS |  |  | C |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 235 | 800 | - | - | 1048 | - | - | 351 |
| HCM Lane V/C Ratio | 0.051 | 0.015 | - | - | 0.008 | - | - | 0.182 |
| HCM Control Delay (s) | 21.1 | 9.6 | - | - | 8.5 | 0 | - | 17.5 |
| HCM Lane LOS | C | A | - | - | A | A | - | C |
| HCM 95th \%tile Q(veh) | 0.2 | 0 | - | - | 0 | - | - | 0.7 |


| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | SBL | SBT | SBR |
| Vol, veh/h | 8 | 4 | 52 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | - | - | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 |
| Heavy Vehicles, \% | 86 | 100 | 38 |
| Mvmt Flow | 8 | 4 | 52 |
|  |  |  |  |


| Major/Minor | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Conflicting Flow All | 976 | 976 | 540 |
| Stage 1 | 556 | 556 | - |
| Stage 2 | 420 | 420 | - |
| Critical Hdwy | 7.96 | 7.5 | 6.58 |
| Critical Hdwy Stg 1 | 6.96 | 6.5 | - |
| Critical Hdwy Stg 2 | 6.96 | 6.5 | - |
| Follow-up Hdwy | 4.274 | 4.9 | 3.642 |
| Pot Cap-1 Maneuver | 164 | 174 | 478 |
| $\quad$ Stage 1 | 393 | 384 | - |
| Stage 2 | 475 | 452 | - |
| Platoon blocked, \% | 160 | 170 | 478 |
| Mov Cap-1 Maneuver | 160 | 170 | - |
| Mov Cap-2 Maneuver | 387 | 380 | - |
| Stage 1 | 465 | 445 | - |
| Stage 2 |  |  |  |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | 17.5 |
| HCM LOS | C |

[^15]Area Type: Other


| Major/Minor | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 78 | 0 | 357 | 76 |
| Stage 1 | - | - | - | - | 76 | - |
| Stage 2 | - | - | - | - | 281 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.4 | 6.27 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.5 | 3.363 |
| Pot Cap-1 Maneuver | - | - | 1520 | - | 645 | 971 |
| Stage 1 | - | - | - | - | 952 | - |
| Stage 2 | - | - | - | - | 771 |  |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1520 | - | 602 | 971 |
| Mov Cap-2 Maneuver | - | - | - | - | 602 | - |
| Stage 1 | - | - | - | - | 952 | - |
| Stage 2 | - | - | - | - | 719 | - |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0 | 4 | 9.6 |
| HCM LOS |  |  | A |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 889 | - | - | 1520 | - |
| HCM Lane V/C Ratio | 0.127 | - | - | 0.064 | - |
| HCM Control Delay (s) | 9.6 | - | - | 7.5 | 0 |
| HCM Lane LOS | A | - | - | A | A |
| HCM 95th \%tile Q(veh) | 0.4 | - | - | 0.2 | - |


|  | $\Rightarrow$ | $\rightarrow$ | $\geqslant$ | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $P$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | F |  |  | $\uparrow$ |  |  |  |  |  | $\uparrow$ | F |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 25 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 1 |
| Taper Length (tt) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  | 0.973 |  |  |  |  |  |  |  |  |  | 0.850 |
| Flt Protected |  |  |  |  | 0.963 |  |  |  |  |  | 0.953 |  |
| Satd. Flow (prot) | 0 | 1725 | 0 | 0 | 1735 | 0 | 0 | 0 | 0 | 0 | 1632 | 1583 |
| Flt Permitted |  |  |  |  | 0.963 |  |  |  |  |  | 0.953 |  |
| Satd. Flow (perm) | 0 | 1725 | 0 | 0 | 1735 | 0 | 0 | 0 | 0 | 0 | 1632 | 1583 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance ( t ) |  | 144 |  |  | 502 |  |  | 626 |  |  | 699 |  |
| Travel Time (s) |  | 3.3 |  |  | 11.4 |  |  | 14.2 |  |  | 15.9 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 23.3 |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 0 | 135 | 34 | 374 | 116 | 0 | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 0 | 9 | 0 | 5 | 7 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 0 | 135 | 34 | 374 | 116 | 0 | 0 | 0 | 0 |
| Major/Minor | Major1 |  |  | Major2 |  |  |  |  |  |
| Conflicting Flow All | 116 | 0 | 0 | 169 | 0 | 0 |  |  |  |
| Stage 1 | - | - | - | - | - | - |  |  |  |
| Stage 2 | - | - | - | - | - | - |  |  |  |
| Critical Hdwy | 4.1 | - | - | 4.15 | - | - |  |  |  |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |  |  |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |  |  |  |
| Follow-up Hdwy | 2.2 | - | - | 2.245 | - | - |  |  |  |
| Pot Cap-1 Maneuver | 1485 | - | - | 1390 | - | - |  |  |  |
| Stage 1 | - | - | - | - | - | - |  |  |  |
| Stage 2 | - | - | - | - | - | - |  |  |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1485 | - | - | 1390 | - | - |  |  |  |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |  |  |  |
| Stage 1 | - | - | - | - | - | - |  |  |  |
| Stage 2 | - | - | - | - | - | - |  |  |  |


| Approach | EB | WB |
| :--- | :---: | :---: |
| HCM Control Delay, s | 0 | 6.5 |
| HCM LOS |  |  |


| Minor Lane/Major Mvmt | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 | SBLn2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1485 | - | - | 1390 | - | - | 182 | 936 |
| HCM Lane V/C Ratio | - | - | - | 0.269 | - | - | 0.929 | 0.073 |
| HCM Control Delay (s) | 0 | - | - | 8.5 | 0 | - | 101 | 9.1 |
| HCM Lane LOS | A | - | - | A | A | - | F | A |
| HCM 95th \%tile Q(veh) | 0 | - | - | 1.1 | - | - | 7.2 | 0.2 |


| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | SBL | SBT | SBR |
| Vol, veh/h | 0 | 4 | 68 |
| Conflicting Peds, \#/hr | Stop | Stop | Stop |
| Sign Control | - | - | None |
| RT Channelized | - | - | 25 |
| Storage Length | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | 100 | 100 | 100 |
| Peak Hour Factor | 10 | 50 | 2 |
| Heavy Vehicles, \% | 165 | 4 | 68 |
| Mvmt Flow |  |  |  |
|  |  |  |  |


| Major/Minor | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Conflicting Flow All | 1016 | 1033 | 116 |
| $\quad$ Stage 1 | 864 | 864 | - |
| $\quad$ Stage 2 | 152 | 169 | - |
| Critical Hdwy | 6.5 | 7 | 6.22 |
| Critical Hdwy Stg 1 | 5.5 | 6 | - |
| Critical Hdwy Stg 2 | 5.5 | 6 | - |
| Follow-up Hdwy | 3.59 | 4.45 | 3.318 |
| Pot Cap-1 Maneuver | 255 | 192 | 936 |
| $\quad$ Stage 1 | 400 | 312 | - |
| $\quad$ Stage 2 | 857 | 676 | - |
| Platoon blocked, \% |  |  |  |
| Mov Cap-1 Maneuver | 182 | 0 | 936 |
| Mov Cap-2 Maneuver | 182 | 0 | - |
| Stage 1 | 285 | 0 | - |
| Stage 2 | 857 | 0 | - |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | 74.6 |
| HCM LOS | F |

## Minor Lane/Major Mvmt

|  | * | $\rightarrow$ | $\rangle$ | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | F |  |  | $\uparrow$ | 7 |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 50 | 0 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 0 |  | 1 | 0 |  | 0 |
| Taper Length (tt) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  |  |  |  | 0.971 |  |  |  | 0.850 |  |  |  |
| FIt Protected |  | 0.995 |  |  |  |  |  | 0.958 |  |  |  |  |
| Satd. Flow (prot) | 0 | 1741 | 0 | 0 | 1770 | 0 | 0 | 1630 | 1568 | 0 | 0 | 0 |
| Flt Permitted |  | 0.995 |  |  |  |  |  | 0.958 |  |  |  |  |
| Satd. Flow (perm) | 0 | 1741 | 0 | 0 | 1770 | 0 | 0 | 1630 | 1568 | 0 | 0 | 0 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance ( t ) |  | 502 |  |  | 143 |  |  | 542 |  |  | 648 |  |
| Travel Time (s) |  | 11.4 |  |  | 3.3 |  |  | 12.3 |  |  | 14.7 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |



| Major/Minor | Major1 |  | Major2 |  |  | Minor1 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 555 | 0 | 0 | 268 | 0 | 0 | 828 | 887 | 268 |
| Stage 1 | - | - | - | - | - | - | 332 | 332 |  |
| Stage 2 | - | - | - |  | - | - | 496 | 555 |  |
| Critical Hdwy | 4.15 | - | - | 4.1 | - | - | 6.46 | 7 | 6.23 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 5.46 | 6 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 5.46 | 6 |  |
| Follow-up Hdwy | 2.245 | - | - | 2.2 | - | - | 3.554 | 4.45 | 3.327 |
| Pot Cap-1 Maneuver | 1001 | - | - | 1307 | - | - | 336 | 237 | 768 |
| Stage 1 | - | - | - | - | - | - | 718 | 567 |  |
| Stage 2 | - | - | - | - | - | - | 604 | 443 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1001 | - | - | 1307 | - | - | 323 | 0 | 768 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 323 | 0 |  |
| Stage 1 | - | - | - | - | - | - | 691 | 0 |  |
| Stage 2 | - | - | - | - | - | - | 604 | 0 |  |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0.9 | 0 | 23.1 |
| HCM LOS |  |  | $C$ |


| Minor Lane/Major Mvmt | NBLn1 | NBLn2 | EBL | EBT | EBR | WBL | WBT | WBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 323 | 768 | 1001 | - | - | 1307 | - | - |
| HCM Lane V/C Ratio | 0.192 | 0.77 | 0.032 | - | - | - | - | - |
| HCM Control Delay (s) | 18.8 | 23.5 | 8.7 | 0 | - | 0 | - | - |
| HCM Lane LOS | C | C | A | A | - | A | - | - |
| HCM 95th \%tile Q(veh) | 0.7 | 7.5 | 0.1 | - | - | 0 | - | - |


| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | SBL | SBT | SBR |
| Vol, veh/h | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | - | - | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 |
| Heavy Vehicles, \% | 0 | 0 | 0 |
| Mvmt Flow | 0 | 0 | 0 |


| Major/Minor |
| :--- |
| Conflicting Flow All |
| $\quad$ Stage 1 |
| $\quad$ Stage 2 |
| Critical Hdwy |
| Critical Hdwy Stg 1 |
| Critical Hdwy Stg 2 |
| Follow-up Hdwy |
| Pot Cap-1 Maneuver |
| $\quad$ Stage 1 |
| $\quad$ Stage 2 |
| Platoon blocked, \% |
| Mov Cap-1 Maneuver |
| Mov Cap-2 Maneuver |
| Stage 1 |
| Stage 2 |

## Approach

HCM Control Delay, s
HCM LOS

## Minor Lane/Major Mvmt

|  | $\rangle$ | $\rightarrow$ | $\rangle$ | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | F |  |  | ¢ |  |  | ${ }_{4}$ |  |  | ${ }_{\dagger}$ |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length ( t ) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  | 0.998 |  |  | 0.998 |  |  | 0.932 |  |  | 0.879 |  |
| Flt Protected | 0.950 |  |  |  | 0.999 |  |  | 0.976 |  |  | 0.997 |  |
| Satd. Flow (prot) | 1308 | 1818 | 0 | 0 | 1829 | 0 | 0 | 1728 | 0 | 0 | 1381 | 0 |
| Flt Permitted | 0.950 |  |  |  | 0.999 |  |  | 0.976 |  |  | 0.997 |  |
| Satd. Flow (perm) | 1308 | 1818 | 0 | 0 | 1829 | 0 | 0 | 1728 | 0 | 0 | 1381 | 0 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance ( t ) |  | 143 |  |  | 173 |  |  | 583 |  |  | 174 |  |
| Travel Time (s) |  | 3.3 |  |  | 3.9 |  |  | 13.3 |  |  | 4.0 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type:

Other

| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 1.8 |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 32 | 815 | 12 | 5 | 448 | 8 | 5 | 0 | 5 |
| Conflicting Peds, \#hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | 0 | - | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 38 | 4 | 25 | 25 | 2 | 77 | 0 | 0 | 0 |
| Mvmt Flow | 32 | 815 | 12 | 5 | 448 | 8 | 5 | 0 | 5 |
| Major/Minor | Major1 |  |  | Major2 |  |  | Minor1 |  |  |
| Conflicting Flow All | 456 | 0 | 0 | 827 | 0 | 0 | 1401 | 1351 | 821 |
| Stage 1 | - | - | - | - | - | - | 885 | 885 |  |
| Stage 2 | - | - | - | - | - | - | 516 | 466 |  |
| Critical Hdwy | 4.48 | - | - | 4.35 | - | - | 7.1 | 6.5 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.5 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.1 | 5.5 |  |
| Follow-up Hdwy | 2.542 | - | - | 2.425 | - | - | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 939 | - | - | 713 | - | - | 119 | 152 | 378 |
| Stage 1 | - | - | - | - | - | - | 342 | 366 | - |
| Stage 2 | - | - | - | - | - | - | 546 | 566 | - |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 939 | - | - | 713 | - | - | 92 | 145 | 378 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 92 | 145 |  |
| Stage 1 | - | - | - | - | - | - | 330 | 354 |  |
| Stage 2 | - | - | - | - | - | - | 439 | 561 |  |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0.3 | 0.1 | 31.1 |
| HCM LOS |  |  | D |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 148 | 939 | - | - | 713 | - | - | 419 |
| HCM Lane V/C Ratio | 0.068 | 0.034 | - | - | 0.007 | - | - | 0.274 |
| HCM Control Delay (s) | 31.1 | 9 | - | - | 10.1 | 0 | - | 16.8 |
| HCM Lane LOS | D | A | - | - | B | A | - | C |
| HCM 95th \%tile Q(veh) | 0.2 | 0.1 | - | - | 0 | - | - | 1.1 |


| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | 8 | 4 | 103 |
| Vol, veh/h | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | Stop | Stop | Stop |
| Sign Control | - | - | None |
| RT Channelized | - | - | - |
| Storage Length | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | 100 | 100 | 100 |
| Peak Hour Factor | 0 | 0 | 23 |
| Heavy Vehicles, \% | 8 | 4 | 103 |
| Mvmt Flow |  |  |  |
|  |  |  |  |


| Major/Minor | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Conflicting Flow All | 1350 | 1353 | 452 |
| $\quad$ Stage 1 | 462 | 462 | - |
| $\quad$ Stage 2 | 888 | 891 | - |
| Critical Hdwy | 7.1 | 6.5 | 6.43 |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - |
| Follow-up Hdwy | 3.5 | 4 | 3.507 |
| Pot Cap-1 Maneuver | 129 | 151 | 566 |
| $\quad$ Stage 1 | 584 | 568 | - |
| $\quad$ Stage 2 | 341 | 363 | - |
| Platoon blocked, \% |  |  |  |
| Mov Cap-1 Maneuver | 123 | 145 | 566 |
| Mov Cap-2 Maneuver | 123 | 145 | - |
| Stage 1 | 564 | 563 | - |
| Stage 2 | 325 | 351 | - |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | 16.8 |
| HCM LOS | C |

## Minor Lane/Major Mvmt




| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0 | 4.1 | 9 |
| HCM LOS |  |  | A |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 967 | - | - | 1513 | - |
| HCM Lane V/C Ratio | 0.058 | - | - | 0.044 | - |
| HCM Control Delay (s) | 9 | - | - | 7.5 | 0 |
| HCM Lane LOS | A | - | - | A | A |
| HCM 95th \%tile Q(veh) | 0.2 | - | - | 0.1 | - |


|  | $\Rightarrow$ | $\rightarrow$ | $\geqslant$ | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | F |  |  | $\uparrow$ |  |  |  |  |  | $\uparrow$ | F |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 25 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 1 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Fit |  | 0.948 |  |  |  |  |  |  |  |  |  | 0.850 |
| Flt Protected |  |  |  |  | 0.958 |  |  |  |  |  | 0.954 |  |
| Satd. Flow (prot) | 0 | 1673 | 0 | 0 | 1774 | 0 | 0 | 0 | 0 | 0 | 1745 | 1429 |
| Flt Permitted |  |  |  |  | 0.958 |  |  |  |  |  | 0.954 |  |
| Satd. Flow (perm) | 0 | 1673 | 0 | 0 | 1774 | 0 | 0 | 0 | 0 | 0 | 1745 | 1429 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance ( t ) |  | 144 |  |  | 502 |  |  | 626 |  |  | 699 |  |
| Travel Time (s) |  | 3.3 |  |  | 11.4 |  |  | 14.2 |  |  | 15.9 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |



| Approach | EB | WB |
| :--- | ---: | :---: |
| HCM Control Delay, s | 0 | 7.1 |
| HCM LOS |  |  |


| Minor Lane/Major Mvmt | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 | SBLn2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1577 | - | - | 1488 | - | - | 286 | 996 |
| HCM Lane V/C Ratio | - | - | - | 0.215 | - | - | 0.524 | 0.076 |
| HCM Control Delay (s) | 0 | - | - | 8.1 | 0 | - | 30.7 | 8.9 |
| HCM Lane LOS | A | - | - | A | A | - | D | A |
| HCM 95th \%tile Q(veh) | 0 | - | - | 0.8 | - | - | 2.8 | 0.2 |


| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | SBL | SBT | SBR |
| Vol, veh/h | 0 | 4 | 76 |
| Conflicting Peds, \#/hr | Stop | Stop | Stop |
| Sign Control | - | - | None |
| RT Channelized | - | - | 25 |
| Storage Length | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | 100 | 100 | 100 |
| Peak Hour Factor | 4 | 0 | 13 |
| Heavy Vehicles, \% | 146 | 4 | 76 |
| Mvmt Flow |  |  |  |


| Major/Minor | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Conflicting Flow All | 768 | 788 | 44 |
| Stage 1 | 684 | 684 | - |
| Stage 2 | 84 | 104 | - |
| Critical Hdwy | 6.44 | 6.5 | 6.33 |
| Critical Hdwy Stg 1 | 5.44 | 5.5 | - |
| Critical Hdwy Stg 2 | 5.44 | 5.5 | - |
| Follow-up Hdwy | 3.536 | 4 | 3.417 |
| Pot Cap-1 Maneuver | 367 | 326 | 996 |
| $\quad$ Stage 1 | 497 | 452 | - |
| Stage 2 | 934 | 813 | - |
| Platoon blocked, \% | 286 | 0 | 996 |
| Mov Cap-1 Maneuver | 286 | 0 | - |
| Mov Cap-2 Maneuver | 388 | 0 | - |
| Stage 1 | 934 | 0 | - |
| Stage 2 |  |  |  |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | 23.4 |
| HCM LOS | C |

## Minor Lane/Major Mvmt

|  | $\rangle$ | $\rightarrow$ | $\geqslant$ | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | F |  |  | $\uparrow$ | F |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 50 | 0 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 0 |  | 1 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  |  |  |  | 0.970 |  |  |  | 0.850 |  |  |  |
| Flt Protected |  | 0.992 |  |  |  |  |  | 0.960 |  |  |  |  |
| Satd. Flow (prot) | 0 | 1808 | 0 | 0 | 1755 | 0 | 0 | 1765 | 1568 | 0 | 0 | 0 |
| FIt Permitted |  | 0.992 |  |  |  |  |  | 0.960 |  |  |  |  |
| Satd. Flow (perm) | 0 | 1808 | 0 | 0 | 1755 | 0 | 0 | 1765 | 1568 | 0 | 0 | 0 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance ( t ) |  | 502 |  |  | 143 |  |  | 542 |  |  | 648 |  |
| Travel Time (s) |  | 11.4 |  |  | 3.3 |  |  | 12.3 |  |  | 14.7 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 6.7 |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 32 | 178 | 0 | 0 | 344 | 100 | 20 | 4 | 494 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | 50 |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 0 | 5 | 0 | 0 | 3 | 12 | 4 | 0 | 3 |
| Mumt Flow | 32 | 178 | 0 | 0 | 344 | 100 | 20 | 4 | 494 |
| Major/Minor | Major1 |  |  | Major2 |  |  | Minor1 |  |  |
| Conflicting Flow All | 444 | 0 | 0 | 178 | 0 | 0 | 636 | 686 | 178 |
| Stage 1 | - | - | - | - | - | - | 242 | 242 |  |
| Stage 2 |  | - | - | - | - | - | 394 | 444 |  |
| Critical Hdwy | 4.1 | - | - | 4.1 | - | - | 6.44 | 6.5 | 6.23 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 5.44 | 5.5 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 5.44 | 5.5 |  |
| Follow-up Hdwy | 2.2 | - | - | 2.2 | - | - | 3.536 | 4 | 3.327 |
| Pot Cap-1 Maneuver | 1127 | - | - | 1410 | - | - | 439 | 373 | 862 |
| Stage 1 | - | - | - | - | - | - | 794 | 709 |  |
| Stage 2 | - | - | - | - | - | - | 677 | 579 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1127 | - | - | 1410 | - | - | 425 | 0 | 862 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 425 | 0 |  |
| Stage 1 | - | - | - | - | - | - | 769 | 0 |  |
| Stage 2 | - | - | - | - | - | - | 677 | 0 |  |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 1.3 | 0 | 14.6 |
| HCM LOS |  |  | B |


| Minor Lane/Major Mvmt | NBLn1 | NBLn2 | EBL | EBT | EBR | WBL | WBT | WBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 425 | 862 | 1127 | - | - | 1410 | - | - |
| HCM Lane V/C Ratio | 0.056 | 0.573 | 0.028 | - | - | - | - | - |
| HCM Control Delay (s) | 14 | 14.6 | 8.3 | 0 | - | 0 | - | - |
| HCM Lane LOS | B | B | A | A | - | A | - | - |
| HCM 95th \%tile Q(veh) | 0.2 | 3.7 | 0.1 | - | - | 0 | - | - |


| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | SBL | SBT | SBR |
| Vol, veh/h | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | - | - | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 |
| Heavy Vehicles, \% | 0 | 0 | 0 |
| Mvmt Flow | 0 | 0 | 0 |


| Major/Minor |
| :--- |
| Conflicting Flow All |
| $\quad$ Stage 1 |
| $\quad$ Stage 2 |
| Critical Hdwy |
| Critical Hdwy Stg 1 |
| Critical Hdwy Stg 2 |
| Follow-up Hdwy |
| Pot Cap-1 Maneuver |
| $\quad$ Stage 1 |
| $\quad$ Stage 2 |
| Platoon blocked, \% |
| Mov Cap-1 Maneuver |
| Mov Cap-2 Maneuver |
| Stage 1 |
| Stage 2 |

## Approach

HCM Control Delay, s
HCMLOS

## Minor Lane/Major Mvmt

|  | $\rangle$ | $\rightarrow$ | 7 | $\downarrow$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | F |  |  | ¢ |  |  | $\uparrow$ |  |  | ${ }_{\text {¢ }}$ |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Fit |  | 0.999 |  |  | 0.999 |  |  | 0.966 |  |  | 0.883 |  |
| Flt Protected | 0.950 |  |  |  | 0.999 |  |  | 0.976 |  |  | 0.995 |  |
| Satd. Flow (prot) | 1570 | 1824 | 0 | 0 | 1829 | 0 | 0 | 1518 | 0 | 0 | 1456 | 0 |
| Flt Permitted | 0.950 |  |  |  | 0.999 |  |  | 0.976 |  |  | 0.995 |  |
| Satd. Flow (perm) | 1570 | 1824 | 0 | 0 | 1829 | 0 | 0 | 1518 | 0 | 0 | 1456 | 0 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 143 |  |  | 173 |  |  | 583 |  |  | 174 |  |
| Travel Time (s) |  | 3.3 |  |  | 3.9 |  |  | 13.3 |  |  | 4.0 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type:

Other

| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 1.4 |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 4 | 664 | 4 | 4 | 360 | 4 | 8 | 4 | 4 |
| Conflicting Peds, \#hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | 0 | - | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 15 | 4 | 17 | 0 | 3 | 67 | 11 | 0 | 50 |
| Mvmt Flow | 4 | 664 | 4 | 4 | 360 | 4 | 8 | 4 | 4 |
| Major/Minor | Major1 |  |  | Major2 |  |  | Minor1 |  |  |
| Conflicting Flow All | 364 | 0 | 0 | 668 | 0 | 0 | 1084 | 1046 | 666 |
| Stage 1 | - | - | - | - | - | - | 674 | 674 |  |
| Stage 2 | - | - | - | - | - | - | 410 | 372 |  |
| Critical Hdwy | 4.25 | - | - | 4.1 | - | - | 7.21 | 6.5 | 6.7 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.21 | 5.5 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.21 | 5.5 |  |
| Follow-up Hdwy | 2.335 | - | - | 2.2 | - | - | 3.599 | 4 | 3.75 |
| Pot Cap-1 Maneuver | 1126 | - | - | 931 | - | - | 187 | 230 | 385 |
| Stage 1 | - | - | - | - | - | - | 430 | 457 | - |
| Stage 2 | - | - | - | - | - | - | 601 | 622 | - |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1126 | - | - | 931 | - | - | 162 | 228 | 385 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 162 | 228 |  |
| Stage 1 | - | - | - | - | - | - | 428 | 455 |  |
| Stage 2 | - | - | - | - | - | - | 525 | 619 |  |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0 | 0.1 | 23.8 |
| HCM LOS |  |  | $C$ |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 207 | 1126 | - | - | 931 | - | - | 506 |
| HCM Lane V/C Ratio | 0.077 | 0.004 | - | - | 0.004 | - | - | 0.174 |
| HCM Control Delay (s) | 23.8 | 8.2 | - | - | 8.9 | 0 | - | 13.6 |
| HCM Lane LOS | C | A | - | - | A | A | - | B |
| HCM 95th \%tile Q(veh) | 0.2 | 0 | - | - | 0 | - | - | 0.6 |


| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | 8 | 4 | 76 |
| Vol, veh/h | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | Stop | Stop | Stop |
| Sign Control | - | - | None |
| RT Channelized | - | - | - |
| Storage Length | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | 100 | 100 | 100 |
| Peak Hour Factor | 0 | 0 | 17 |
| Heavy Vehicles, \% | 8 | 4 | 76 |
| Mvmt Flow |  |  |  |


| Major/Minor | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Conflicting Flow All | 1048 | 1046 | 362 |
| $\quad$ Stage 1 | 370 | 370 | - |
| $\quad$ Stage 2 | 678 | 676 | - |
| Critical Hdwy | 7.1 | 6.5 | 6.37 |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - |
| Follow-up Hdwy | 3.5 | 4 | 3.453 |
| Pot Cap-1 Maneuver | 208 | 230 | 650 |
| $\quad$ Stage 1 | 654 | 624 | - |
| $\quad$ Stage 2 | 445 | 456 | - |
| Platoon blocked, \% |  |  |  |
| Mov Cap-1 Maneuver | 202 | 228 | 650 |
| Mov Cap-2 Maneuver | 202 | 228 | - |
| Stage 1 | 652 | 621 | - |
| Stage 2 | 435 | 454 | - |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | 13.6 |
| HCM LOS | B |

## Minor Lane/Major Mvmt

## Appendix N Signal Warrant Analysis Worksheets for Existing Conditions



| Project \#: | 12393 |
| :--- | :--- |
| Project Name: | Cowlitz Reservation Development |
| Analyst: | JJW |
| Date: | $8 / 27 / 2014$ |
| File: | H:\projfile $\backslash 12393$-Cowlitz Reservation Development $\backslash$ excel $\backslash 2014$ |
|  | Data 1 signal warrants $\backslash$ [103 2014 Existing AM Sig Warrant.x\|s]Data |
| Intersection: | NW La Center Road and SB Ramp |
| Scenario: | 2014 Existing |

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610 SW Alder, Suite 700
Portland, Oregon 97205
(503) 228-5230

Fax: (503) 273-8169

12393
Project Name: Cowlitz Reservation Development
$\begin{array}{ll}\text { File: } & \text { H:\projfile } \backslash 12393 \text { - Cowlitz Reservation Development } \backslash \text { excel } \backslash 2014 \\ & \text { Data } \text { Ssignal warrants } \backslash[1032014 \text { Existing AM Sig Warrant.xls]Data } \\ \text { Intersection: } & \bar{N} W \text { La Center Road and SB Ramp } \\ \text { Scenario: } & 2014 \text { Existing }\end{array}$

Warrant Summary

| Warrant | Name | Analyzed? | Met? |
| :---: | :--- | :---: | :---: |
| $\# 1$ | Eight-Hour Vehicular Volume | Yes | No |
| $\# 2$ | Four-Hour Vehicular volume | Yes | No |
| $\# 3$ | Peak Hour | Yes | No |
| $\# 4$ | Pedestrian Volume | No | - |
| $\# 5$ | School Crossing | No | - |
| $\# 6$ | Coordinated Signal System | No | - |
| $\# 7$ | Crash Experience | No | - |
| $\# 8$ | Roadway Network | No | - |


| Hour |  | Major Street |  | Minor Street |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Begin | End | EB | WB | NB | SB |
| 7:00 AM | 8:00 AM | 112 | 512 | 0 | 112 |
| 2nd | Highest Hour | 108 | 492 | 0 | 108 |
| 3rd | Highest Hour | 105 | 481 | 0 | 105 |
| 4th | Highest Hour | 90 | 410 | 0 | 90 |
| 5th | Highest Hour | 85 | 389 | 0 | 85 |
| 6th | Highest Hour | 76 | 348 | 0 | 76 |
| 7th | Highest Hour | 71 | 323 | 0 | 71 |
| 8th | Highest Hour | 67 | 307 | 0 | 67 |
| 9th | Highest Hour | 54 | 246 | 0 | 54 |
| 10th | Highest Hour | 50 | 230 | 0 | 50 |
| 11th | Highest Hour | 50 | 230 | 0 | 50 |
| 12th | Highest Hour | 48 | 220 | 0 | 48 |
| 13th | Highest Hour | 44 | 200 | 0 | 44 |
| 14th | Highest Hour | 40 | 184 | 0 | 40 |
| 15th | Highest Hour | 40 | 184 | 0 | 40 |
| 16th | Highest Hour | 39 | 179 | 0 | 39 |
| 17th | Highest Hour | 22 | 102 | 0 | 22 |
| 18th | Highest Hour | 12 | 56 | 0 | 12 |
| 19th | Highest Hour | 11 | 51 | 0 | 11 |
| 20th | Highest Hour | 4 | 20 | 0 | 4 |
| 21st | Highest Hour | 3 | 15 | 0 | 3 |
| 22nd | Highest Hour | 3 | 15 | 0 | 3 |
| 23rd | Highest Hour | 2 | 10 | 0 | 2 |
| 24th | Highest Hour | 2 | 10 | 0 | 2 |


| Analysis Traffic Volumes |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Hour |  | Major Street |  | Minor Street |  |
| Begin | End | EB | WB | NB | SB |
| 7:00 AM | 8:00 AM | 112 | 512 | 0 | 112 |
| 2nd | Highest Hour | 108 | 492 | 0 | 108 |
| 3 rd | Highest Hour | 105 | 481 | 0 | 105 |
| 4th | Highest Hour | 90 | 410 | 0 | 90 |
| 5 th | Highest Hour | 85 | 389 | 0 | 85 |
| 6th | Highest Hour | 76 | 348 | 0 | 76 |
| 7th | Highest Hour | 71 | 323 | 0 | 71 |
| 8th | Highest Hour | 67 | 307 | 0 | 67 |
| 9th | Highest Hour | 54 | 246 | 0 | 54 |
| 10th | Highest Hour | 50 | 230 | 0 | 50 |
| 11th | Highest Hour | 50 | 230 | 0 | 50 |
| 12th | Highest Hour | 48 | 220 | 0 | 48 |
| 13th | Highest Hour | 44 | 200 | 0 | 44 |
| 14th | Highest Hour | 40 | 184 | 0 | 40 |
| 15th | Highest Hour | 40 | 184 | 0 | 40 |
| 16th | Highest Hour | 39 | 179 | 0 | 39 |
| 17th | Highest Hour | 22 | 102 | 0 | 22 |
| 18th | Highest Hour | 12 | 56 | 0 | 12 |
| 19th | Highest Hour | 11 | 51 | 0 | 11 |
| 20th | Highest Hour | 4 | 20 | 0 | 4 |
| 21st | Highest Hour | 3 | 15 | 0 | 3 |
| 22nd | Highest Hour | 3 | 15 | 0 | 3 |
| 23rd | Highest Hour | 2 | 10 | 0 | 2 |
| 24th | Highest Hour | 2 | 10 | 0 | 2 |

## Appendix O 2017 Background Conditions Worksheets - Freeway Mainline








| BASIC FREEWAY SEGMENTS WORKSHEET |  |  |  |
| :---: | :---: | :---: | :---: |
| General Information |  | \|Site Information |  |
| Analyst <br> Agency or Company <br> Date Performed <br> Analysis Time Period | KML <br> KAI <br> 6/25/2014 <br> Weekday PM Peak Hour | From/To La C <br> Jurisdiction WSD <br> Analysis Year 2017 | er Rd to SR 503 |
| Project Description 12393 |  |  |  |
| $\checkmark$ Oper.(LOS) $\square$ |  | Des.(N) $\quad \square$ | $\square$ Planning Data |
| Flow Inputs |  |  |  |
| Volume, V <br> AADT | $2775 \quad \begin{aligned} & \text { veh/h } \\ & \text { veh/day }\end{aligned}$ | Peak-Hour Factor, PHF 1.00 <br> \%Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ 11 |  |
| Peak-Hr Prop. of AADT, K |  | \%RVs, $\mathrm{P}_{\mathrm{R}}$ |  |
| Peak-Hr Direction Prop, D DDHV $=$ AADT $\times K \times D$ | veh/h | $\begin{array}{lll} \text { General Terrain: } & \text { Leve } \\ \text { Grade } & \% & \text { Length } \\ & \text { Up/Down \% } & \text { mi } \end{array}$ |  |
| Calculate Flow Adjustments |  |  |  |
| $\mathrm{f}_{\mathrm{p}}$ | 1.00 | $\begin{aligned} & E_{R} \quad 1.2 \\ & f_{H V}=1\left[1+P_{T}\left(E_{T}-1\right)+P_{R}\left(E_{R}-1\right)\right] 0.948 \end{aligned}$ |  |
| $E_{T}$ | 1.5 |  |  |
| Speed Inputs |  | Calc Speed Adj and FFS |  |
| Lane Width | 12.0 ft | $f_{L w}$ 0.0 <br> $f_{L C}$ 0.0 <br> TRD Adjustment 2.3 <br> FFS 73.1 | mph <br> mph <br> mph <br> mph |
| Rt-Side Lat. Clearance | 6.0 ft |  |  |
| Number of Lanes, N | 3 |  |  |
| Total Ramp Density, TRD | $0.67 \mathrm{ramps} / \mathrm{mi}$ |  |  |
| FFS (measured) <br> Base free-flow Speed, <br> BFFS | 75.4 mph |  |  |
| LOS and Performance Measures |  | Design (N) |  |
| Operational (LOS) |  | Design (N) |  |
| $\begin{array}{lll} \left.\begin{array}{lll} \mathrm{v}_{\mathrm{p}}=(\mathrm{V} \text { or DDHV }) /\left(\mathrm{PHF} \times \mathrm{N} \times \mathrm{f}_{\mathrm{Hv}} 976\right. & \mathrm{pc} / \mathrm{h} / \mathrm{ln} \\ \times \mathrm{f}_{\mathrm{p}} \end{array}\right) & & \mathrm{mph} \\ \mathrm{~S} \end{array}$ |  | $\begin{aligned} & \text { Design LOS } \\ & v_{p}=(V \text { or DDHV }) /\left(\text { PHF } \times N \times f_{H V}\right. \\ & \left.\times f_{p}\right) \end{aligned}$ | $\mathrm{pc} / \mathrm{h} / \mathrm{ln}$ |
|  |  |  |  |
| $D=v_{p} / S$ | $\begin{array}{ll} 75.0 & \mathrm{mph} \\ 13.0 & \mathrm{pc} / \mathrm{mi} / \mathrm{ln} \end{array}$ | $D=v_{p} / s$ <br> Required Number of Lanes, N | mph <br> pc/mi/ln |
| LOS | B |  |  |
| Glossary |  | Factor Location |  |
| N - Number of lanes <br> V - Hourly volume <br> $v_{p}$ - Flow rate <br> LOS - Level of service <br> speed <br> DDHV - Directional design | D - Density <br> FFS - Free-flow speed BFFS - Base free-flow | $\begin{aligned} & E_{R} \text { - Exhibits 11-10, 11-12 } \\ & E_{T} \text { - Exhibits 11-10, 11-11, 11-13 } \\ & f_{p} \text { - Page 11-18 } \\ & \text { LOS, S, FFS, } v_{p} \text { - Exhibits 11-2, } \\ & 11-3 \end{aligned}$ | $\begin{aligned} & \mathrm{f}_{\mathrm{LW}}-\text { Exhibit } 11-8 \\ & \mathrm{f}_{\mathrm{LC}} \text { - Exhibit } 11-9 \\ & \text { TRD - Page 11-11 } \end{aligned}$ |







## Appendix P 2017 Background Conditions Worksheets - Merge/Diverge Locations




















## Appendix Q 2017 Background Conditions Worksheets - Study Intersections



| Intersection |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 4.4 |  |  |  |  |  |  |
| Movement |  | EBT | EBR | WBL | WBT | NBL | NBR |
| Vol, veh/h |  | 55 | 20 | 49 | 51 | 5 | 78 |
| Conflicting Peds, \#/hr |  | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control |  | Free | Free | Free | Free | Stop | Stop |
| RT Channelized |  | - | None | - | None | - | None |
| Storage Length |  | - | - | - | - | 0 | - |
| Veh in Median Storage, \# |  | 0 | - | - | 0 | 0 | - |
| Grade, \% |  | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor |  | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% |  | 8 | 0 | 11 | 4 | 0 | 23 |
| Mvmt Flow |  | 55 | 20 | 49 | 51 | 5 | 78 |


| Major/Minor | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 75 | 0 | 214 | 65 |
| Stage 1 | - | - | - | - | 65 | - |
| Stage 2 | - | - | - | - | 149 | - |
| Critical Hdwy | - | - | 4.21 | - | 6.4 | 6.43 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 | - |
| Follow-up Hdwy | - | - | 2.299 | - | 3.5 | 3.507 |
| Pot Cap-1 Maneuver | - | - | 1469 | - | 779 | 943 |
| Stage 1 | - | - | - | - | 963 |  |
| Stage 2 | - | - | - | - | 884 |  |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1469 | - | 753 | 943 |
| Mov Cap-2 Maneuver | - | - | - | - | 753 |  |
| Stage 1 | - | - | - | - | 963 |  |
| Stage 2 | - | - | - | - | 854 |  |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0 | 3.7 | 9.3 |
| HCM LOS |  |  | A |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 929 | - | - | 1469 | - |
| HCM Lane V/C Ratio | 0.089 | - | - | 0.033 | - |
| HCM Control Delay (s) | 9.3 | - | - | 7.5 | 0 |
| HCM Lane LOS | A | - | - | A | A |
| HCM 95th \%tile Q(veh) | 0.3 | - | - | 0.1 | - |


|  | $\Rightarrow$ | $\rightarrow$ | $\geqslant$ | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $P$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | F |  |  | $\uparrow$ |  |  |  |  |  | $\uparrow$ | F |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 25 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 1 |
| Taper Length (tt) | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  | 0.968 |  |  |  |  |  |  |  |  |  | 0.850 |
| Flt Protected |  |  |  |  | 0.959 |  |  |  |  |  | 0.954 |  |
| Satd. Flow (prot) | 0 | 1566 | 0 | 0 | 1747 | 0 | 0 | 0 | 0 | 0 | 1587 | 1442 |
| Flt Permitted |  |  |  |  | 0.959 |  |  |  |  |  | 0.954 |  |
| Satd. Flow (perm) | 0 | 1566 | 0 | 0 | 1747 | 0 | 0 | 0 | 0 | 0 | 1587 | 1442 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance ( t ) |  | 144 |  |  | 502 |  |  | 626 |  |  | 699 |  |
| Travel Time (s) |  | 3.3 |  |  | 11.4 |  |  | 14.2 |  |  | 15.9 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 33.1 |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 0 | 101 | 32 | 530 | 91 | 0 | 0 | 0 | 0 |
| Conflicting Peds, \#hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - |  | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 0 | 22 | 3 | 4 | 6 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 0 | 101 | 32 | 530 | 91 | 0 | 0 | 0 | 0 |
| Major/Minor | Major1 |  |  | Major2 |  |  |  |  |  |
| Conflicting Flow All | 91 | 0 | 0 | 133 | 0 | 0 |  |  |  |
| Stage 1 | - | - | - | - | - | - |  |  |  |
| Stage 2 | - | - | - | - | - | - |  |  |  |
| Critical Hdwy | 4.1 | - | - | 4.14 | - | - |  |  |  |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |  |  |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |  |  |  |
| Follow-up Hdwy | 2.2 | - | - | 2.236 | - | - |  |  |  |
| Pot Cap-1 Maneuver | 1517 | - | - | 1440 | - | - |  |  |  |
| Stage 1 | - | - | - | - | - | - |  |  |  |
| Stage 2 | - | - | - | - | - | - |  |  |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1517 | - | - | 1440 | - | - |  |  |  |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |  |  |  |
| Stage 1 | - | - | - | - | - | - |  |  |  |
| Stage 2 | - | - | - | - | - | - |  |  |  |


| Approach | EB | WB |
| :--- | :---: | :---: |
| HCM Control Delay, s | 0 | 7.6 |
| HCM LOS |  |  |


| Minor Lane/Major Mvmt | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 | SBLn2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1517 | - | - | 1440 | - | - | 108 | 940 |
| HCM Lane V/C Ratio | - | - | - | 0.368 | - | - | 1.13 | 0.009 |
| HCM Control Delay (s) | 0 | - | - | 8.9 | 0 | - | 200.9 | 8.9 |
| HCM Lane LOS | A | - | - | A | A | - | F | A |
| HCM 95th \%tile Q(veh) | 0 | - | - | 1.7 | - | - | 7.7 | 0 |

## Notes

~: Volume exceeds capacity $\quad \$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ *: All major volume in platoon

| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | 118 | 4 | 8 |
| Vol, veh/h | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | Stop | Stop | Stop |
| Sign Control | - | - | None |
| RT Channelized | - | - | 25 |
| Storage Length | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | 100 | 100 | 100 |
| Peak Hour Factor | 13 | 50 | 12 |
| Heavy Vehicles, \% | 118 | 4 | 8 |
| Mvmt Flow |  |  |  |


| Major/Minor | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Conflicting Flow All | 1268 | 1284 | 91 |
| Stage 1 | 1151 | 1151 | - |
| $\quad$ Stage 2 | 117 | 133 | - |
| Critical Hdwy | 6.53 | 7 | 6.32 |
| Critical Hdwy Stg 1 | 5.53 | 6 | - |
| Critical Hdwy Stg 2 | 5.53 | 6 | - |
| Follow-up Hdwy | 3.617 | 4.45 | 3.408 |
| Pot Cap-1 Maneuver | 176 | 133 | 940 |
| $\quad$ Stage 1 | 287 | 223 | - |
| $\quad$ Stage 2 | 881 | 703 | - |
| Platoon blocked, \% |  |  |  |
| Mov Cap-1 Maneuver | $\sim 108$ | 0 | 940 |
| Mov Cap-2 Maneuver | $\sim 108$ | 0 | - |
| Stage 1 | 176 | 0 | - |
| Stage 2 | 881 | 0 | - |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | 189.1 |
| HCM LOS | F |

[^16]|  | * | $\rightarrow$ | $\rangle$ | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | F |  |  | $\uparrow$ | 7 |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 50 | 0 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 0 |  | 1 | 0 |  | 0 |
| Taper Length (tt) | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  |  |  |  | 0.972 |  |  |  | 0.850 |  |  |  |
| FIt Protected |  | 0.986 |  |  |  |  |  | 0.959 |  |  |  |  |
| Satd. Flow (prot) | 0 | 1601 | 0 | 0 | 1731 | 0 | 0 | 1696 | 1509 | 0 | 0 | 0 |
| Flt Permitted |  | 0.986 |  |  |  |  |  | 0.959 |  |  |  |  |
| Satd. Flow (perm) | 0 | 1601 | 0 | 0 | 1731 | 0 | 0 | 1696 | 1509 | 0 | 0 | 0 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 502 |  |  | 143 |  |  | 542 |  |  | 648 |  |
| Travel Time (s) |  | 11.4 |  |  | 3.3 |  |  | 12.3 |  |  | 14.7 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 3.7 |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 64 | 155 | 0 | 0 | 598 | 156 | 23 | 4 | 321 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | 50 |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 17 | 17 | 0 | 0 | 4 | 17 | 0 | 50 | 7 |
| Mumt Flow | 64 | 155 | 0 | 0 | 598 | 156 | 23 | 4 | 321 |
| Major/Minor | Major1 |  |  | Major2 |  |  | inor1 |  |  |
| Conflicting Flow All | 754 | 0 | 0 | 155 | 0 | 0 | 959 | 1037 | 155 |
| Stage 1 | - | - | - | - | - | - | 283 | 283 |  |
| Stage 2 |  | - | - | - | - | - | 676 | 754 |  |
| Critical Hdwy | 4.27 | - | - | 4.1 | - | - | 6.4 | 7 | 6.27 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 5.4 | 6 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 5.4 | 6 |  |
| Follow-up Hdwy | 2.353 | - | - | 2.2 | - | - | 3.5 | 4.45 | 3.363 |
| Pot Cap-1 Maneuver | 792 | - | - | 1438 | - | - | 288 | 191 | 878 |
| Stage 1 | - | - | - | - | - | - | 770 | 598 |  |
| Stage 2 | - | - | - | - | - | - | 509 | 354 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 792 | - | - | 1438 | - | - | 263 | 0 | 878 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 263 | 0 | - |
| Stage 1 | - | - | - | - | - | - | 702 | 0 | - |
| Stage 2 | - | - | - | - | - | - | 509 | 0 |  |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 2.9 | 0 | 12.1 |
| HCM LOS |  |  | B |


| Minor Lane/Major Mvmt | NBLn1 | NBLn2 | EBL | EBT | EBR | WBL | WBT | WBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 263 | 878 | 792 | - | - | 1438 | - | - |
| HCM Lane V/C Ratio | 0.103 | 0.366 | 0.081 | - | - | - | - | - |
| HCM Control Delay (s) | 20.2 | 11.4 | 9.9 | 0 | - | 0 | - | - |
| HCM Lane LOS | C | B | A | A | - | A | - | - |
| HCM 95th \%tile Q(veh) | 0.3 | 1.7 | 0.3 | - | - | 0 | - | - |


| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | SBL | SBT | SBR |
| Vol, veh/h | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | - | - | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 |
| Heavy Vehicles, \% | 0 | 0 | 0 |
| Mvmt Flow | 0 | 0 | 0 |


| Major/Minor |
| :--- |
| Conflicting Flow All |
| $\quad$ Stage 1 |
| $\quad$ Stage 2 |
| Critical Hdwy |
| Critical Hdwy Stg 1 |
| Critical Hdwy Stg 2 |
| Follow-up Hdwy |
| Pot Cap-1 Maneuver |
| $\quad$ Stage 1 |
| $\quad$ Stage 2 |
| Platoon blocked, \% |
| Mov Cap-1 Maneuver |
| Mov Cap-2 Maneuver |
| Stage 1 |
| Stage 2 |

## Approach

HCM Control Delay, s
HCMLOS

## Minor Lane/Major Mvmt

|  | \% | $\rightarrow$ | 7 | $\dagger$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | 1 | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | F |  |  | $\uparrow$ |  |  | ¢ |  |  | ${ }^{\text {¢ }}$ |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  | 0.999 |  |  | 0.998 |  |  | 0.955 |  |  | 0.896 |  |
| Flt Protected | 0.950 |  |  |  | 0.999 |  |  | 0.968 |  |  | 0.990 |  |
| Satd. Flow (prot) | 1150 | 1727 | 0 | 0 | 1817 | 0 | 0 | 1493 | 0 | 0 | 1399 | 0 |
| Flt Permitted | 0.950 |  |  |  | 0.999 |  |  | 0.968 |  |  | 0.990 |  |
| Satd. Flow (perm) | 1150 | 1727 | 0 | 0 | 1817 | 0 | 0 | 1493 | 0 | 0 | 1399 | 0 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 143 |  |  | 173 |  |  | 583 |  |  | 174 |  |
| Travel Time (s) |  | 3.3 |  |  | 3.9 |  |  | 13.3 |  |  | 4.0 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type:

Other

| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 3.9 |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 30 | 441 | 4 | 10 | 630 | 9 | 10 | 0 | 5 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | 0 | - | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 57 | 10 | 0 | 25 | 3 | 67 | 14 | 0 | 25 |
| Mvmt Flow | 30 | 441 | 4 | 10 | 630 | 9 | 10 | 0 | 5 |
| Major/Minor | Major1 |  |  | Major2 |  |  | Minor1 |  |  |
| Conflicting Flow All | 639 | 0 | 0 | 445 | 0 | 0 | 1217 | 1162 | 443 |
| Stage 1 | - | - | - | - | - | - | 503 | 503 |  |
| Stage 2 | - | - | - | - | - | - | 714 | 659 |  |
| Critical Hdwy | 4.67 | - | - | 4.35 | - | - | 7.24 | 6.5 | 6.45 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.24 | 5.5 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.24 | 5.5 |  |
| Follow-up Hdwy | 2.713 | - | - | 2.425 | - | - | 3.626 | 4 | 3.525 |
| Pot Cap-1 Maneuver | 730 | - | - | 1004 | - | - | 149 | 197 | 569 |
| Stage 1 | - | - | - | - | - | - | 529 | 545 | - |
| Stage 2 | - | - | - | - | - | - | 404 | 464 | - |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 730 | - | - | 1004 | - | - | 104 | 186 | 569 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 104 | 186 |  |
| Stage 1 | - | - | - | - | - | - | 507 | 523 |  |
|  | - | - | - | - | - | - | 293 | 457 |  |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0.6 | 0.1 | 33.1 |
| HCM LOS |  |  | D |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 143 | 730 | - | - | 1004 | - | - | 303 |
| HCM Lane V/C Ratio | 0.105 | 0.041 | - | - | 0.01 | - | - | 0.495 |
| HCM Control Delay (s) | 33.1 | 10.1 | - | - | 8.6 | 0 | - | 28 |
| HCM Lane LOS | D | B | - | - | A | A | - | D |
| HCM 95th \%tile Q(veh) | 0.3 | 0.1 | - | - | 0 | - | - | 2.6 |


| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | SBL | SBT | SBR |
| Vol, veh/h | 31 | 4 | 115 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | - | - | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 |
| Heavy Vehicles, \% | 23 | 100 | 17 |
| Mvmt Flow | 31 | 4 | 115 |
|  |  |  |  |


| Major/Minor | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Conflicting Flow All | 1161 | 1160 | 635 |
| $\quad$ Stage 1 | 655 | 655 | - |
| $\quad$ Stage 2 | 506 | 505 | - |
| Critical Hdwy | 7.33 | 7.5 | 6.37 |
| Critical Hdwy Stg 1 | 6.33 | 6.5 | - |
| Critical Hdwy Stg 2 | 6.33 | 6.5 | - |
| Follow-up Hdwy | 3.707 | 4.9 | 3.453 |
| Pot Cap-1 Maneuver | 157 | 130 | 453 |
| $\quad$ Stage 1 | 422 | 340 | - |
| $\quad$ Stage 2 | 512 | 408 | - |
| Platoon blocked, \% |  |  |  |
| Mov Cap-1 Maneuver | 149 | 123 | 453 |
| Mov Cap-2 Maneuver | 149 | 123 | - |
| Stage 1 | 405 | 335 | - |
| Stage 2 | 487 | 391 | - |


| Approach | SB |
| :--- | :---: |
| HCM Control Delay, s | 28 |
| HCM LOS | D |

[^17]Area Type: Other


| Major/Minor | Major1 |  | Major2 |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 78 | 0 | 357 | 76 |
| Stage 1 | - | - | - | - | 76 | - |
| Stage 2 | - | - | - | - | 281 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.4 | 6.27 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.5 | 3.363 |
| Pot Cap-1 Maneuver | - | - | 1520 | - | 645 | 971 |
| Stage 1 | - | - | - | - | 952 | - |
| Stage 2 | - | - | - | - | 771 |  |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1520 | - | 602 | 971 |
| Mov Cap-2 Maneuver | - | - | - | - | 602 | - |
| Stage 1 | - | - | - | - | 952 | - |
| Stage 2 | - | - | - | - | 719 | - |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0 | 4 | 9.6 |
| HCM LOS |  |  | A |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 889 | - | - | 1520 | - |
| HCM Lane V/C Ratio | 0.127 | - | - | 0.064 | - |
| HCM Control Delay (s) | 9.6 | - | - | 7.5 | 0 |
| HCM Lane LOS | A | - | - | A | A |
| HCM 95th \%tile Q(veh) | 0.4 | - | - | 0.2 | - |


|  | $\Rightarrow$ | $\rightarrow$ | $\geqslant$ | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $P$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | F |  |  | $\uparrow$ |  |  |  |  |  | $\uparrow$ | F |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 25 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 1 |
| Taper Length (tt) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  | 0.973 |  |  |  |  |  |  |  |  |  | 0.850 |
| Flt Protected |  |  |  |  | 0.963 |  |  |  |  |  | 0.953 |  |
| Satd. Flow (prot) | 0 | 1725 | 0 | 0 | 1735 | 0 | 0 | 0 | 0 | 0 | 1632 | 1583 |
| Flt Permitted |  |  |  |  | 0.963 |  |  |  |  |  | 0.953 |  |
| Satd. Flow (perm) | 0 | 1725 | 0 | 0 | 1735 | 0 | 0 | 0 | 0 | 0 | 1632 | 1583 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance ( t ) |  | 144 |  |  | 502 |  |  | 626 |  |  | 699 |  |
| Travel Time (s) |  | 3.3 |  |  | 11.4 |  |  | 14.2 |  |  | 15.9 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 23.3 |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 0 | 135 | 34 | 374 | 116 | 0 | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 0 | 9 | 0 | 5 | 7 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 0 | 135 | 34 | 374 | 116 | 0 | 0 | 0 | 0 |
| Major/Minor | Major1 |  |  | Major2 |  |  |  |  |  |
| Conflicting Flow All | 116 | 0 | 0 | 169 | 0 | 0 |  |  |  |
| Stage 1 | - | - | - | - | - | - |  |  |  |
| Stage 2 | - | - | - | - | - | - |  |  |  |
| Critical Hdwy | 4.1 | - | - | 4.15 | - | - |  |  |  |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |  |  |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |  |  |  |
| Follow-up Hdwy | 2.2 | - | - | 2.245 | - | - |  |  |  |
| Pot Cap-1 Maneuver | 1485 | - | - | 1390 | - | - |  |  |  |
| Stage 1 | - | - | - | - | - | - |  |  |  |
| Stage 2 | - | - | - | - | - | - |  |  |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1485 | - | - | 1390 | - | - |  |  |  |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |  |  |  |
| Stage 1 | - | - | - | - | - | - |  |  |  |
| Stage 2 | - | - | - | - | - | - |  |  |  |


| Approach | EB | WB |
| :--- | :---: | :---: |
| HCM Control Delay, s | 0 | 6.5 |
| HCM LOS |  |  |


| Minor Lane/Major Mvmt | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 | SBLn2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1485 | - | - | 1390 | - | - | 182 | 936 |
| HCM Lane V/C Ratio | - | - | - | 0.269 | - | - | 0.929 | 0.073 |
| HCM Control Delay (s) | 0 | - | - | 8.5 | 0 | - | 101 | 9.1 |
| HCM Lane LOS | A | - | - | A | A | - | F | A |
| HCM 95th \%tile Q(veh) | 0 | - | - | 1.1 | - | - | 7.2 | 0.2 |


| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | SBL | SBT | SBR |
| Vol, veh/h | 0 | 4 | 68 |
| Conflicting Peds, \#/hr | Stop | Stop | Stop |
| Sign Control | - | - | None |
| RT Channelized | - | - | 25 |
| Storage Length | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | 100 | 100 | 100 |
| Peak Hour Factor | 10 | 50 | 2 |
| Heavy Vehicles, \% | 165 | 4 | 68 |
| Mvmt Flow |  |  |  |
|  |  |  |  |


| Major/Minor | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Conflicting Flow All | 1016 | 1033 | 116 |
| $\quad$ Stage 1 | 864 | 864 | - |
| $\quad$ Stage 2 | 152 | 169 | - |
| Critical Hdwy | 6.5 | 7 | 6.22 |
| Critical Hdwy Stg 1 | 5.5 | 6 | - |
| Critical Hdwy Stg 2 | 5.5 | 6 | - |
| Follow-up Hdwy | 3.59 | 4.45 | 3.318 |
| Pot Cap-1 Maneuver | 255 | 192 | 936 |
| $\quad$ Stage 1 | 400 | 312 | - |
| $\quad$ Stage 2 | 857 | 676 | - |
| Platoon blocked, \% |  |  |  |
| Mov Cap-1 Maneuver | 182 | 0 | 936 |
| Mov Cap-2 Maneuver | 182 | 0 | - |
| Stage 1 | 285 | 0 | - |
| Stage 2 | 857 | 0 | - |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | 74.6 |
| HCM LOS | F |

## Minor Lane/Major Mvmt

|  | * | $\rightarrow$ | $\rangle$ | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | F |  |  | $\uparrow$ | 7 |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 50 | 0 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 0 |  | 1 | 0 |  | 0 |
| Taper Length (tt) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  |  |  |  | 0.971 |  |  |  | 0.850 |  |  |  |
| FIt Protected |  | 0.995 |  |  |  |  |  | 0.958 |  |  |  |  |
| Satd. Flow (prot) | 0 | 1741 | 0 | 0 | 1770 | 0 | 0 | 1630 | 1568 | 0 | 0 | 0 |
| Flt Permitted |  | 0.995 |  |  |  |  |  | 0.958 |  |  |  |  |
| Satd. Flow (perm) | 0 | 1741 | 0 | 0 | 1770 | 0 | 0 | 1630 | 1568 | 0 | 0 | 0 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance ( t ) |  | 502 |  |  | 143 |  |  | 542 |  |  | 648 |  |
| Travel Time (s) |  | 11.4 |  |  | 3.3 |  |  | 12.3 |  |  | 14.7 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |



| Major/Minor | Major1 |  | Major2 |  |  | Minor1 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 555 | 0 | 0 | 268 | 0 | 0 | 828 | 887 | 268 |
| Stage 1 | - | - | - | - | - | - | 332 | 332 |  |
| Stage 2 | - | - | - |  | - | - | 496 | 555 |  |
| Critical Hdwy | 4.15 | - | - | 4.1 | - | - | 6.46 | 7 | 6.23 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 5.46 | 6 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 5.46 | 6 |  |
| Follow-up Hdwy | 2.245 | - | - | 2.2 | - | - | 3.554 | 4.45 | 3.327 |
| Pot Cap-1 Maneuver | 1001 | - | - | 1307 | - | - | 336 | 237 | 768 |
| Stage 1 | - | - | - | - | - | - | 718 | 567 |  |
| Stage 2 | - | - | - | - | - | - | 604 | 443 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1001 | - | - | 1307 | - | - | 323 | 0 | 768 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 323 | 0 |  |
| Stage 1 | - | - | - | - | - | - | 691 | 0 |  |
| Stage 2 | - | - | - | - | - | - | 604 | 0 |  |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0.9 | 0 | 23.1 |
| HCM LOS |  |  | $C$ |


| Minor Lane/Major Mvmt | NBLn1 | NBLn2 | EBL | EBT | EBR | WBL | WBT | WBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 323 | 768 | 1001 | - | - | 1307 | - | - |
| HCM Lane V/C Ratio | 0.192 | 0.77 | 0.032 | - | - | - | - | - |
| HCM Control Delay (s) | 18.8 | 23.5 | 8.7 | 0 | - | 0 | - | - |
| HCM Lane LOS | C | C | A | A | - | A | - | - |
| HCM 95th \%tile Q(veh) | 0.7 | 7.5 | 0.1 | - | - | 0 | - | - |


| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | SBL | SBT | SBR |
| Vol, veh/h | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | - | - | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 |
| Heavy Vehicles, \% | 0 | 0 | 0 |
| Mvmt Flow | 0 | 0 | 0 |


| Major/Minor |
| :--- |
| Conflicting Flow All |
| $\quad$ Stage 1 |
| $\quad$ Stage 2 |
| Critical Hdwy |
| Critical Hdwy Stg 1 |
| Critical Hdwy Stg 2 |
| Follow-up Hdwy |
| Pot Cap-1 Maneuver |
| $\quad$ Stage 1 |
| $\quad$ Stage 2 |
| Platoon blocked, \% |
| Mov Cap-1 Maneuver |
| Mov Cap-2 Maneuver |
| Stage 1 |
| Stage 2 |

## Approach

HCM Control Delay, s
HCM LOS

## Minor Lane/Major Mvmt

|  | $\rangle$ | $\rightarrow$ | $\rangle$ | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | F |  |  | ¢ |  |  | ${ }_{4}$ |  |  | ${ }_{\dagger}$ |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length ( t ) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  | 0.998 |  |  | 0.998 |  |  | 0.932 |  |  | 0.879 |  |
| Flt Protected | 0.950 |  |  |  | 0.999 |  |  | 0.976 |  |  | 0.997 |  |
| Satd. Flow (prot) | 1308 | 1818 | 0 | 0 | 1829 | 0 | 0 | 1728 | 0 | 0 | 1381 | 0 |
| Flt Permitted | 0.950 |  |  |  | 0.999 |  |  | 0.976 |  |  | 0.997 |  |
| Satd. Flow (perm) | 1308 | 1818 | 0 | 0 | 1829 | 0 | 0 | 1728 | 0 | 0 | 1381 | 0 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance ( t ) |  | 143 |  |  | 173 |  |  | 583 |  |  | 174 |  |
| Travel Time (s) |  | 3.3 |  |  | 3.9 |  |  | 13.3 |  |  | 4.0 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type:

Other

| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 1.8 |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 32 | 815 | 12 | 5 | 448 | 8 | 5 | 0 | 5 |
| Conflicting Peds, \#hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | 0 | - | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 38 | 4 | 25 | 25 | 2 | 77 | 0 | 0 | 0 |
| Mvmt Flow | 32 | 815 | 12 | 5 | 448 | 8 | 5 | 0 | 5 |
| Major/Minor | Major1 |  |  | Major2 |  |  | Minor1 |  |  |
| Conflicting Flow All | 456 | 0 | 0 | 827 | 0 | 0 | 1401 | 1351 | 821 |
| Stage 1 | - | - | - | - | - | - | 885 | 885 |  |
| Stage 2 | - | - | - | - | - | - | 516 | 466 |  |
| Critical Hdwy | 4.48 | - | - | 4.35 | - | - | 7.1 | 6.5 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.5 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.1 | 5.5 |  |
| Follow-up Hdwy | 2.542 | - | - | 2.425 | - | - | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 939 | - | - | 713 | - | - | 119 | 152 | 378 |
| Stage 1 | - | - | - | - | - | - | 342 | 366 | - |
| Stage 2 | - | - | - | - | - | - | 546 | 566 | - |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 939 | - | - | 713 | - | - | 92 | 145 | 378 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 92 | 145 |  |
| Stage 1 | - | - | - | - | - | - | 330 | 354 |  |
| Stage 2 | - | - | - | - | - | - | 439 | 561 |  |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0.3 | 0.1 | 31.1 |
| HCM LOS |  |  | D |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 148 | 939 | - | - | 713 | - | - | 419 |
| HCM Lane V/C Ratio | 0.068 | 0.034 | - | - | 0.007 | - | - | 0.274 |
| HCM Control Delay (s) | 31.1 | 9 | - | - | 10.1 | 0 | - | 16.8 |
| HCM Lane LOS | D | A | - | - | B | A | - | C |
| HCM 95th \%tile Q(veh) | 0.2 | 0.1 | - | - | 0 | - | - | 1.1 |


| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | 8 | 4 | 103 |
| Vol, veh/h | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | Stop | Stop | Stop |
| Sign Control | - | - | None |
| RT Channelized | - | - | - |
| Storage Length | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | 100 | 100 | 100 |
| Peak Hour Factor | 0 | 0 | 23 |
| Heavy Vehicles, \% | 8 | 4 | 103 |
| Mvmt Flow |  |  |  |
|  |  |  |  |


| Major/Minor | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Conflicting Flow All | 1350 | 1353 | 452 |
| $\quad$ Stage 1 | 462 | 462 | - |
| $\quad$ Stage 2 | 888 | 891 | - |
| Critical Hdwy | 7.1 | 6.5 | 6.43 |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - |
| Follow-up Hdwy | 3.5 | 4 | 3.507 |
| Pot Cap-1 Maneuver | 129 | 151 | 566 |
| $\quad$ Stage 1 | 584 | 568 | - |
| $\quad$ Stage 2 | 341 | 363 | - |
| Platoon blocked, \% |  |  |  |
| Mov Cap-1 Maneuver | 123 | 145 | 566 |
| Mov Cap-2 Maneuver | 123 | 145 | - |
| Stage 1 | 564 | 563 | - |
| Stage 2 | 325 | 351 | - |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | 16.8 |
| HCM LOS | C |

## Minor Lane/Major Mvmt




| Major/Minor | Major1 | Major2 |  |  | Minor1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 84 | 0 | 301 | 77 |
| Stage 1 | - | - | - | - | 77 | - |
| Stage 2 | - | - | - | - | 224 | - |
| Critical Hdwy | - | - | 4.16 | - | 6.65 | 6.24 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.65 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.65 | - |
| Follow-up Hdwy | - | - | 2.254 | - | 3.725 | 3.336 |
| Pot Cap-1 Maneuver | - | - | 1488 | - | 645 | 978 |
| Stage 1 | - | - | - | - | 891 |  |
| Stage 2 | - | - | - | - | 762 |  |
| Platoon blocked, \% | - | - |  | - |  |  |
| Mov Cap-1 Maneuver | - | - | 1488 | - | 610 | 978 |
| Mov Cap-2 Maneuver | - | - | - | - | 610 |  |
| Stage 1 | - | - | - | - | 891 |  |
| Stage 2 | - | - | - | - | 721 |  |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 4 | 9.2 |
| HCM LOS |  |  | A |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 938 | - | - | 1488 | - |
| HCM Lane V/C Ratio | 0.076 | - | - | 0.052 | - |
| HCM Control Delay (s) | 9.2 | - | - | 7.6 | 0 |
| HCM Lane LOS | A | - | - | A | A |
| HCM 95th \%tile Q(veh) | 0.2 | - | - | 0.2 | - |


|  | $\Rightarrow$ | $\rightarrow$ | $\geqslant$ | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | F |  |  | $\uparrow$ |  |  |  |  |  | $\uparrow$ | F |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 25 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 1 |
| Taper Length (tt) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Fit |  | 0.958 |  |  |  |  |  |  |  |  |  | 0.850 |
| Flt Protected |  |  |  |  | 0.959 |  |  |  |  |  | 0.953 |  |
| Satd. Flow (prot) | 0 | 1698 | 0 | 0 | 1773 | 0 | 0 | 0 | 0 | 0 | 1743 | 1429 |
| Flt Permitted |  |  |  |  | 0.959 |  |  |  |  |  | 0.953 |  |
| Satd. Flow (perm) | 0 | 1698 | 0 | 0 | 1773 | 0 | 0 | 0 | 0 | 0 | 1743 | 1429 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance ( t ) |  | 144 |  |  | 502 |  |  | 626 |  |  | 699 |  |
| Travel Time (s) |  | 3.3 |  |  | 11.4 |  |  | 14.2 |  |  | 15.9 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 18.1 |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 0 | 93 | 42 | 365 | 66 | 0 | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 0 | 5 | 12 | 2 | 7 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 0 | 93 | 42 | 365 | 66 | 0 | 0 | 0 | 0 |
| Major/Minor | Major1 |  |  | Major2 |  |  |  |  |  |
| Conflicting Flow All | 66 | 0 | 0 | 135 | 0 | 0 |  |  |  |
| Stage 1 | - | - | - | - | - | - |  |  |  |
| Stage 2 | - | - | - | - | - | - |  |  |  |
| Critical Hdwy | 4.1 | - | - | 4.12 | - | - |  |  |  |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |  |  |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |  |  |  |
| Follow-up Hdwy | 2.2 | - | - | 2.218 | - | - |  |  |  |
| Pot Cap-1 Maneuver | 1549 | - | - | 1449 | - | - |  |  |  |
| Stage 1 | - | - | - | - | - | - |  |  |  |
| Stage 2 | - | - | - | - | - | - |  |  |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1549 | - | - | 1449 | - | - |  |  |  |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |  |  |  |
| Stage 1 | - | - | - | - | - | - |  |  |  |
| Stage 2 | - | - | - | - | - | - |  |  |  |


| Approach | EB | WB |
| :--- | :---: | :---: |
| HCM Control Delay, s | 0 | 7 |
| HCM LOS |  |  |


| Minor Lane/Major Mvmt | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 | SBLn2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1549 | - | - | 1449 | - | - | 223 | 968 |
| HCM Lane V/C Ratio | - | - | - | 0.252 | - | - | 0.789 | 0.084 |
| HCM Control Delay (s) | 0 | - | - | 8.3 | 0 | - | 63.1 | 9.1 |
| HCM Lane LOS | A | - | - | A | A | - | F | A |
| HCM 95th \%tile Q(veh) | 0 | - | - | 1 | - | - | 5.7 | 0.3 |


| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | SBL | SBT | SBR |
| Vol, veh/h | 0 | 4 | 81 |
| Conflicting Peds, \#/hr | Stop | Stop | Stop |
| Sign Control | - | - | None |
| RT Channelized | - | - | 25 |
| Storage Length | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | 100 | 100 | 100 |
| Peak Hour Factor | 4 | 0 | 13 |
| Heavy Vehicles, \% | 172 | 4 | 81 |
| Mvmt Flow |  |  |  |


|  | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Major/Minor | 910 | 931 | 66 |
| Conflicting Flow All | 796 | 796 | - |
| Stage 1 | 114 | 135 | - |
| Stage 2 | 6.44 | 6.5 | 6.33 |
| Critical Hdwy | 5.44 | 5.5 | - |
| Critical Hdwy Stg 1 | 5.44 | 5.5 | - |
| Critical Hdwy Stg 2 | 3.536 | 4 | 3.417 |
| Follow-up Hdwy | 302 | 269 | 968 |
| Pot Cap-1 Maneuver | 441 | 402 | - |
| Stage 1 | 906 | 789 | - |
| Stage 2 |  |  |  |
| Platoon blocked, \% | 223 | 0 | 968 |
| Mov Cap-1 Maneuver | 223 | 0 | - |
| Mov Cap-2 Maneuver | 326 | 0 | - |
| Stage 1 | 906 | 0 | - |
| Stage 2 |  |  |  |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | 46.1 |
| HCM LOS | E |

## Minor Lane/Major Mvmt

|  | * | $\rightarrow$ | $\rangle$ | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | F |  |  | $\uparrow$ | 7 |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 50 | 0 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 0 |  | 1 | 0 |  | 0 |
| Taper Length (tt) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  |  |  |  | 0.969 |  |  |  | 0.850 |  |  |  |
| FIt Protected |  | 0.994 |  |  |  |  |  | 0.960 |  |  |  |  |
| Satd. Flow (prot) | 0 | 1810 | 0 | 0 | 1752 | 0 | 0 | 1765 | 1568 | 0 | 0 | 0 |
| Flt Permitted |  | 0.994 |  |  |  |  |  | 0.960 |  |  |  |  |
| Satd. Flow (perm) | 0 | 1810 | 0 | 0 | 1752 | 0 | 0 | 1765 | 1568 | 0 | 0 | 0 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance ( t ) |  | 502 |  |  | 143 |  |  | 542 |  |  | 648 |  |
| Travel Time (s) |  | 11.4 |  |  | 3.3 |  |  | 12.3 |  |  | 14.7 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 8.3 |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 34 | 231 | 0 | 0 | 410 | 124 | 21 | 4 | 564 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | 50 |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 0 | 5 | 0 | 0 | 3 | 12 | 4 | 0 | 3 |
| Mvmt Flow | 34 | 231 | 0 | 0 | 410 | 124 | 21 | 4 | 564 |


| Major/Minor | Major1 |  | Major2 |  |  | Minor1 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 534 | 0 | 0 | 231 | 0 | 0 | 771 | 833 | 231 |
| Stage 1 | - | - | - | - | - | - | 299 | 299 |  |
| Stage 2 | - | - | - | - | - | - | 472 | 534 |  |
| Critical Hdwy | 4.1 | - | - | 4.1 | - | - | 6.44 | 6.5 | 6.23 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 5.44 | 5.5 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 5.44 | 5.5 |  |
| Follow-up Hdwy | 2.2 | - | - | 2.2 | - | - | 3.536 | 4 | 3.327 |
| Pot Cap-1 Maneuver | 1044 | - | - | 1349 | - | - | 366 | 307 | 806 |
| Stage 1 | - | - | - | - | - | - | 748 | 670 |  |
| Stage 2 | - | - | - | - | - | - | 623 | 528 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1044 | - | - | 1349 | - | - | 352 | 0 | 806 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 352 | 0 |  |
| Stage 1 | - | - | - | - | - | - | 720 | 0 |  |
| Stage 2 | - | - | - | - | - | - | 623 | 0 |  |


| Approach | EB | WB | NB |
| :--- | :---: | ---: | :---: |
| HCM Control Delay, s | 1.1 | 0 | 19.1 |
| HCM LOS |  |  | $C$ |


| Minor Lane/Major Mvmt | NBLn1 | NBLn2 | EBL | EBT | EBR | WBL | WBT | WBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 352 | 806 | 1044 | - | - | 1349 | - | - |
| HCM Lane V/C Ratio | 0.071 | 0.7 | 0.033 | - | - | - | - | - |
| HCM Control Delay (s) | 16 | 19.2 | 8.6 | 0 | - | 0 | - | - |
| HCM Lane LOS | C | C | A | A | - | A | - | - |
| HCM 95th \%tile Q(veh) | 0.2 | 5.9 | 0.1 | - | - | 0 | - | - |


| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | SBL | SBT | SBR |
| Vol, veh/h | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | - | - | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 |
| Heavy Vehicles, \% | 0 | 0 | 0 |
| Mvmt Flow | 0 | 0 | 0 |


| Major/Minor |
| :--- |
| Conflicting Flow All |
| $\quad$ Stage 1 |
| $\quad$ Stage 2 |
| Critical Hdwy |
| Critical Hdwy Stg 1 |
| Critical Hdwy Stg 2 |
| Follow-up Hdwy |
| Pot Cap-1 Maneuver |
| $\quad$ Stage 1 |
| $\quad$ Stage 2 |
| Platoon blocked, \% |
| Mov Cap-1 Maneuver |
| Mov Cap-2 Maneuver |
| Stage 1 |
| Stage 2 |

## Approach

HCM Control Delay, s
HCMLOS

## Minor Lane/Major Mvmt

|  | $\rangle$ | $\rightarrow$ | 7 | $\downarrow$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | F |  |  | ¢ |  |  | $\dagger$ |  |  | ${ }_{\text {¢ }}$ |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Fit |  | 0.999 |  |  | 0.998 |  |  | 0.966 |  |  | 0.884 |  |
| Flt Protected | 0.950 |  |  |  | 0.999 |  |  | 0.976 |  |  | 0.995 |  |
| Satd. Flow (prot) | 1570 | 1824 | 0 | 0 | 1819 | 0 | 0 | 1518 | 0 | 0 | 1458 | 0 |
| Flt Permitted | 0.950 |  |  |  | 0.999 |  |  | 0.976 |  |  | 0.995 |  |
| Satd. Flow (perm) | 1570 | 1824 | 0 | 0 | 1819 | 0 | 0 | 1518 | 0 | 0 | 1458 | 0 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 143 |  |  | 173 |  |  | 583 |  |  | 174 |  |
| Travel Time (s) |  | 3.3 |  |  | 3.9 |  |  | 13.3 |  |  | 4.0 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type:

Other

| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 2.1 |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 16 | 774 | 5 | 5 | 421 | 8 | 10 | 5 | 5 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | 0 | - | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 15 | 4 | 17 | 0 | 3 | 67 | 11 | 0 | 50 |
| Mvmt Flow | 16 | 774 | 5 | 5 | 421 | 8 | 10 | 5 | 5 |
| Major/Minor | Major1 |  |  | Major2 |  |  | Minor1 |  |  |
| Conflicting Flow All | 429 | 0 | 0 | 779 | 0 | 0 | 1298 | 1248 | 777 |
| Stage 1 | - | - | - | - | - | - | 809 | 809 |  |
| Stage 2 | - | - | - | - | - | - | 489 | 439 |  |
| Critical Hdwy | 4.25 | - | - | 4.1 | - | - | 7.21 | 6.5 | 6.7 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.21 | 5.5 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.21 | 5.5 |  |
| Follow-up Hdwy | 2.335 | - | - | 2.2 | - | - | 3.599 | 4 | 3.75 |
| Pot Cap-1 Maneuver | 1064 | - | - | 847 | - | - | 133 | 175 | 330 |
| Stage 1 | - | - | - | - | - | - | 361 | 396 | - |
| Stage 2 | - | - | - | - | - | - | 544 | 582 | - |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1064 | - | - | 847 | - | - | 106 | 171 | 330 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 106 | 171 |  |
| Stage 1 | - | - | - | - | - | - | 356 | 390 |  |
|  |  | - | - | - | - | - | 444 | 577 |  |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0.2 | 0.1 | 34 |
| HCM LOS |  |  | D |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 144 | 1064 | - | - | 847 | - | - | 419 |
| HCM Lane V/C Ratio | 0.139 | 0.015 | - | - | 0.006 | - | - | 0.286 |
| HCM Control Delay (s) | 34 | 8.4 | - | - | 9.3 | 0 | - | 17 |
| HCM Lane LOS | D | A | - | - | A | A | - | C |
| HCM 95th \%tile Q(veh) | 0.5 | 0 | - | - | 0 | - | - | 1.2 |


| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | SBL | SBT | SBR |
| Vol, veh/h | 13 | 4 | 103 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | - | - | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 |
| Heavy Vehicles, \% | 0 | 0 | 17 |
| Mvmt Flow | 13 | 4 | 103 |
|  |  |  |  |


| Major/Minor | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Conflicting Flow All | 1249 | 1246 | 425 |
| $\quad$ Stage 1 | 435 | 435 | - |
| $\quad$ Stage 2 | 814 | 811 | - |
| Critical Hdwy | 7.1 | 6.5 | 6.37 |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - |
| Follow-up Hdwy | 3.5 | 4 | 3.453 |
| Pot Cap-1 Maneuver | 151 | 175 | 598 |
| $\quad$ Stage 1 | 604 | 584 | - |
| $\quad$ Stage 2 | 375 | 396 | - |
| Platoon blocked, \% |  |  |  |
| Mov Cap-1 Maneuver | 143 | 171 | 598 |
| Mov Cap-2 Maneuver | 143 | 171 | - |
| Stage 1 | 595 | 579 | - |
| Stage 2 | 359 | 390 | - |


| Approach | SB |
| :--- | :---: |
| HCM Control Delay, s | 17 |
| HCM LOS | C |

[^18]
## Appendix R 2017 Total Traffic Conditions Worksheets - Freeway Mainline







## BASIC FREEWAY SEGMENTS WORKSHEET

| BASIC FREEWAY SEGMENTS WORKSHEET |  |  |  |
| :---: | :---: | :---: | :---: |
| General Information |  | Site Information |  |
| Analyst <br> Agency or Company <br> Date Performed <br> Analysis Time Period | $\begin{aligned} & \text { KML } \\ & \text { KAI } \\ & 6 / 25 / 2014 \\ & \text { Weekday PM Peak Period } \end{aligned}$ | Highway/Direction of Tra <br> From/To <br> Jurisdiction <br> Analysis Year | I-5 SB <br> SR 501 to La Center <br> WSDOT <br> 2017_casino |
| Project Description 12393 |  |  |  |
| $\checkmark$ Oper.(LOS) |  | es.(N) | $\square$ Planning Data |
| Flow Inputs |  |  |  |
| Volume, V <br> AADT <br> Peak-Hr Prop. of AADT, K <br> Peak-Hr Direction Prop, D $\text { DDHV }=\text { AADT } \times K \times D$ | 3516 veh/h veh/day | Peak-Hour Factor, PHF \%Trucks and Buses, $\mathrm{P}_{\mathrm{T}}$ \%RVs, $\mathrm{P}_{\mathrm{R}}$ General Terrain: | $\begin{aligned} & 1.00 \\ & 13 \\ & 0 \\ & \text { Level } \end{aligned}$ |








## Appendix S 2017 Total Traffic Conditions Worksheets - Merge/Diverge Locations




















# Appendix T 2017 Total Traffic Conditions (Build) Worksheets Northbound Off-Ramp Diverge 





## Appendix U 2017 Total Traffic Conditions (No Build) Worksheets - Study Intersections

|  | $\dagger$ | $\rightarrow$ | $\leftarrow$ | 4 | $\checkmark$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\uparrow$ | $\stackrel{\text { F }}{ }$ |  | Y |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% | 0\% |  | 0\% |  |
| Storage Length (ft) | 100 |  |  | 0 | 0 | 0 |
| Storage Lanes | 0 |  |  | 0 | 1 | 0 |
| Taper Length (ft) | 25 |  |  |  | 25 |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |
| Frt |  |  | 0.900 |  | 0.999 |  |
| Flt Protected |  | 0.998 |  |  | 0.953 |  |
| Satd. Flow (prot) | 0 | 1825 | 1647 | 0 | 1791 | 0 |
| Flt Permitted |  | 0.998 |  |  | 0.953 |  |
| Satd. Flow (perm) | 0 | 1825 | 1647 | 0 | 1791 | 0 |
| Link Speed (mph) |  | 30 | 30 |  | 30 |  |
| Link Distance (ft) |  | 909 | 1364 |  | 495 |  |
| Travel Time (s) |  | 20.7 | 31.0 |  | 11.3 |  |
| Intersection Summary |  |  |  |  |  |  |

Area Type:

Other


| Approach | EB | WB | SB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0.2 | 0 | 10.2 |
| HCM LOS |  |  | B |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1382 | - | - | - | 803 |
| HCM Lane V/C Ratio | 0.001 | - | - | - | 0.138 |
| HCM Control Delay (s) | 7.6 | 0 | - | - | 10.2 |
| HCM Lane LOS | A | A | - | - | B |
| HCM 95th \%tile Q(veh) | 0 | - | - | - | 0.5 |


|  | $\stackrel{ }{\prime}$ | $\rightarrow$ | $\geqslant$ | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | P | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | F |  | \% | $\stackrel{\text { F }}{ }$ |  |  | ¢ |  | 7 | F |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 150 |  | 0 | 0 |  | 0 | 0 |  | 0 | 200 |  | 0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 0 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Fit |  | 0.987 |  |  | 0.935 |  |  | 0.880 |  |  |  |  |
| Flt Protected |  |  |  | 0.950 |  |  |  | 0.997 |  | 0.950 |  |  |
| Satd. Flow (prot) | 1900 | 1809 | 0 | 1626 | 1749 | 0 | 0 | 1384 | 0 | 1787 | 1881 | 0 |
| Flt Permitted |  |  |  | 0.950 |  |  |  | 0.997 |  | 0.950 |  |  |
| Satd. Flow (perm) | 1900 | 1809 | 0 | 1626 | 1749 | 0 | 0 | 1384 | 0 | 1787 | 1881 | 0 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 1364 |  |  | 144 |  |  | 957 |  |  | 354 |  |
| Travel Time (s) |  | 31.0 |  |  | 3.3 |  |  | 21.8 |  |  | 8.0 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |



| Major/Minor | Major1 |  | Major2 |  |  | Minor1 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 338 | 0 | 0 | 170 | 0 | 0 | 529 | 599 | 163 |
| Stage 1 | - | - | - | - | - | - | 163 | 163 |  |
| Stage 2 | - | - | - | - | - | - | 366 | 436 |  |
| Critical Hdwy | 4.1 | - | - | 4.21 | - | - | 7.1 | 6.51 | 6.43 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.51 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.1 | 5.51 |  |
| Follow-up Hdwy | 2.2 | - | - | 2.299 | - | - | 3.5 | 4.009 | 3.507 |
| Pot Cap-1 Maneuver | 1232 | - | - | 1355 | - | - | 463 | 417 | 830 |
| Stage 1 | - | - | - | - | - | - | 844 | 765 |  |
| Stage 2 | - | - | - | - | - | - | 657 | 582 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1232 | - | - | 1355 | - | - | 446 | 402 | 830 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 446 | 402 |  |
| Stage 1 | - | - | - | - | - | - | 844 | 765 | - |
| Stage 2 | - | - | - | - | - | - | 628 | 561 |  |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0 | 1 | 10.5 |
| HCM LOS |  |  | B |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 | SBLn2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 748 | 1232 | - | - | 1355 | - | - | 380 | 438 |
| HCM Lane V/C Ratio | 0.118 | - | - | - | 0.036 | - | - | 0.289 | 0.011 |
| HCM Control Delay (s) | 10.5 | 0 | - | - | 7.8 | - | - | 18.3 | 13.3 |
| HCM Lane LOS | B | A | - | - | A | - | - | C | B |
| HCM 95th \%tile Q(veh) | 0.4 | 0 | - | - | 0.1 | - | - | 1.2 | 0 |


| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | SBL | SBT | SBR |
| Vol, veh/h | 0 | 5 | 0 |
| Conflicting Peds, \#/hr | Stop | Stop | Stop |
| Sign Control | - | - | None |
| RT Channelized | 200 | - | - |
| Storage Length | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | 100 | 100 | 100 |
| Peak Hour Factor | 1 | 1 | 1 |
| Heavy Vehicles, \% | 110 | 5 | 0 |
| Mvmt Flow |  |  |  |


| Major/Minor | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Conflicting Flow All | 567 | 533 | 265 |
| Stage 1 | 363 | 363 | - |
| Stage 2 | 204 | 170 | - |
| Critical Hdwy | 7.11 | 6.51 | 6.21 |
| Critical Hdwy Stg 1 | 6.11 | 5.51 | - |
| Critical Hdwy Stg 2 | 6.11 | 5.51 | - |
| Follow-up Hdwy | 3.509 | 4.009 | 3.309 |
| Pot Cap-1 Maneuver | 436 | 454 | 776 |
| $\quad$ Stage 1 | 658 | 626 | - |
| Stage 2 | 800 | 760 | - |
| Platoon blocked, \% |  |  |  |
| Mov Cap-1 Maneuver | 380 | 438 | 776 |
| Mov Cap-2 Maneuver | 380 | 438 | - |
| Stage 1 | 658 | 603 | - |
| Stage 2 | 720 | 760 | - |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | 18.1 |
| HCM LOS | C |

[^19]|  | $\Rightarrow$ | $\rightarrow$ | $\geqslant$ | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $P$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | F |  |  | $\uparrow$ |  |  |  |  |  | $\uparrow$ | F |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 25 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 1 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  | 0.911 |  |  |  |  |  |  |  |  |  | 0.850 |
| Flt Protected |  |  |  |  | 0.971 |  |  |  |  |  | 0.954 |  |
| Satd. Flow (prot) | 0 | 1600 | 0 | 0 | 1788 | 0 | 0 | 0 | 0 | 0 | 1587 | 1495 |
| Flt Permitted |  |  |  |  | 0.971 |  |  |  |  |  | 0.954 |  |
| Satd. Flow (perm) | 0 | 1600 | 0 | 0 | 1788 | 0 | 0 | 0 | 0 | 0 | 1587 | 1495 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 144 |  |  | 502 |  |  | 626 |  |  | 699 |  |
| Travel Time (s) |  | 3.3 |  |  | 11.4 |  |  | 14.2 |  |  | 15.9 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 89.2 |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 0 | 118 | 225 | 535 | 361 | 0 | 0 | 0 | 0 |
| Conflicting Peds, \#hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - |  |  |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 0 | 20 | 2 | 4 | 2 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 0 | 118 | 225 | 535 | 361 | 0 | 0 | 0 | 0 |
| Major/Minor | Major1 |  |  | Major2 |  |  |  |  |  |
| Conflicting Flow All | 361 | 0 | 0 | 343 | 0 | 0 |  |  |  |
| Stage 1 | - | - | - | - | - | - |  |  |  |
| Stage 2 | - | - | - | - | - | - |  |  |  |
| Critical Hdwy | 4.1 | - | - | 4.14 | - | - |  |  |  |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |  |  |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |  |  |  |
| Follow-up Hdwy | 2.2 | - | - | 2.236 | - | - |  |  |  |
| Pot Cap-1 Maneuver | 1209 | - | - | 1205 | - | - |  |  |  |
| Stage 1 | - | - | - | - | - | - |  |  |  |
| Stage 2 | - | - | - | - | - | - |  |  |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1209 | - | - | 1205 | - | - |  |  |  |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |  |  |  |
| Stage 1 | - | - | - | - | - | - |  |  |  |
| Stage 2 | - | - | - | - | - | - |  |  |  |


| Approach | EB | WB |
| :--- | :---: | :---: |
| HCM Control Delay, s | 0 | 6.2 |
| HCM LOS |  |  |


| Minor Lane/Major Mvmt | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 | SBLn2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1209 | - | - | 1205 | - | - | 45 | 670 |
| HCM Lane V/C Ratio | - | - | - | 0.444 | - | - | 2.711 | 0.037 |
| HCM Control Delay (s) | 0 | - | - | 10.4 | 0 | $-\$ 965.8$ | 10.6 |  |
| HCM Lane LOS | A | - | - | $B$ | A | - | F | B |
| HCM 95th \%tile Q(veh) | 0 | - | - | 2.3 | - | - | 13.1 | 0.1 |

## Notes

~: Volume exceeds capacity $\quad \$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ *: All major volume in platoon

| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
|  | SBL | SBT | SBR |
| Movement | 118 | 4 | 25 |
| Vol, veh/h | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | Stop | Stop | Stop |
| Sign Control | - | - | None |
| RT Channelized | - | - | 25 |
| Storage Length | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | 100 | 100 | 100 |
| Peak Hour Factor | 13 | 50 | 8 |
| Heavy Vehicles, \% | 118 | 4 | 25 |
| Mvmt Flow |  |  |  |
|  |  |  |  |


| Major/Minor | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Conflicting Flow All | 1662 | 1774 | 361 |
| $\quad$ Stage 1 | 1431 | 1431 | - |
| $\quad$ Stage 2 | 231 | 343 | - |
| Critical Hdwy | 6.53 | 7 | 6.28 |
| Critical Hdwy Stg 1 | 5.53 | 6 | - |
| Critical Hdwy Stg 2 | 5.53 | 6 | - |
| Follow-up Hdwy | 3.617 | 4.45 | 3.372 |
| Pot Cap-1 Maneuver | $\sim 100$ | 63 | 670 |
| $\quad$ Stage 1 | 208 | 159 | - |
| $\quad 782$ | 560 | - |  |
| Stage 2 |  |  |  |
| Platoon blocked, \% | $\sim 45$ | 0 | 670 |
| Mov Cap-1 Maneuver | $\sim 45$ | 0 | - |
| Mov Cap-2 Maneuver | $\sim 93$ | 0 | - |
| Stage 1 | 782 | 0 | - |
| Stage 2 |  |  |  |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | $\$ 803.4$ |
| HCM LOS | F |

[^20]|  | * | $\rightarrow$ | $\rangle$ | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | F |  |  | $\uparrow$ | 7 |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 50 | 0 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 0 |  | 1 | 0 |  | 0 |
| Taper Length (tt) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  |  |  |  | 0.972 |  |  |  | 0.850 |  |  |  |
| FIt Protected |  | 0.984 |  |  |  |  |  | 0.953 |  |  |  |  |
| Satd. Flow (prot) | 0 | 1598 | 0 | 0 | 1731 | 0 | 0 | 1781 | 1509 | 0 | 0 | 0 |
| Flt Permitted |  | 0.984 |  |  |  |  |  | 0.953 |  |  |  |  |
| Satd. Flow (perm) | 0 | 1598 | 0 | 0 | 1731 | 0 | 0 | 1781 | 1509 | 0 | 0 | 0 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance ( t ) |  | 502 |  |  | 143 |  |  | 542 |  |  | 648 |  |
| Travel Time (s) |  | 11.4 |  |  | 3.3 |  |  | 12.3 |  |  | 14.7 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 33.9 |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 77 | 159 | 0 | 0 | 604 | 156 | 292 | 4 | 321 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None |  |  | None | - | - | None |
| Storage Length | - | - | - |  |  | - | - |  | 50 |
| Veh in Median Storage, \# | - | 0 | - |  | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 17 | 17 | 0 | 0 | 4 | 17 | 1 | 50 | 7 |
| Mvmt Flow | 77 | 159 | 0 | 0 | 604 | 156 | 292 | 4 | 321 |
| Major/Minor | Major1 |  |  | Major2 |  |  | Minor1 |  |  |
| Conflicting Flow All | 760 | 0 | 0 | 159 | 0 | 0 | 995 | 1073 | 159 |
| Stage 1 | - | - | - | - | - | - | 313 | 313 |  |
| Stage 2 | - | - | - | - |  | - | 682 | 760 |  |
| Critical Hdwy | 4.27 | - | - | 4.1 |  | - | 6.41 | 7 | 6.27 |
| Critical Hdwy Stg 1 | - | - | - |  |  | - | 5.41 | 6 |  |
| Critical Hdwy Stg 2 | - | - | - | - |  | - | 5.41 | 6 |  |
| Follow-up Hdwy | 2.353 | - | - | 2.2 | - | - | 3.509 | 4.45 | 3.363 |
| Pot Cap-1 Maneuver | 788 | - | - | 1433 | - | - | $\sim 273$ | 181 | 873 |
| Stage 1 | - | - | - | - |  | - | 744 | 579 |  |
| Stage 2 | - | - | - | - |  | - | 504 | 352 |  |
| Platoon blocked, \% |  | - | - |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 788 | - | - | 1433 |  | - | $\sim 244$ | 0 | 873 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | $\sim 244$ | 0 |  |
| Stage 1 | - | - | - | - | - | - | 664 | 0 |  |
| Stage 2 | - | - | - | - | - | - | 504 | 0 |  |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 3.3 | 0 | 87.3 |
| HCM LOS |  |  | F |


| Minor Lane/Major Mvmt | NBLn1 | NBLn2 | EBL | EBT | EBR | WBL | WBT | WBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 244 | 873 | 788 | - | - | 1433 | - | - |
| HCM Lane V/C Ratio | 1.213 | 0.368 | 0.098 | - | - | - | - | - |
| HCM Control Delay (s) | 169.5 | 11.5 | 10.1 | 0 | - | 0 | - | - |
| HCM Lane LOS | F | B | B | A | - | A | - | - |
| HCM 95th \%tile Q(veh) | 14.3 | 1.7 | 0.3 | - | - | 0 | - | - |

Notes
~: Volume exceeds capacity $\quad \$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ *: All major volume in platoon

| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | SBL | SBT | SBR |
| Vol, veh/h | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | - | - | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 |
| Heavy Vehicles, \% | 0 | 0 | 0 |
| Mvmt Flow | 0 | 0 | 0 |


| Major/Minor |
| :--- |
| Conflicting Flow All |
| $\quad$ Stage 1 |
| $\quad$ Stage 2 |
| Critical Hdwy |
| Critical Hdwy Stg 1 |
| Critical Hdwy Stg 2 |
| Follow-up Hdwy |
| Pot Cap-1 Maneuver |
| $\quad$ Stage 1 |
| $\quad$ Stage 2 |
| Platoon blocked, \% |
| Mov Cap-1 Maneuver |
| Mov Cap-2 Maneuver |
| Stage 1 |
| Stage 2 |

## Approach

HCM Control Delay, s
HCMLOS

## Minor Lane/Major Mvmt

|  | $\rangle$ | $\rightarrow$ | $\rangle$ | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | F |  |  | ¢ |  |  | ${ }_{4}$ |  |  | ${ }_{\dagger}$ |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length ( t ) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  | 0.999 |  |  | 0.998 |  |  | 0.958 |  |  | 0.896 |  |
| Flt Protected | 0.950 |  |  |  | 0.999 |  |  | 0.967 |  |  | 0.990 |  |
| Satd. Flow (prot) | 1150 | 1727 | 0 | 0 | 1818 | 0 | 0 | 1499 | 0 | 0 | 1399 | 0 |
| Flt Permitted | 0.950 |  |  |  | 0.999 |  |  | 0.967 |  |  | 0.990 |  |
| Satd. Flow (perm) | 1150 | 1727 | 0 | 0 | 1818 | 0 | 0 | 1499 | 0 | 0 | 1399 | 0 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance ( t ) |  | 143 |  |  | 173 |  |  | 583 |  |  | 174 |  |
| Travel Time (s) |  | 3.3 |  |  | 3.9 |  |  | 13.3 |  |  | 4.0 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type:

Other

| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 3.9 |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 30 | 445 | 4 | 9 | 636 | 9 | 9 | 0 | 4 |
| Conflicting Peds, \#hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | 0 | - | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 57 | 10 | 0 | 25 | 3 | 67 | 14 | 0 | 25 |
| Mvmt Flow | 30 | 445 | 4 | 9 | 636 | 9 | 9 | 0 | 4 |
| Major/Minor | Major1 |  |  | Major2 |  |  | Minor1 |  |  |
| Conflicting Flow All | 645 | 0 | 0 | 449 | 0 | 0 | 1225 | 1170 | 447 |
| Stage 1 | - | - | - | - | - | - | 507 | 507 |  |
| Stage 2 | - | - | - | - | - | - | 718 | 663 |  |
| Critical Hdwy | 4.67 | - | - | 4.35 | - | - | 7.24 | 6.5 | 6.45 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.24 | 5.5 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.24 | 5.5 |  |
| Follow-up Hdwy | 2.713 | - | - | 2.425 | - | - | 3.626 | 4 | 3.525 |
| Pot Cap-1 Maneuver | 726 | - | - | 1000 | - | - | 147 | 195 | 566 |
| Stage 1 | - | - | - | - | - | - | 526 | 543 | - |
| Stage 2 | - | - | - | - | - | - | 402 | 462 | - |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 726 | - | - | 1000 | - | - | 102 | 184 | 566 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 102 | 184 |  |
| Stage 1 | - | - | - | - | - | - | 504 | 521 |  |
| Stage 2 | - | - | - | - | - | - | 291 | 456 |  |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0.6 | 0.1 | 34.2 |
| HCM LOS |  |  | D |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 136 | 726 | - | - | 1000 | - | - | 300 |
| HCM Lane V/C Ratio | 0.096 | 0.041 | - | - | 0.009 | - | - | 0.5 |
| HCM Control Delay (s) | 34.2 | 10.2 | - | - | 8.6 | 0 | - | 28.4 |
| HCM Lane LOS | D | B | - | - | A | A | - | D |
| HCM 95th \%tile Q(veh) | 0.3 | 0.1 | - | - | 0 | - | - | 2.6 |


| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | SBL | SBT | SBR |
| Vol, veh/h | 31 | 4 | 115 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | - | - | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 |
| Heavy Vehicles, \% | 23 | 100 | 17 |
| Mvmt Flow | 31 | 4 | 115 |
|  |  |  |  |


| Major/Minor | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Conflicting Flow All | 1168 | 1168 | 641 |
| Stage 1 | 659 | 659 | - |
| $\quad$ Stage 2 | 509 | 509 | - |
| Critical Hdwy | 7.33 | 7.5 | 6.37 |
| Critical Hdwy Stg 1 | 6.33 | 6.5 | - |
| Critical Hdwy Stg 2 | 6.33 | 6.5 | - |
| Follow-up Hdwy | 3.707 | 4.9 | 3.453 |
| Pot Cap-1 Maneuver | 155 | 129 | 449 |
| $\quad$ Stage 1 | 420 | 339 | - |
| $\quad$ Stage 2 | 510 | 406 | - |
| Platoon blocked, \% |  |  |  |
| Mov Cap-1 Maneuver | 147 | 122 | 449 |
| Mov Cap-2 Maneuver | 147 | 122 | - |
| Stage 1 | 403 | 334 | - |
| Stage 2 | 485 | 389 | - |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | 28.4 |
| HCM LOS | D |

[^21]|  | $\dagger$ | $\rightarrow$ | $\leftarrow$ | 4 | $\checkmark$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\uparrow$ | $\stackrel{\text { F }}{ }$ |  | Y |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% | 0\% |  | 0\% |  |
| Storage Length (ft) | 100 |  |  | 0 | 0 | 0 |
| Storage Lanes | 0 |  |  | 0 | 1 | 0 |
| Taper Length (ft) | 25 |  |  |  | 25 |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |
| Frt |  |  | 0.894 |  | 0.998 |  |
| Flt Protected |  | 0.996 |  |  | 0.953 |  |
| Satd. Flow (prot) | 0 | 1891 | 1678 | 0 | 1789 | 0 |
| Flt Permitted |  | 0.996 |  |  | 0.953 |  |
| Satd. Flow (perm) | 0 | 1891 | 1678 | 0 | 1789 | 0 |
| Link Speed (mph) |  | 30 | 30 |  | 30 |  |
| Link Distance (ft) |  | 909 | 1364 |  | 495 |  |
| Travel Time (s) |  | 20.7 | 31.0 |  | 11.3 |  |
| Intersection Summary |  |  |  |  |  |  |

Area Type:

Other

| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Vol, veh/h | 6 | 78 | 104 | 377 | 308 | 4 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 1 | 0 | 2 | 1 | 1 | 1 |
| Mvmt Flow | 6 | 78 | 104 | 377 | 308 | 4 |
| Major/Minor | Major1 |  | Major2 |  | Minor2 |  |
| Conflicting Flow All | 481 | 0 | - | 0 | 383 | 293 |
| Stage 1 | - | - | - | - | 293 | - |
| Stage 2 | - | - | - | - | 90 | - |
| Critical Hdwy | 4.11 | - | - | - | 6.41 | 6.21 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.41 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.41 | - |
| Follow-up Hdwy | 2.209 | - | - | - | 3.509 | 3.309 |
| Pot Cap-1 Maneuver | 1087 | - | - | - | 622 | 749 |
| Stage 1 | - | - | - | - | 759 | - |
| Stage 2 | - | - | - | - | 936 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1087 | - | - | - | 618 | 749 |
| Mov Cap-2 Maneuver | - | - | - | - | 618 | - |
| Stage 1 | - | - | - | - | 759 | - |
| Stage 2 | - | - | - | - | 930 | - |


| Approach | EB | WB | SB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0.6 | 0 | 16.6 |
| HCM LOS |  |  | C |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1087 | - | - | - | 619 |
| HCM Lane V/C Ratio | 0.006 | - | - | - | 0.504 |
| HCM Control Delay (s) | 8.3 | 0 | - | - | 16.6 |
| HCM Lane LOS | A | A | - | - | C |
| HCM 95th \%tile Q(veh) | 0 | - | - | - | 2.8 |


|  | $\stackrel{ }{*}$ | $\rightarrow$ | 7 | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | F |  | \% | F |  |  | ¢ |  | 7 | F |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 150 |  | 0 | 0 |  | 0 | 0 |  | 0 | 150 |  | 0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 0 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  | 0.998 |  |  | 0.933 |  |  | 0.893 |  |  |  |  |
| Flt Protected |  |  |  | 0.950 |  |  |  | 0.994 |  | 0.950 |  |  |
| Satd. Flow (prot) | 1900 | 1842 | 0 | 1770 | 1682 | 0 | 0 | 1585 | 0 | 1787 | 1727 | 0 |
| Flt Permitted |  |  |  | 0.950 |  |  |  | 0.994 |  | 0.950 |  |  |
| Satd. Flow (perm) | 1900 | 1842 | 0 | 1770 | 1682 | 0 | 0 | 1585 | 0 | 1787 | 1727 | 0 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 1364 |  |  | 144 |  |  | 957 |  |  | 513 |  |
| Travel Time (s) |  | 31.0 |  |  | 3.3 |  |  | 21.8 |  |  | 11.7 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type: ..... Other

| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 167.2 |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 0 | 381 | 5 | 97 | 464 | 377 | 15 | 10 | 96 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - |  | None |
| Storage Length | 150 | - | - | 0 | - | - | - |  |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 0 | 3 | 0 | 2 | 9 | 1 | 0 | 10 | 7 |
| Mvmt Flow | 0 | 381 | 5 | 97 | 464 | 377 | 15 | 10 | 96 |
| Major/Minor | Major1 |  |  | Major2 |  |  | Minor1 |  |  |
| Conflicting Flow All | 841 | 0 | 0 | 386 | 0 | 0 | 1236 | 1419 | 384 |
| Stage 1 | - | - | - | - | - | - | 384 | 384 |  |
| Stage 2 | - | - | - | - | - | - | 852 | 1035 |  |
| Critical Hdwy | 4.1 | - | - | 4.12 | - | - | 7.1 | 6.6 | 6.27 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.6 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - |  | 6.1 | 5.6 |  |
| Follow-up Hdwy | 2.2 | - | - | 2.218 | - | - | 3.5 | 4.09 | 3.363 |
| Pot Cap-1 Maneuver | 803 | - | - | 1172 | - | - | 154 | 131 | 653 |
| Stage 1 | - | - | - | - | - |  | 643 | 598 |  |
| Stage 2 | - | - | - | - | - | - | 357 | 299 | - |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 803 | - | - | 1172 | - | - | 137 | 120 | 653 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 137 | 120 |  |
| Stage 1 | - | - | - | - | - |  | 643 | 598 |  |
| Stage 2 | - | - | - | - | - | - | 318 | 274 |  |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0 | 0.9 | 20.2 |
| HCM LOS |  |  | $C$ |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 | SBLn2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 356 | 803 | - | - | 1172 | - | - | 106 | 157 |
| HCM Lane V/C Ratio | 0.34 | - | - | - | 0.083 | - | - | 2.906 | 0.064 |
| HCM Control Delay (s) | 20.2 | 0 | - | - | 8.3 | - | $-\$ 945.5$ | 29.5 |  |
| HCM Lane LOS | C | A | - | - | A | - | - | F | D |
| HCM 95th \%tile Q(veh) | 1.5 | 0 | - | - | 0.3 | - | - | 29.2 | 0.2 |

## Notes

~: Volume exceeds capacity $\quad \$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ *: All major volume in platoon

| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
|  | SBL | SBT | SBR |
| Movement | 308 | 10 | 0 |
| Vol, veh/h | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | Stop | Stop | Stop |
| Sign Control | - | - | None |
| RT Channelized | 150 | - | - |
| Storage Length | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade \% | 100 | 100 | 100 |
| Peak Hour Factor | 1 | 10 | 0 |
| Heavy Vehicles, \% | 308 | 10 | 0 |
| Mvmt Flow |  |  |  |


| Major/Minor | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Conflicting Flow All | 1284 | 1233 | 653 |
| Stage 1 | 847 | 847 | - |
| Stage 2 | 437 | 386 | - |
| Critical Hdwy | 7.11 | 6.6 | 6.2 |
| Critical Hdwy Stg 1 | 6.11 | 5.6 | - |
| Critical Hdwy Stg 2 | 6.11 | 5.6 | - |
| Follow-up Hdwy | 3.509 | 4.09 | 3.3 |
| Pot Cap-1 Maneuver | $\sim 142$ | 171 | 471 |
| Stage 1 | 358 | 367 | - |
| Stage 2 | 600 | 596 | - |
| Platoon blocked, \% | $\sim 106$ | 157 | 471 |
| Mov Cap-1 Maneuver | $\sim 106$ | 157 | - |
| Mov Cap-2 Maneuver | 358 | 337 | - |
| Stage 1 | 503 | 596 | - |
| Stage 2 |  |  |  |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | $\$ 916.7$ |
| HCM LOS | F |

[^22]|  | $\Rightarrow$ | $\rightarrow$ | $\geqslant$ | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $P$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | F |  |  | $\uparrow$ |  |  |  |  |  | $\uparrow$ | F |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 25 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 1 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  | 0.897 |  |  |  |  |  |  |  |  |  | 0.850 |
| Flt Protected |  |  |  |  | 0.985 |  |  |  |  |  | 0.953 |  |
| Satd. Flow (prot) | 0 | 1664 | 0 | 0 | 1818 | 0 | 0 | 0 | 0 | 0 | 1632 | 1583 |
| Flt Permitted |  |  |  |  | 0.985 |  |  |  |  |  | 0.953 |  |
| Satd. Flow (perm) | 0 | 1664 | 0 | 0 | 1818 | 0 | 0 | 0 | 0 | 0 | 1632 | 1583 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance ( t ) |  | 144 |  |  | 502 |  |  | 626 |  |  | 699 |  |
| Travel Time (s) |  | 3.3 |  |  | 11.4 |  |  | 14.2 |  |  | 15.9 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 660 |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 0 | 185 | 600 | 374 | 824 | 0 | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - |  |  |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 0 | 7 | 1 | 5 | 2 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 0 | 185 | 600 | 374 | 824 | 0 | 0 | 0 | 0 |
| Major/Minor | Major1 |  |  | Major2 |  |  |  |  |  |
| Conflicting Flow All | 824 | 0 | 0 | 785 | 0 | 0 |  |  |  |
| Stage 1 | - | - | - | - | - | - |  |  |  |
| Stage 2 | - | - | - | - | - | - |  |  |  |
| Critical Hdwy | 4.1 | - | - | 4.15 | - | - |  |  |  |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |  |  |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |  |  |  |
| Follow-up Hdwy | 2.2 | - | - | 2.245 | - | - |  |  |  |
| Pot Cap-1 Maneuver | 815 | - | - | 820 | - | - |  |  |  |
| Stage 1 | - | - | - | - | - | - |  |  |  |
| Stage 2 | - | - | - | - | - | - |  |  |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 815 | - | - | 820 | - | - |  |  |  |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |  |  |  |
| Stage 1 | - | - | - | - | - | - |  |  |  |
| Stage 2 | - | - | - | - | - | - |  |  |  |


| Approach | EB | WB |
| :--- | :---: | :---: |
| HCM Control Delay, s | 0 | 4.1 |
| HCM LOS |  |  |


| Minor Lane/Major Mvmt | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 | SBLn2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 815 | - | - | 820 | - | - | 9 | 373 |
| HCM Lane V/C Ratio | - | - | - | 0.456 | - | - | 18.778 | 0.306 |
| HCM Control Delay (s) | 0 | - | - | 13 | 0 | $-\$ 8807.3$ | 18.8 |  |
| HCM Lane LOS | A | - | - | B | A | - | F | C |
| HCM 95th \%tile Q(veh) | 0 | - | - | 2.4 | - | - | 22.8 | 1.3 |

## Notes

~: Volume exceeds capacity $\quad \$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ *: All major volume in platoon

| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | SBL | SBT | SBR |
| Vol, veh/h | 0 | 4 | 114 |
| Conflicting Peds, \#/hr | Stop | Stop | Stop |
| Sign Control | - | - | None |
| RT Channelized | - | - | 25 |
| Storage Length | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | 100 | 100 | 100 |
| Peak Hour Factor | 10 | 50 | 2 |
| Heavy Vehicles, \% | 165 | 4 | 114 |
| Mvmt Flow |  |  |  |
|  |  |  |  |


| Major/Minor | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Conflicting Flow All | 2057 | 2357 | 824 |
| Stage 1 | 1572 | 1572 | - |
| Stage 2 | 485 | 785 | - |
| Critical Hdwy | 6.5 | 7 | 6.22 |
| Critical Hdwy Stg 1 | 5.5 | 6 | - |
| Critical Hdwy Stg 2 | 5.5 | 6 | - |
| Follow-up Hdwy | 3.59 | 4.45 | 3.318 |
| Pot Cap-1 Maneuver | $\sim 58$ | 25 | 373 |
| $\quad$ Stage 1 | 180 | 134 | - |
| Stage 2 | 603 | 342 | - |
| Platoon blocked, \% | $\sim 9$ | 0 | 373 |
| Mov Cap-1 Maneuver | $\sim 9$ | 0 | - |
| Mov Cap-2 Maneuver | $\sim 29$ | 0 | - |
| Stage 1 | 603 | 0 | - |
| Stage 2 |  |  |  |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | $\$ 5267.1$ |
| HCM LOS | F |

[^23]|  | $\rangle$ | $\rightarrow$ | $\rangle$ | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | F |  |  | $\uparrow$ | F |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 50 | 0 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 0 |  | 1 | 0 |  | 0 |
| Taper Length ( t ) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  |  |  |  | 0.972 |  |  |  | 0.850 |  |  |  |
| Flt Protected |  | 0.990 |  |  |  |  |  | 0.953 |  |  |  |  |
| Satd. Flow (prot) | 0 | 1741 | 0 | 0 | 1772 | 0 | 0 | 1784 | 1568 | 0 | 0 | 0 |
| Flt Permitted |  | 0.990 |  |  |  |  |  | 0.953 |  |  |  |  |
| Satd. Flow (perm) | 0 | 1741 | 0 | 0 | 1772 | 0 | 0 | 1784 | 1568 | 0 | 0 | 0 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance ( t ) |  | 502 |  |  | 143 |  |  | 542 |  |  | 648 |  |
| Travel Time (s) |  | 11.4 |  |  | 3.3 |  |  | 12.3 |  |  | 14.7 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type: ..... Other

| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 282.7 |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 69 | 281 | 0 | 0 | 451 | 119 | 747 | 8 | 591 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | 50 |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 4 |  | 0 | 0 | 4 | 5 | 1 | 50 | 3 |
| Mvmt Flow | 69 | 281 | 0 | 0 | 451 | 119 | 747 | 8 | 591 |
| Major/Minor | Major1 |  |  | Major2 |  |  | Minor1 |  |  |
| Conflicting Flow All | 570 | 0 | 0 | 281 | 0 | 0 | 930 | 989 | 281 |
| Stage 1 | - | - | - | - | - | - | 419 | 419 |  |
| Stage 2 | - | - | - | - | - | - | 511 | 570 |  |
| Critical Hdwy | 4.14 | - | - | 4.1 | - | - | 6.41 | 7 | 6.23 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 5.41 | 6 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 5.41 | 6 |  |
| Follow-up Hdwy | 2.236 | - | - | 2.2 | - | - | 3.509 | 4.45 | 3.327 |
| Pot Cap-1 Maneuver | 993 | - | - | 1293 | - | - | $\sim 298$ | 205 | 755 |
| Stage 1 | - | - | - | - | - | - | $\sim 666$ | 516 |  |
| Stage 2 | - | - | - | - | - | - | $\sim 604$ | 436 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 993 | - | - | 1293 | - | - | $\sim 274$ | 0 | 755 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | $\sim 274$ | 0 |  |
| Stage 1 | - | - | - | - | - | - | $\sim 611$ | 0 |  |
| Stage 2 | - | - | - | - | - | - | $\sim 604$ | 0 |  |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 1.8 | 0 | $\$ 475.4$ |
| HCM LOS |  |  | F |


| Minor Lane/Major Mvmt | NBLn1 | NBLn2 | EBL | EBT | EBR | WBL | WBT | WBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 274 | 755 | 993 | - | - | 1293 | - | - |
| HCM Lane V/C Ratio | 2.755 | 0.783 | 0.069 | - | - | - | - | - |
| HCM Control Delay (s) | $\$ 828.2$ | 24.7 | 8.9 | 0 | - | 0 | - | - |
| HCM Lane LOS | F | C | A | A | - | A | - | - |
| HCM 95th \%tile Q(veh) | 64.5 | 7.8 | 0.2 | - | - | 0 | - | - |

Notes
~: Volume exceeds capacity $\quad \$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ *: All major volume in platoon

| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | SBL | SBT | SBR |
| Vol, veh/h | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | - | - | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 |
| Heavy Vehicles, \% | 0 | 0 | 0 |
| Mvmt Flow | 0 | 0 | 0 |


| Major/Minor |
| :--- |
| Conflicting Flow All |
| $\quad$ Stage 1 |
| $\quad$ Stage 2 |
| Critical Hdwy |
| Critical Hdwy Stg 1 |
| Critical Hdwy Stg 2 |
| Follow-up Hdwy |
| Pot Cap-1 Maneuver |
| $\quad$ Stage 1 |
| $\quad$ Stage 2 |
| Platoon blocked, \% |
| Mov Cap-1 Maneuver |
| Mov Cap-2 Maneuver |
| Stage 1 |
| Stage 2 |

## Approach

HCM Control Delay, s
HCM LOS

## Minor Lane/Major Mvmt

|  | \% | $\rightarrow$ | 7 | $\dagger$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | 1 | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | F |  |  | $\uparrow$ |  |  | ¢ |  |  | ${ }^{\text {¢ }}$ |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  | 0.998 |  |  | 0.998 |  |  | 0.932 |  |  | 0.879 |  |
| Flt Protected | 0.950 |  |  |  | 0.999 |  |  | 0.976 |  |  | 0.997 |  |
| Satd. Flow (prot) | 1308 | 1818 | 0 | 0 | 1830 | 0 | 0 | 1728 | 0 | 0 | 1381 | 0 |
| Flt Permitted | 0.950 |  |  |  | 0.999 |  |  | 0.976 |  |  | 0.997 |  |
| Satd. Flow (perm) | 1308 | 1818 | 0 | 0 | 1830 | 0 | 0 | 1728 | 0 | 0 | 1381 | 0 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 143 |  |  | 173 |  |  | 583 |  |  | 174 |  |
| Travel Time (s) |  | 3.3 |  |  | 3.9 |  |  | 13.3 |  |  | 4.0 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type:

Other

| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 1.8 |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 32 | 828 | 12 | 5 | 463 | 8 | 5 | 0 | 5 |
| Conflicting Peds, \#hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | 0 | - | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 38 | 4 | 25 | 25 | 2 | 77 | 0 | 0 | 0 |
| Mvmt Flow | 32 | 828 | 12 | 5 | 463 | 8 | 5 | 0 | 5 |
| Major/Minor | Major1 |  |  | Major2 |  |  | Minor1 |  |  |
| Conflicting Flow All | 471 | 0 | 0 | 840 | 0 | 0 | 1429 | 1379 | 834 |
| Stage 1 | - | - | - | - | - | - | 898 | 898 |  |
| Stage 2 | - | - | - | - | - | - | 531 | 481 |  |
| Critical Hdwy | 4.48 | - | - | 4.35 | - | - | 7.1 | 6.5 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.5 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.1 | 5.5 |  |
| Follow-up Hdwy | 2.542 | - | - | 2.425 | - | - | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 926 | - | - | 704 | - | - | 114 | 146 | 371 |
| Stage 1 | - | - | - | - | - | - | 337 | 361 | - |
| Stage 2 | - | - | - | - | - | - | 536 | 557 | - |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 926 | - | - | 704 | - | - | 88 | 140 | 371 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 88 | 140 |  |
| Stage 1 | - | - | - | - | - | - | 325 | 349 |  |
| Stage 2 | - | - | - | - | - | - | 429 | 551 |  |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0.3 | 0.1 | 32.3 |
| HCM LOS |  |  | D |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 142 | 926 | - | - | 704 | - | - | 407 |
| HCM Lane V/C Ratio | 0.07 | 0.035 | - | - | 0.007 | - | - | 0.283 |
| HCM Control Delay (s) | 32.3 | 9 | - | - | 10.2 | 0 | - | 17.3 |
| HCM Lane LOS | D | A | - | - | B | A | - | C |
| HCM 95th \%tile Q(veh) | 0.2 | 0.1 | - | - | 0 | - | - | 1.1 |


| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | 8 | 4 | 103 |
| Vol, veh/h | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | Stop | Stop | Stop |
| Sign Control | - | - | None |
| RT Channelized | - | - | - |
| Storage Length | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | 100 | 100 | 100 |
| Peak Hour Factor | 0 | 0 | 23 |
| Heavy Vehicles, \% | 8 | 4 | 103 |
| Mvmt Flow |  |  |  |
|  |  |  |  |


| Major/Minor | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Conflicting Flow All | 1378 | 1381 | 467 |
| $\quad$ Stage 1 | 477 | 477 | - |
| $\quad$ Stage 2 | 901 | 904 | - |
| Critical Hdwy | 7.1 | 6.5 | 6.43 |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - |
| Follow-up Hdwy | 3.5 | 4 | 3.507 |
| Pot Cap-1 Maneuver | 123 | 145 | 555 |
| $\quad$ Stage 1 | 573 | 559 | - |
| $\quad$ Stage 2 | 335 | 358 | - |
| Platoon blocked, \% |  |  |  |
| Mov Cap-1 Maneuver | 117 | 139 | 555 |
| Mov Cap-2 Maneuver | 117 | 139 | - |
| Stage 1 | 553 | 553 | - |
| Stage 2 | 319 | 346 | - |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | 17.3 |
| HCM LOS | C |

## Minor Lane/Major Mvmt

|  | \% | $\rightarrow$ | $\leftarrow$ | 4 | $\checkmark$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\uparrow$ | $\stackrel{\text { F }}{ }$ |  | M |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% | 0\% |  | 0\% |  |
| Storage Length (ft) | 100 |  |  | 0 | 0 | 0 |
| Storage Lanes | 0 |  |  | 0 | 1 | 0 |
| Taper Length (t) | 25 |  |  |  | 25 |  |
| Lane Utill. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |
| Frt |  |  | 0.881 |  | 0.998 |  |
| Flt Protected |  | 0.996 |  |  | 0.953 |  |
| Satd. Flow (prot) | 0 | 1747 | 1637 | 0 | 1789 | 0 |
| Flt Permitted |  | 0.996 |  |  | 0.953 |  |
| Satd. Flow (perm) | 0 | 1747 | 1637 | 0 | 1789 | 0 |
| Link Speed (mph) |  | 30 | 30 |  | 30 |  |
| Link Distance (ft) |  | 909 | 1364 |  | 495 |  |
| Travel Time (s) |  | 20.7 | 31.0 |  | 11.3 |  |
| Intersection Summary |  |  |  |  |  |  |

Area Type:

Other

| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 6.2 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Vol, veh/h | 7 | 74 | 65 | 493 | 328 | 5 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 1 | 9 | 12 | 1 | 1 | 1 |
| Mvmt Flow | 7 | 74 | 65 | 493 | 328 | 5 |
| Major/Minor | Major1 |  | Major2 |  | Minor2 |  |
| Conflicting Flow All | 558 | 0 | - | 0 | 400 | 312 |
| Stage 1 | - | - | - | - | 312 | - |
| Stage 2 | - | - | - | - | 88 | - |
| Critical Hdwy | 4.11 | - | - | - | 6.41 | 6.21 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.41 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.41 | - |
| Follow-up Hdwy | 2.209 | - | - | - | 3.509 | 3.309 |
| Pot Cap-1 Maneuver | 1018 | - | - | - | 608 | 731 |
| Stage 1 | - | - | - | - | 744 | - |
| Stage 2 | - | - | - | - | 938 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1018 | - | - | - | 604 | 731 |
| Mov Cap-2 Maneuver | - | - | - | - | 604 | - |
| Stage 1 | - | - | - | - | 744 | - |
| Stage 2 | - | - | - | - | 931 | - |


| Approach | EB | WB | SB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0.7 | 0 | 17.9 |
| HCM LOS |  |  | C |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1018 | - | - | - | 606 |
| HCM Lane V/C Ratio | 0.007 | - | - | - | 0.55 |
| HCM Control Delay (s) | 8.6 | 0 | - | - | 17.9 |
| HCM Lane LOS | A | A | - | - | C |
| HCM 95th \%tile Q(veh) | 0 | - | - | - | 3.3 |


|  | $\stackrel{ }{*}$ | $\rightarrow$ | 7 | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | F |  | \% | F |  |  | ¢ |  | 7 | F |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 150 |  | 0 | 0 |  | 0 | 0 |  | 0 | 200 |  | 0 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 0 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  | 0.994 |  |  | 0.929 |  |  | 0.896 |  |  |  |  |
| Flt Protected |  |  |  | 0.950 |  |  |  | 0.997 |  | 0.950 |  |  |
| Satd. Flow (prot) | 1881 | 1819 | 0 | 1703 | 1739 | 0 | 0 | 1621 | 0 | 1787 | 1881 | 0 |
| Flt Permitted |  |  |  | 0.950 |  |  |  | 0.997 |  | 0.950 |  |  |
| Satd. Flow (perm) | 1881 | 1819 | 0 | 1703 | 1739 | 0 | 0 | 1621 | 0 | 1787 | 1881 | 0 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 1364 |  |  | 144 |  |  | 957 |  |  | 513 |  |
| Travel Time (s) |  | 31.0 |  |  | 3.3 |  |  | 21.8 |  |  | 11.7 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type: ..... Other

| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 216.4 |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 0 | 387 | 15 | 77 | 553 | 493 | 5 | 15 | 66 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | 150 | - | - | 0 | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 1 | 4 | 0 | 6 | 2 | 1 | 25 | 1 | 4 |
| Mvmt Flow | 0 | 387 | 15 | 77 | 553 | 493 | 5 | 15 | 66 |
| Major/Minor | Major1 |  |  | Major2 |  |  | Minor1 |  |  |
| Conflicting Flow All | 1046 | 0 | 0 | 402 | 0 | 0 | 1354 | 1595 | 395 |
| Stage 1 | - | - | - | - | - | - | 395 | 395 |  |
| Stage 2 | - | - | - | - | - | - | 959 | 1200 |  |
| Critical Hdwy | 4.11 | - | - | 4.16 | - | - | 7.35 | 6.51 | 6.24 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.35 | 5.51 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.35 | 5.51 |  |
| Follow-up Hdwy | 2.209 | - | - | 2.254 | - | - | 3.725 | 4.009 | 3.336 |
| Pot Cap-1 Maneuver | 669 | - | - | 1135 | - | - | 113 | 107 | 650 |
| Stage 1 | - | - | - | - | - | - | 587 | 606 |  |
| Stage 2 | - | - | - | - | - | - | 281 | 259 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 669 | - | - | 1135 | - | - | 101 | 100 | 650 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 101 | 100 |  |
| Stage 1 | - | - | - | - | - | - | 587 | 606 |  |
| Stage 2 | - | - | - | - | - | - | 254 | 241 |  |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0 | 0.6 | 22.9 |
| HCM LOS |  |  | $C$ |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 | SBLn2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 286 | 669 | - | - | 1135 | - | - | 91 | 140 |
| HCM Lane V/C Ratio | 0.301 | - | - | - | 0.068 | - | - | 3.615 | 0.071 |
| HCM Control Delay (s) | 22.9 | 0 | - | - | 8.4 | - | $-\$ 1273.8$ | 32.7 |  |
| HCM Lane LOS | C | A | - | - | A | - | - | F | D |
| HCM 95th \%tile Q(veh) | 1.2 | 0 | - | - | 0.2 | - | - | 33.4 | 0.2 |

## Notes

~: Volume exceeds capacity $\quad \$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ *: All major volume in platoon

| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
|  | SBL | SBT | SBR |
| Movement | 329 | 10 | 0 |
| Vol, veh/h | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | Stop | Stop | Stop |
| Sign Control | - | - | None |
| RT Channelized | 200 | - | - |
| Storage Length | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade \% | 100 | 100 | 100 |
| Peak Hour Factor | 1 | 1 | 1 |
| Heavy Vehicles, \% | 329 | 10 | 0 |
| Mvmt Flow |  |  |  |
|  |  |  |  |


| Major/Minor | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Conflicting Flow All | 1389 | 1356 | 800 |
| Stage 1 | 954 | 954 | - |
| Stage 2 | 435 | 402 | - |
| Critical Hdwy | 7.11 | 6.51 | 6.21 |
| Critical Hdwy Stg 1 | 6.11 | 5.51 | - |
| Critical Hdwy Stg 2 | 6.11 | 5.51 | - |
| Follow-up Hdwy | 3.509 | 4.009 | 3.309 |
| Pot Cap-1 Maneuver | $\sim 121$ | 150 | 387 |
| $\quad$ Stage 1 | $\sim 312$ | 339 | - |
| $\quad$ Stage 2 | 602 | 602 | - |
| Platoon blocked, \% | $\sim 91$ | 140 | 387 |
| Mov Cap-1 Maneuver | $\sim 91$ | 140 | - |
| Mov Cap-2 Maneuver | $\sim 312$ | 316 | - |
| Stage 1 | 527 | 602 | - |
| Stage 2 |  |  |  |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | $\$ 1237.2$ |
| HCM LOS | F |

[^24]|  | $\Rightarrow$ | $\rightarrow$ | $\geqslant$ | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $P$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | F |  |  | $\uparrow$ |  |  |  |  |  | $\uparrow$ | F |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 25 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 1 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Fit |  | 0.890 |  |  |  |  |  |  |  |  |  | 0.850 |
| Flt Protected |  |  |  |  | 0.986 |  |  |  |  |  | 0.953 |  |
| Satd. Flow (prot) | 0 | 1655 | 0 | 0 | 1850 | 0 | 0 | 0 | 0 | 0 | 1743 | 1495 |
| Flt Permitted |  |  |  |  | 0.986 |  |  |  |  |  | 0.953 |  |
| Satd. Flow (perm) | 0 | 1655 | 0 | 0 | 1850 | 0 | 0 | 0 | 0 | 0 | 1743 | 1495 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance ( t ) |  | 144 |  |  | 502 |  |  | 626 |  |  | 699 |  |
| Travel Time (s) |  | 3.3 |  |  | 11.4 |  |  | 14.2 |  |  | 15.9 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 6153.7 |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 0 | 146 | 636 | 375 | 982 | 0 | 0 | 0 | 0 |
| Conflicting Peds, \#hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - |  |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 0 | 3 | 2 | 2 | 1 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 0 | 146 | 636 | 375 | 982 | 0 | 0 | 0 | 0 |
| Major/Minor | Major1 |  |  | Major2 |  |  |  |  |  |
| Conflicting Flow All | 982 | 0 | 0 | 782 | 0 | 0 |  |  |  |
| Stage 1 | - | - | - | - | - | - |  |  |  |
| Stage 2 | - | - | - | - | - | - |  |  |  |
| Critical Hdwy | 4.1 | - | - | 4.12 | - | - |  |  |  |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |  |  |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |  |  |  |
| Follow-up Hdwy | 2.2 | - | - | 2.218 | - | - |  |  |  |
| Pot Cap-1 Maneuver | 711 | - | - | 836 | - | - |  |  |  |
| Stage 1 | - | - | - | - | - | - |  |  |  |
| Stage 2 | - | - | - | - | - | - |  |  |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 711 | - | - | 836 | - | - |  |  |  |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |  |  |  |
| Stage 1 | - | - | - | - | - | - |  |  |  |
| Stage 2 | - | - | - | - | - | - |  |  |  |


| Approach | EB | WB |
| :--- | :---: | :---: |
| HCM Control Delay, s | 0 | 3.5 |
| HCM LOS |  |  |


| Minor Lane/Major Mvmt | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 | SBLn2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 711 | - | - | 836 | - | - | 1 | 294 |
| HCM Lane V/C Ratio | - | - | - | 0.449 | - | - | 176 | 0.48 |
| HCM Control Delay (s) | 0 | - | - | 12.8 | 0 | $\$ 85822.9$ | 28 |  |
| HCM Lane LOS | A | - | - | B | A | - | F | D |
| HCM 95th \%tile Q(veh) | 0 | - | - | 2.3 | - | - | 24.6 | 2.5 |

## Notes

~: Volume exceeds capacity $\quad \$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ *: All major volume in platoon

| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | SBL | SBT | SBR |
| Vol, veh/h | 0 | 4 | 141 |
| Conflicting Peds, \#/hr | Stop | Stop | Stop |
| Sign Control | - | - | None |
| RT Channelized | - | - | 25 |
| Storage Length | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | 100 | 100 | 100 |
| Peak Hour Factor | 4 | 0 | 8 |
| Heavy Vehicles, \% | 172 | 4 | 141 |
| Mvmt Flow |  |  |  |


| Major/Minor | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Conflicting Flow All | 2196 | 2514 | 982 |
| $\quad$ Stage 1 | 1732 | 1732 | - |
| $\quad$ Stage 2 | 464 | 782 | - |
| Critical Hdwy | 6.44 | 6.5 | 6.28 |
| Critical Hdwy Stg 1 | 5.44 | 5.5 | - |
| Critical Hdwy Stg 2 | 5.44 | 5.5 | - |
| Follow-up Hdwy | 3.536 | 4 | 3.372 |
| Pot Cap-1 Maneuver | $\sim 49$ | 29 | 294 |
| $\quad$ Stage 1 | $\sim 155$ | 144 | - |
| $\quad 629$ | 408 | - |  |
| Stage 2 |  |  |  |
| Platoon blocked, \% | $\sim 1$ | 0 | 294 |
| Mov Cap-1 Maneuver | $\sim 1$ | 0 | - |
| Mov Cap-2 Maneuver | $\sim 2$ | 0 | - |
| Stage 1 | 629 | 0 | - |
| Stage 2 |  |  |  |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | $\$ 47661.8$ |
| HCM LOS | F |

[^25]|  | * | $\rightarrow$ | $\rangle$ | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ |  |  | F |  |  | $\uparrow$ | 7 |  |  |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 50 | 0 |  | 0 |
| Storage Lanes | 0 |  | 0 | 0 |  | 0 | 0 |  | 1 | 0 |  | 0 |
| Taper Length (tt) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  |  |  |  | 0.970 |  |  |  | 0.850 |  |  |  |
| FIt Protected |  | 0.988 |  |  |  |  |  | 0.953 |  |  |  |  |
| Satd. Flow (prot) | 0 | 1804 | 0 | 0 | 1755 | 0 | 0 | 1793 | 1568 | 0 | 0 | 0 |
| Flt Permitted |  | 0.988 |  |  |  |  |  | 0.953 |  |  |  |  |
| Satd. Flow (perm) | 0 | 1804 | 0 | 0 | 1755 | 0 | 0 | 1793 | 1568 | 0 | 0 | 0 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance ( t ) |  | 502 |  |  | 143 |  |  | 542 |  |  | 648 |  |
| Travel Time (s) |  | 11.4 |  |  | 3.3 |  |  | 12.3 |  |  | 14.7 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |


| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 410.1 |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 74 | 244 | 0 | 0 | 430 | 124 | 927 | 4 | 564 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - | - | 50 |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 1 | 5 | 0 | 0 | 3 | 12 | 1 | 0 | 3 |
| Mvmt Flow | 74 | 244 | 0 | 0 | 430 | 124 | 927 | 4 | 564 |
| Major/Minor | Major1 |  |  | Major2 |  |  | Minor1 |  |  |
| Conflicting Flow All | 554 | 0 | 0 | 244 | 0 | 0 | 884 | 946 | 244 |
| Stage 1 | - | - | - | - | - | - | 392 | 392 |  |
| Stage 2 | - | - | - | - | - | - | 492 | 554 |  |
| Critical Hdwy | 4.11 | - | - | 4.1 | - | - | 6.41 | 6.5 | 6.23 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 5.41 | 5.5 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 5.41 | 5.5 |  |
| Follow-up Hdwy | 2.209 | - | - | 2.2 | - | - | 3.509 | 4 | 3.327 |
| Pot Cap-1 Maneuver | 1021 | - | - | 1334 | - | - | $\sim 317$ | 264 | 792 |
| Stage 1 | - | - | - | - | - | - | $\sim 685$ | 610 |  |
| Stage 2 | - | - | - | - | - | - | $\sim 617$ | 517 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1021 | - | - | 1334 | - | - | $\sim 290$ | 0 | 792 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | $\sim 290$ | 0 |  |
| Stage 1 | - | - | - | - | - | - | $\sim 627$ | 0 |  |
| Stage 2 | - | - | - | - | - | - | $\sim 617$ | 0 |  |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 2 | 0 | $\$ 648.8$ |
| HCM LOS |  |  | F |


| Minor Lane/Major Mvmt | NBLn1 | NBLn2 | EBL | EBT | EBR | WBL | WBT | WBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 290 | 792 | 1021 | - | - | 1334 | - | - |
| HCM Lane V/C Ratio | 3.21 | 0.712 | 0.072 | - | - | - | - | - |
| HCM Control Delay (s) | $\$ 1029.8$ | 20 | 8.8 | 0 | - | 0 | - | - |
| HCM Lane LOS | F | C | A | A | - | A | - | - |
| HCM 95th \%tile Q(veh) | 84.3 | 6.1 | 0.2 | - | - | 0 | - | - |
| Notes |  |  |  |  |  |  |  |  |

$\sim$ : Volume exceeds capacity $\quad \$$ : Delay exceeds $300 \mathrm{~s} \quad+$ Computation Not Defined $\quad$ *: All major volume in platoon

| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | SBL | SBT | SBR |
| Vol, veh/h | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | - | - | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 |
| Heavy Vehicles, \% | 0 | 0 | 0 |
| Mvmt Flow | 0 | 0 | 0 |


| Major/Minor |
| :--- |
| Conflicting Flow All |
| $\quad$ Stage 1 |
| $\quad$ Stage 2 |
| Critical Hdwy |
| Critical Hdwy Stg 1 |
| Critical Hdwy Stg 2 |
| Follow-up Hdwy |
| Pot Cap-1 Maneuver |
| $\quad$ Stage 1 |
| $\quad$ Stage 2 |
| Platoon blocked, \% |
| Mov Cap-1 Maneuver |
| Mov Cap-2 Maneuver |
| Stage 1 |
| Stage 2 |

## Approach

HCM Control Delay, s
HCM LOS

## Minor Lane/Major Mvmt

|  | $\Rightarrow$ | $\rightarrow$ | 7 | $\checkmark$ | $\leftarrow$ | 4 | 4 | $\uparrow$ | $p$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | F |  |  | ¢ |  |  | ¢ |  |  | ${ }^{\text {¢ }}$ |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  | 0.999 |  |  | 0.998 |  |  | 0.966 |  |  | 0.884 |  |
| Flt Protected | 0.950 |  |  |  | 0.999 |  |  | 0.976 |  |  | 0.995 |  |
| Satd. Flow (prot) | 1570 | 1824 | 0 | 0 | 1820 | 0 | 0 | 1518 | 0 | 0 | 1458 | 0 |
| Flt Permitted | 0.950 |  |  |  | 0.999 |  |  | 0.976 |  |  | 0.995 |  |
| Satd. Flow (perm) | 1570 | 1824 | 0 | 0 | 1820 | 0 | 0 | 1518 | 0 | 0 | 1458 | 0 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance ( t ) |  | 143 |  |  | 173 |  |  | 583 |  |  | 174 |  |
| Travel Time (s) |  | 3.3 |  |  | 3.9 |  |  | 13.3 |  |  | 4.0 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type:

Other

| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 2.2 |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 16 | 787 | 5 | 5 | 441 | 8 | 10 | 5 | 5 |
| Conflicting Peds, \#hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | 0 | - | - | - | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 15 | 4 | 17 | 0 | 3 | 67 | 11 | 0 | 50 |
| Mvmt Flow | 16 | 787 | 5 | 5 | 441 | 8 | 10 | 5 | 5 |
| Major/Minor | Major1 |  |  | Major2 |  |  | Minor1 |  |  |
| Conflicting Flow All | 449 | 0 | 0 | 792 | 0 | 0 | 1331 | 1281 | 790 |
| Stage 1 | - | - | - | - | - | - | 822 | 822 |  |
| Stage 2 | - | - | - | - | - | - | 509 | 459 |  |
| Critical Hdwy | 4.25 | - | - | 4.1 | - | - | 7.21 | 6.5 | 6.7 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.21 | 5.5 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.21 | 5.5 |  |
| Follow-up Hdwy | 2.335 | - | - | 2.2 | - | - | 3.599 | 4 | 3.75 |
| Pot Cap-1 Maneuver | 1046 | - | - | 838 | - | - | 126 | 167 | 324 |
| Stage 1 | - | - | - | - | - | - | 355 | 391 | - |
| Stage 2 | - | - | - | - | - | - | 530 | 570 | - |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1046 | - | - | 838 | - | - | 100 | 163 | 324 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 100 | 163 |  |
| Stage 1 | - | - | - | - | - | - | 350 | 385 |  |
| Stage 2 | - | - | - | - | - | - | 430 | 565 |  |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0.2 | 0.1 | 35.7 |
| HCM LOS |  |  | E |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 137 | 1046 | - | - | 838 | - | - | 404 |
| HCM Lane V/C Ratio | 0.146 | 0.015 | - | - | 0.006 | - | - | 0.297 |
| HCM Control Delay (s) | 35.7 | 8.5 | - | - | 9.3 | 0 | - | 17.6 |
| HCM Lane LOS | E | A | - | - | A | A | - | C |
| HCM 95th \%tile Q(veh) | 0.5 | 0 | - | - | 0 | - | - | 1.2 |


| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | SBL | SBT | SBR |
| Vol, veh/h | 0 | 4 | 103 |
| Conflicting Peds, \#/hr | Stop | Stop | Stop |
| Sign Control | - | - | None |
| RT Channelized | - | - | - |
| Storage Length | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | 100 | 100 | 100 |
| Peak Hour Factor | 0 | 0 | 17 |
| Heavy Vehicles, \% | 13 | 4 | 103 |
| Mvmt Flow |  |  |  |


| Major/Minor | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Conflicting Flow All | 1282 | 1279 | 445 |
| $\quad$ Stage 1 | 455 | 455 | - |
| $\quad$ Stage 2 | 827 | 824 | - |
| Critical Hdwy | 7.1 | 6.5 | 6.37 |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - |
| Follow-up Hdwy | 3.5 | 4 | 3.453 |
| Pot Cap-1 Maneuver | 144 | 167 | 583 |
| $\quad$ Stage 1 | 589 | 572 | - |
| $\quad$ Stage 2 | 369 | 390 | - |
| Platoon blocked, \% |  |  |  |
| Mov Cap-1 Maneuver | 136 | 163 | 583 |
| Mov Cap-2 Maneuver | 136 | 163 | - |
| Stage 1 | 580 | 567 | - |
| Stage 2 | 353 | 384 | - |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | 17.6 |
| HCM LOS | C |

[^26]
## Appendix V 2017 Total Traffic Conditions (Build) Worksheets - Study Intersections

## SITE LAYOUT

## Site: 2017 Total Build NW 319 St and NW 31st Ave Weekday AM

2017 Total Traffic Weekday AM
Roundabout


## MOVEMENT SUMMARY

Site: 2017 Total Build NW 319 St and NW 31st Ave Weekday AM
2017 Total Traffic Weekday AM
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \mathrm{Mov} \\ & \mathrm{ID} \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | Flows HV $\%$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles veh | Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| South: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 5 | 0.0 | 0.117 | 6.0 | LOS A | 0.5 | 15.8 | 0.46 | 0.33 | 34.4 |
| 8 | T1 | 5 | 1.0 | 0.117 | 6.0 | LOS A | 0.5 | 15.8 | 0.46 | 0.33 | 34.3 |
| 18 | R2 | 78 | 23.0 | 0.117 | 6.0 | LOS A | 0.5 | 15.8 | 0.46 | 0.33 | 30.2 |
| Appr |  | 88 | 20.4 | 0.117 | 6.0 | LOS A | 0.5 | 15.8 | 0.46 | 0.33 | 30.7 |
| East: NW 319th St |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 49 | 11.0 | 0.153 | 3.5 | LOS A | 0.8 | 21.8 | 0.07 | 0.01 | 34.2 |
| 6 | T1 | 192 | 2.0 | 0.153 | 3.5 | LOS A | 0.8 | 21.8 | 0.07 | 0.01 | 33.7 |
| 16 | R2 | 146 | 1.0 | 0.108 | 3.5 | LOS A | 0.6 | 14.1 | 0.07 | 0.01 | 32.6 |
| Appr |  | 387 | 2.8 | 0.153 | 3.5 | LOS A | 0.8 | 21.8 | 0.07 | 0.01 | 33.4 |
| North: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 110 | 1.0 | 0.120 | 4.8 | LOS A | 0.6 | 14.2 | 0.41 | 0.27 | 30.2 |
| 4 | T1 | 5 | 1.0 | 0.120 | 4.8 | LOS A | 0.6 | 14.2 | 0.41 | 0.27 | 32.4 |
| 14 | R2 | 1 | 1.0 | 0.120 | 4.8 | LOS A | 0.6 | 14.2 | 0.41 | 0.27 | 30.8 |
| Appr |  | 116 | 1.0 | 0.120 | 4.8 | LOS A | 0.6 | 14.2 | 0.41 | 0.27 | 30.4 |
| West: NW 319th St |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 1 | 1.0 | 0.172 | 5.2 | LOS A | 0.9 | 22.4 | 0.37 | 0.23 | 34.8 |
| 2 | T1 | 155 | 4.0 | 0.172 | 5.2 | LOS A | 0.9 | 22.4 | 0.37 | 0.23 | 32.9 |
| 12 | R2 | 15 | 0.0 | 0.172 | 5.2 | LOS A | 0.9 | 22.4 | 0.37 | 0.23 | 33.9 |
| Approach |  | 171 | 3.6 | 0.172 | 5.2 | LOS A | 0.9 | 22.4 | 0.37 | 0.23 | 33.0 |
| All Vehicles |  | 762 | 4.7 | 0.172 | 4.4 | LOS A | 0.9 | 22.4 | 0.24 | 0.14 | 32.4 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2017 Total Build NW 319 St and NW 31st Ave Weekday AM

## 2017 Total Traffic Weekday AM

Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand <br> Total veh/h | $\begin{aligned} & \text { Flows } \\ & \text { HV } \\ & \% \end{aligned}$ | Cap. veh/h | Deg. Satn v/c | $\begin{aligned} & \text { Lane } \\ & \text { Util. } \\ & \% \\ & \hline \end{aligned}$ | Average Delay sec | Level of Service | 95\% Bac Veh | $\begin{aligned} & \text { ueue } \\ & \text { Dist } \\ & \mathrm{ft} \end{aligned}$ | Lane Config | Lane Length ft | Cap. Adj. \% | Prob. Block. \% |
| South: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 88 | 20.4 | 754 | 0.117 | 100 | 6.0 | LOS A | 0.5 | 15.8 | Full | 1600 | 0.0 | 0.0 |
| Approach | 88 | 20.4 |  | 0.117 |  | 6.0 | LOS A | 0.5 | 15.8 |  |  |  |  |
| East: NW 319th St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 241 | 3.8 | 1578 | 0.153 | 100 | 3.5 | LOS A | 0.8 | 21.8 | Full | 650 | 0.0 | 0.0 |
| Lane 2 | 146 | 1.0 | 1356 | 0.108 | 100 | 3.5 | LOS A | 0.6 | 14.1 | Full | 650 | 0.0 | 0.0 |
| Approach | 387 | 2.8 |  | 0.153 |  | 3.5 | LOS A | 0.8 | 21.8 |  |  |  |  |
| North: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 116 | 1.0 | 966 | 0.120 | 100 | 4.8 | LOS A | 0.6 | 14.2 | Full | 1400 | 0.0 | 0.0 |
| Approach | 116 | 1.0 |  | 0.120 |  | 4.8 | LOS A | 0.6 | 14.2 |  |  |  |  |
| West: NW 319th St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 171 | 3.6 | 997 | 0.172 | 100 | 5.2 | LOS A | 0.9 | 22.4 | Full | 1300 | 0.0 | 0.0 |
| Approach | 171 | 3.6 |  | 0.172 |  | 5.2 | LOS A | 0.9 | 22.4 |  |  |  |  |
| Intersection | 762 | 4.7 |  | 0.172 |  | 4.4 | LOS A | 0.9 | 22.4 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

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SIDRA INTERSECTION 6.0.22.4722 www.sidrasolutions.com
Project: H:\projfile\12393 - Cowlitz Reservation Development\Sidral2014 Analysis $\$
Project: H:\projfile\12393 - Cowlitz Reservation Development\Sidra\2014 Analysis\Interchange Roundabouts\102 NW 319th St and NW 31st Ave\2017 AnalysisINW 319 St and NW 31st Ave.sip6
8001045, KITTELSON AND ASSOCIATES INC, PLUS / Floating

## SITE LAYOUT

Site: 2017 Total Build NW La Center and SB Ramps Weekday AM
2017 Total Traffic Weekday AM
Roundabout


## MOVEMENT SUMMARY

Site: 2017 Total Build NW La Center and SB Ramps Weekday AM

## 2017 Total Traffic Weekday AM

Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \\ \hline \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 535 | 4.0 | 0.314 | 4.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 32.2 |
| 6 | T1 | 361 | 2.0 | 0.245 | 4.5 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 38.5 |
| Appr |  | 896 | 3.2 | 0.314 | 4.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 33.9 |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 118 | 13.0 | 0.269 | 10.4 | LOS B | 1.0 | 26.4 | 0.59 | 0.59 | 26.5 |
| 4 | T1 | 4 | 50.0 | 0.269 | 10.4 | LOS B | 1.0 | 26.4 | 0.59 | 0.59 | 28.7 |
| 14 | R2 | 25 | 8.0 | 0.269 | 10.4 | LOS B | 1.0 | 26.4 | 0.59 | 0.59 | 25.9 |
| Appr |  | 147 | 13.2 | 0.269 | 10.4 | LOS B | 1.0 | 26.4 | 0.59 | 0.59 | 26.5 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 2 | T1 | 118 | 20.0 | 0.172 | 7.2 | LOS A | 0.9 | 26.3 | 0.67 | 0.60 | 29.1 |
| 12 | R2 | 225 | 2.0 | 0.137 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.9 |
| Approach |  | 343 | 8.2 | 0.172 | 2.5 | LOS A | 0.9 | 26.3 | 0.23 | 0.20 | 33.8 |
| All V |  | 1386 | 5.5 | 0.314 | 4.7 | LOS A | 1.0 | 26.4 | 0.12 | 0.11 | 32.8 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2017 Total Build NW La Center and SB Ramps Weekday AM

## 2017 Total Traffic Weekday AM <br> Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \\ \hline \end{gathered}$ | Cap. veh/h | Deg. <br> Satn <br> v/c | Lane Util. $\%$ | Average Delay sec | Level of Service | 95\% Bac Veh | $\begin{aligned} & \text { ueue } \\ & \text { Dist } \\ & \text { ft } \end{aligned}$ | Lane Config | Lane Length ft | $\begin{aligned} & \text { Cap. } \\ & \text { Adj. } \\ & \% \end{aligned}$ | Prob. Block. \% |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 535 | 4.0 | 1706 | 0.314 | 100 | 4.6 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Lane 2 | 361 | 2.0 | 1471 | 0.245 | $78{ }^{5}$ | 4.5 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 896 | 3.2 |  | 0.314 |  | 4.6 | LOS A | 0.0 | 0.0 |  |  |  |  |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 147 | 13.2 | 546 | 0.269 | 100 | 10.4 | LOS B | 1.0 | 26.4 | Full | 1300 | 0.0 | 0.0 |
| Approach | 147 | 13.2 |  | 0.269 |  | 10.4 | LOS B | 1.0 | 26.4 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 118 | 20.0 | 688 | 0.172 | 100 | 7.2 | LOS A | 0.9 | 26.3 | Full | 650 | 0.0 | 0.0 |
| Lane 2 | 225 | 2.0 | 1642 | 0.137 | 100 | 0.0 | LOS A | 0.0 | 0.0 | Short | 200 | 0.0 | 0.0 |
| Approach | 343 | 8.2 |  | 0.172 |  | 2.5 | LOS A | 0.9 | 26.3 |  |  |  |  |
| Intersection | 1386 | 5.5 |  | 0.314 |  | 4.7 | LOS A | 1.0 | 26.4 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
5 Lane underutilisation determined by program
d Dominant lane on roundabout approach

## SITE LAYOUT

Site: 2017 Total Build NW La Center and NB Ramps Weekday AM

## 2017 Total Traffic Weekday AM

Roundabout


## MOVEMENT SUMMARY

Site: 2017 Total Build NW La Center and NB Ramps Weekday AM

## 2017 Total Traffic Weekday AM

Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{array}{r} \text { Flows } \\ \mathrm{HV} \\ \% \\ \hline \end{array}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| South: NB Ramp |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 292 | 1.0 | 0.163 | 5.5 | LOS A | 0.8 | 19.4 | 0.44 | 0.31 | 24.9 |
| 8 | T1 | 4 | 50.0 | 0.163 | 5.6 | LOS A | 0.8 | 19.6 | 0.44 | 0.31 | 29.1 |
| 18 | R2 | 321 | 7.0 | 0.292 | 6.1 | LOS A | 1.6 | 41.8 | 0.46 | 0.33 | 29.7 |
| Appr |  | 617 | 4.4 | 0.292 | 5.8 | LOS A | 1.6 | 41.8 | 0.45 | 0.32 | 27.1 |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 6 | T1 | 604 | 4.0 | 0.563 | 11.2 | LOS B | 3.5 | 91.4 | 0.59 | 0.56 | 21.1 |
| 16 | R2 | 156 | 17.0 | 0.349 | 10.4 | LOS B | 1.5 | 41.7 | 0.54 | 0.52 | 25.7 |
| Appr |  | 760 | 6.7 | 0.563 | 11.0 | LOS B | 3.5 | 91.4 | 0.58 | 0.55 | 22.1 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 77 | 17.0 | 0.167 | 3.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 34.7 |
| 2 | T1 | 159 | 17.0 | 0.167 | 3.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 34.5 |
| Appr |  | 236 | 17.0 | 0.167 | 3.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 34.5 |
| All Ve |  | 1613 | 7.3 | 0.563 | 8.0 | LOS A | 3.5 | 91.4 | 0.44 | 0.38 | 25.7 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2017 Total Build NW La Center and NB Ramps Weekday AM

## 2017 Total Traffic Weekday AM

Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Average Delay sec | Level of Service | $\begin{gathered} 95 \% \text { Bac } \\ \text { Veh } \end{gathered}$ | $\begin{aligned} & \text { ueue } \\ & \text { Dist } \\ & \text { ft } \end{aligned}$ | Lane Config | Lane Length ft | $\begin{aligned} & \text { Cap. } \\ & \text { Adj. } \\ & \% \end{aligned}$ | Prob. Block \% |
| South: NB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 150 | 1.0 | 923 | 0.163 | 100 | 5.5 | LOS A | 0.8 | 19.4 | Full | 1800 | 0.0 | 0.0 |
| Lane 2 | 146 | 2.3 | 898 | 0.163 | 100 | 5.6 | LOS A | 0.8 | 19.6 | Full | 180 | 0.0 | 0.0 |
| Lane $3^{\text {d }}$ | 321 | 7.0 | 1098 | 0.292 | 100 | 6.1 | LOS A | 1.6 | 41.8 | Short | 250 | 0.0 | 0.0 |
| Approach | 617 | 4.4 |  | 0.292 |  | 5.8 | LOS A | 1.6 | 41.8 |  |  |  |  |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 538 | 4.0 | 956 | 0.563 | 100 | 11.3 | LOS B | 3.5 | 91.4 | Full | 600 | 0.0 | 0.0 |
| Lane 2 | 222 | 13.1 | 637 | 0.349 | $62^{7}$ | 10.4 | LOS B | 1.5 | 41.7 | Full | 600 | 0.0 | 0.0 |
| Approach | 760 | 6.7 |  | 0.563 |  | 11.0 | LOS B | 3.5 | 91.4 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 236 | 17.0 | 1413 | 0.167 | 100 | 3.9 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 236 | 17.0 |  | 0.167 |  | 3.9 | LOS A | 0.0 | 0.0 |  |  |  |  |
| Intersection | 1613 | 7.3 |  | 0.563 |  | 8.0 | LOS A | 3.5 | 91.4 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
7 Lane underutilisation specified by user
d Dominant lane on roundabout approach

| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 5.2 |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 91 | 384 | 5 | 10 | 628 | 9 | 10 | 0 | 5 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | 250 | - | - | 200 | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 42 | 13 | 0 | 25 | 3 | 20 | 14 | 0 | 25 |
| Mvmt Flow | 91 | 384 | 5 | 10 | 628 | 9 | 10 | 0 | 5 |
| Major/Minor | Major1 |  |  | Major2 |  |  | Minor1 |  |  |
| Conflicting Flow All | 637 | 0 | 0 | 389 | 0 | 0 | 1256 | 1226 | 387 |
| Stage 1 | - | - | - | - | - | - | 569 | 569 |  |
| Stage 2 | - | - | - | - | - | - | 687 | 657 |  |
| Critical Hdwy | 4.52 | - | - | 4.35 | - | - | 7.24 | 6.5 | 6.45 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.24 | 5.5 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.24 | 5.5 |  |
| Follow-up Hdwy | 2.578 | - | - | 2.425 | - | - | 3.626 | 4 | 3.525 |
| Pot Cap-1 Maneuver | 782 | - | - | 1055 | - | - | 140 | 180 | 613 |
| Stage 1 | - | - | - | - | - | - | 486 | 509 | - |
| Stage 2 | - | - | - | - | - | - | 418 | 465 | - |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 782 | - | - | 1055 | - | - | 104 | 158 | 613 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 104 | 158 |  |
| Stage 1 | - | - | - | - | - | - | 429 | 450 |  |
| Stage 2 | - | - | - | - | - | - | 348 | 461 |  |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 1.9 | 0.1 | 32.9 |
| HCM LOS |  |  | D |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 144 | 782 | - | - | 1055 | - | - | 190 |
| HCM Lane V/C Ratio | 0.104 | 0.116 | - | - | 0.009 | - | - | 0.568 |
| HCM Control Delay (s) | 32.9 | 10.2 | - | - | 8.4 | - | - | 46.3 |
| HCM Lane LOS | D | B | - | - | A | - | - | E |
| HCM 95th \%tile Q(veh) | 0.3 | 0.4 | - | - | 0 | - | - | 3 |


| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | 39 | 4 | 65 |
| Vol, veh/h | SBT | SBR |  |
| Conflicting Peds, \#/hr | Stop | Stop | Stop |
| Sign Control | - | - | None |
| RT Channelized | - | - | - |
| Storage Length | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | 100 | 100 | 100 |
| Peak Hour Factor | 69 | 100 | 30 |
| Heavy Vehicles, \% | 39 | 4 | 65 |
| Mvmt Flow |  |  |  |


|  | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Major/Minor | 1224 | 1224 | 633 |
| Conflicting Flow All | 653 | 653 | - |
| Stage 1 | 571 | 571 | - |
| Stage 2 | 7.79 | 7.5 | 6.5 |
| Critical Hdwy | 6.79 | 6.5 | - |
| Critical Hdwy Stg 1 | 6.79 | 6.5 | - |
| Critical Hdwy Stg 2 | 4.121 | 4.9 | 3.57 |
| Follow-up Hdwy | 115 | 118 | 433 |
| Pot Cap-1 Maneuver | 362 | 341 | - |
| Stage 1 | 405 | 377 | - |
| Stage 2 |  |  |  |
| Platoon blocked, \% | 103 | 103 | 433 |
| Mov Cap-1 Maneuver | 103 | 103 | - |
| Mov Cap-2 Maneuver | 320 | 338 | - |
| Stage 1 | 355 | 333 | - |
| Stage 2 |  |  |  |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | 46.3 |
| HCM LOS | E |

[^27]
## SITE LAYOUT

Site: 2017 Total Build NW 319 St and NW 31st Ave Weekday AM 85/15 Split
2017 Total Traffic Weekday AM
85/15 Split Sensitivity Analysis
Roundabout


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Project: H:\projfile\12393 - Cowlitz Reservation Development\Sidra\2014 Analysis\Interchange Roundabouts\102 NW 319th St and NW 31st Avel2017 AnalysisINW 319 St and NW 31st Ave 85_15.sip6 8001045, KITTELSON AND ASSOCIATES INC, PLUS / Floating

## MOVEMENT SUMMARY

Site: 2017 Total Build NW 319 St and NW 31st Ave Weekday PM
2017 Total Traffic Weekday PM
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \hline \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue <br> Distance <br> ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| South: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 17 | 0.0 | 0.211 | 8.9 | LOS A | 1.2 | 30.8 | 0.73 | 0.68 | 32.6 |
| 8 | T1 | 10 | 10.0 | 0.211 | 8.9 | LOS A | 1.2 | 30.8 | 0.73 | 0.68 | 32.5 |
| 18 | R2 | 96 | 7.0 | 0.211 | 8.9 | LOS A | 1.2 | 30.8 | 0.73 | 0.68 | 29.2 |
| Appr |  | 123 | 6.3 | 0.211 | 8.9 | LOS A | 1.2 | 30.8 | 0.73 | 0.68 | 30.0 |
| East: NW 319th St |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 97 | 2.0 | 0.378 | 5.8 | LOS A | 2.9 | 77.6 | 0.18 | 0.06 | 33.0 |
| 6 | T1 | 464 | 9.0 | 0.378 | 5.8 | LOS A | 2.9 | 77.6 | 0.18 | 0.06 | 31.8 |
| 16 | R2 | 377 | 1.0 | 0.280 | 5.1 | LOS A | 1.9 | 47.5 | 0.17 | 0.05 | 31.5 |
| Appr |  | 938 | 5.1 | 0.378 | 5.5 | LOS A | 2.9 | 77.6 | 0.18 | 0.06 | 31.8 |
| North: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 308 | 1.0 | 0.450 | 11.4 | LOS B | 3.0 | 75.8 | 0.75 | 0.76 | 26.8 |
| 4 | T1 | 10 | 10.0 | 0.450 | 11.4 | LOS B | 3.0 | 75.8 | 0.75 | 0.76 | 29.4 |
| 14 | R2 | 1 | 0.0 | 0.450 | 11.4 | LOS B | 3.0 | 75.8 | 0.75 | 0.76 | 28.0 |
| Appr |  | 319 | 1.3 | 0.450 | 11.4 | LOS B | 3.0 | 75.8 | 0.75 | 0.76 | 26.9 |
| West: NW 319th St |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 1 | 0.0 | 0.495 | 11.5 | LOS B | 3.6 | 92.3 | 0.73 | 0.67 | 31.4 |
| 2 | T1 | 381 | 3.0 | 0.495 | 11.5 | LOS B | 3.6 | 92.3 | 0.73 | 0.67 | 28.8 |
| 12 | R2 | 5 | 0.0 | 0.495 | 11.5 | LOS B | 3.6 | 92.3 | 0.73 | 0.67 | 30.7 |
| Approach |  | 387 | 3.0 | 0.495 | 11.5 | LOS B | 3.6 | 92.3 | 0.73 | 0.67 | 28.9 |
| All Vehicles |  | 1767 | 4.0 | 0.495 | 8.1 | LOS A | 3.6 | 92.3 | 0.44 | 0.36 | 30.0 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements ( $\mathrm{v} / \mathrm{c}$ not used as specified in HCM 2010). Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2017 Total Build NW 319 St and NW 31st Ave Weekday PM

## 2017 Total Traffic Weekday PM

Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Cap. veh/h | Deg. Satn v/c | $\begin{aligned} & \text { Lane } \\ & \text { Util. } \\ & \% \\ & \hline \end{aligned}$ | Average Delay sec | Level of Service | 95\% Bac Veh | $\begin{aligned} & \text { Deue } \\ & \text { Dist } \\ & \text { ft } \end{aligned}$ | Lane Config | Lane Length ft | Cap. Adj. \% | Prob. Block. \% |
| South: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 123 | 6.3 | 582 | 0.211 | 100 | 8.9 | LOS A | 1.2 | 30.8 | Full | 1600 | 0.0 | 0.0 |
| Approach | 123 | 6.3 |  | 0.211 |  | 8.9 | LOS A | 1.2 | 30.8 |  |  |  |  |
| East: NW 319th St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 561 | 7.8 | 1484 | 0.378 | 100 | 5.8 | LOS A | 2.9 | 77.6 | Full | 650 | 0.0 | 0.0 |
| Lane 2 | 377 | 1.0 | 1348 | 0.280 | 100 | 5.1 | LOS A | 1.9 | 47.5 | Full | 650 | 0.0 | 0.0 |
| Approach | 938 | 5.1 |  | 0.378 |  | 5.5 | LOS A | 2.9 | 77.6 |  |  |  |  |
| North: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 319 | 1.3 | 709 | 0.450 | 100 | 11.4 | LOS B | 3.0 | 75.8 | Full | 1400 | 0.0 | 0.0 |
| Approach | 319 | 1.3 |  | 0.450 |  | 11.4 | LOS B | 3.0 | 75.8 |  |  |  |  |
| West: NW 319th St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 387 | 3.0 | 783 | 0.495 | 100 | 11.5 | LOS B | 3.6 | 92.3 | Full | 1300 | 0.0 | 0.0 |
| Approach | 387 | 3.0 |  | 0.495 |  | 11.5 | LOS B | 3.6 | 92.3 |  |  |  |  |
| Intersection | 1767 | 4.0 |  | 0.495 |  | 8.1 | LOS A | 3.6 | 92.3 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
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Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

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## SITE LAYOUT

Site: 2017 Total Build NW La Center and SB Ramps Weekday AM
2017 Total Traffic Weekday AM
Roundabout


## MOVEMENT SUMMARY

Site: 2017 Total Build NW La Center and SB Ramps Weekday PM

## 2017 Total Traffic Weekday PM <br> Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dem Total veh/h | Flows HV $\%$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles veh | Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 374 | 5.0 | 0.373 | 5.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 33.7 |
| 6 | T1 | 824 | 2.0 | 0.373 | 5.3 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 37.1 |
| Appr |  | 1198 | 2.9 | 0.373 | 5.4 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.7 |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 165 | 10.0 | 0.531 | 16.8 | LOS B | 2.6 | 67.8 | 0.72 | 0.81 | 24.2 |
| 4 | T1 | 4 | 50.0 | 0.531 | 16.8 | LOS B | 2.6 | 67.8 | 0.72 | 0.81 | 26.6 |
| 14 | R2 | 114 | 2.0 | 0.531 | 16.8 | LOS B | 2.6 | 67.8 | 0.72 | 0.81 | 23.8 |
| Approach |  | 283 | 7.3 | 0.531 | 16.8 | LOS B | 2.6 | 67.8 | 0.72 | 0.81 | 24.1 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 2 | T1 | 185 | 7.0 | 0.214 | 6.4 | LOS A | 1.2 | 32.0 | 0.64 | 0.54 | 30.5 |
| 12 | R2 | 600 | 1.0 | 0.362 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.9 |
| Appr |  | 785 | 2.4 | 0.362 | 1.5 | LOS A | 1.2 | 32.0 | 0.15 | 0.13 | 34.8 |
| All V |  | 2266 | 3.3 | 0.531 | 5.5 | LOS A | 2.6 | 67.8 | 0.14 | 0.14 | 33.0 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
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HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2017 Total Build NW La Center and SB Ramps Weekday PM

## 2017 Total Traffic Weekday PM <br> Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand <br> Total veh/h | $\begin{array}{r} \text { lows } \\ \text { HV } \\ \% \\ \hline \end{array}$ | Cap. veh/h | Deg. <br> Satn <br> v/c | Lane Util. \% | Average Delay sec | Level of Service | 95\% Bac <br> Veh | ueue Dist ft | Lane Config | Lane Length ft | $\begin{aligned} & \text { Cap. } \\ & \text { Adj. } \\ & \% \end{aligned}$ | Prob. Block. \% |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 550 | 4.0 | 1474 | 0.373 | 100 | 5.8 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 648 | 2.0 | 1739 | 0.373 | 100 | 5.2 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 1198 | 2.9 |  | 0.373 |  | 5.4 | LOS A | 0.0 | 0.0 |  |  |  |  |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 283 | 7.3 | 533 | 0.531 | 100 | 16.8 | LOS B | 2.6 | 67.8 | Full | 1300 | 0.0 | 0.0 |
| Approach | 283 | 7.3 |  | 0.531 |  | 16.8 | LOS B | 2.6 | 67.8 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 185 | 7.0 | 864 | 0.214 | 100 | 6.4 | LOS A | 1.2 | 32.0 | Full | 650 | 0.0 | 0.0 |
| Lane 2 | 600 | 1.0 | 1658 | 0.362 | 100 | 0.0 | LOS A | 0.0 | 0.0 | Short | 200 | 0.0 | 0.0 |
| Approach | 785 | 2.4 |  | 0.362 |  | 1.5 | LOS A | 1.2 | 32.0 |  |  |  |  |
| Intersection | 2266 | 3.3 |  | 0.531 |  | 5.5 | LOS A | 2.6 | 67.8 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

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NW La Center and SB Ramps\2017 Analysis\103 NW La Center and SB Ramps.sip6
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## SITE LAYOUT

Site: 2017 Total Build NW La Center and NB Ramps Weekday AM

## 2017 Total Traffic Weekday AM

Roundabout


## MOVEMENT SUMMARY

Site: 2017 Total Build NW La Center and NB Ramps Weekday PM
2017 Total Traffic Weekday PM
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{gathered} \text { =lows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles $\qquad$ | Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| South: NB Ramp |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 747 | 1.0 | 0.407 | 8.6 | LOS A | 2.4 | 60.3 | 0.59 | 0.49 | 23.9 |
| 8 | T1 | 8 | 50.0 | 0.407 | 8.6 | LOS A | 2.4 | 60.6 | 0.59 | 0.49 | 27.9 |
| 18 | R2 | 591 | 3.0 | 0.543 | 9.9 | LOS A | 4.0 | 102.7 | 0.64 | 0.54 | 27.9 |
| Appr |  | 1346 | 2.2 | 0.543 | 9.1 | LOS A | 4.0 | 102.7 | 0.61 | 0.51 | 25.5 |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 6 | T1 | 451 | 4.0 | 0.503 | 12.0 | LOS B | 2.8 | 71.1 | 0.69 | 0.73 | 20.7 |
| 16 | R2 | 119 | 5.0 | 0.342 | 11.0 | LOS B | 1.5 | 38.4 | 0.65 | 0.66 | 25.6 |
| Appr |  | 570 | 4.2 | 0.503 | 11.8 | LOS B | 2.8 | 71.1 | 0.69 | 0.71 | 21.8 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 69 | 4.0 | 0.229 | 4.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.8 |
| 2 | T1 | 281 | 9.0 | 0.229 | 4.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 36.0 |
| Approach |  | 350 | 8.0 | 0.229 | 4.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.9 |
| All Vehicles |  | 2266 | 3.6 | 0.543 | 9.1 | LOS A | 4.0 | 102.7 | 0.54 | 0.48 | 25.5 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2017 Total Build NW La Center and NB Ramps Weekday PM

## 2017 Total Traffic Weekday PM <br> Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \\ & \hline \end{aligned}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Average Delay $\qquad$ sec | Level of Service | $\begin{gathered} 95 \% \mathrm{Ba} \\ \text { Veh } \end{gathered}$ | $\begin{array}{r} \text { Queue } \\ \text { Dist } \\ \mathrm{ft} \end{array}$ | Lane Config | Lane Length ft | $\begin{aligned} & \text { Cap. } \\ & \text { Adj. } \\ & \% \end{aligned}$ | Prob. Block. $\qquad$ \% |
| South: NB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 381 | 1.0 | 937 | 0.407 | 100 | 8.5 | LOS A | 2.4 | 60.3 | Full | 1800 | 0.0 | 0.0 |
| Lane 2 | 374 | 2.0 | 918 | 0.407 | 100 | 8.6 | LOS A | 2.4 | 60.6 | Full | 1800 | 0.0 | 0.0 |
| Lane $3^{\text {d }}$ | 591 | 3.0 | 1088 | 0.543 | 100 | 9.9 | LOS A | 4.0 | 102.7 | Short | 250 | 0.0 | 0.0 |
| Approach | 1346 | 2.2 |  | 0.543 |  | 9.1 | LOS A | 4.0 | 102.7 |  |  |  |  |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 369 | 4.0 | 733 | 0.503 | 100 | 12.3 | LOS B | 2.8 | 71.1 | Full | 600 | 0.0 | 0.0 |
| Lane 2 | 201 | 4.6 | 589 | 0.342 | $68^{7}$ | 11.0 | LOS B | 1.5 | 38.4 | Full | 600 | 0.0 | 0.0 |
| Approach | 570 | 4.2 |  | 0.503 |  | 11.8 | LOS B | 2.8 | 71.1 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 350 | 8.0 | 1531 | 0.229 | 100 | 4.2 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 350 | 8.0 |  | 0.229 |  | 4.2 | LOS A | 0.0 | 0.0 |  |  |  |  |
| Intersection | 2266 | 3.6 |  | 0.543 |  | 9.1 | LOS A | 4.0 | 102.7 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
7 Lane underutilisation specified by user
d Dominant lane on roundabout approach

| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 3.3 |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 114 | 745 | 12 | 5 | 460 | 8 | 5 | 0 | 5 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | 250 | - | - | 200 | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 21 | 4 | 25 | 25 | 2 | 20 | 0 | 0 | 0 |
| Mvmt Flow | 114 | 745 | 12 | 5 | 460 | 8 | 5 | 0 | 5 |
| Major/Minor | Major1 |  |  | Major2 |  |  | Minor1 |  |  |
| Conflicting Flow All | 468 | 0 | 0 | 757 | 0 | 0 | 1483 | 1457 | 751 |
| Stage 1 | - | - | - | - | - | - | 979 | 979 |  |
| Stage 2 | - | - | - | - | - | - | 504 | 478 |  |
| Critical Hdwy | 4.31 | - | - | 4.35 | - | - | 7.1 | 6.5 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.5 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.1 | 5.5 |  |
| Follow-up Hdwy | 2.389 | - | - | 2.425 | - | - | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1001 | - | - | 759 | - | - | 104 | 131 | 414 |
| Stage 1 | - | - | - | - | - | - | 304 | 331 |  |
| Stage 2 | - | - | - | - | - | - | 554 | 559 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1001 | - | - | 759 | - | - | 83 | 115 | 414 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 83 | 115 |  |
| Stage 1 | - | - | - | - | - | - | 269 | 293 |  |
| Stage 2 |  | - | - | - | - | - | 493 | 555 |  |


| Approach | EB | WB | NB |
| :--- | :--- | :---: | :---: |
| HCM Control Delay, s | 1.2 | 0.1 | 33.1 |
| HCM LOS |  | D |  |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 138 | 1001 | - | - | 759 | - | - | 197 |
| HCM Lane V/C Ratio | 0.072 | 0.114 | - | - | 0.007 | - | - | 0.452 |
| HCM Control Delay (s) | 33.1 | 9.1 | - | - | 9.8 | - | - | 37.5 |
| HCM Lane LOS | D | A | - | - | A | - | - | E |
| HCM 95th \%tile Q(veh) | 0.2 | 0.4 | - | - | 0 | - | - | 2.1 |


| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | 30 | 4 | 55 |
| Vol, veh/h | SBT | SBR |  |
| Conflicting Peds, \#/hr | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | - | - | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 |
| Heavy Vehicles, \% | 7 | 0 | 17 |
| Mvmt Flow | 30 | 4 | 55 |
|  |  |  |  |


| Major/Minor | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Conflicting Flow All | 1456 | 1459 | 464 |
| Stage 1 | 474 | 474 | - |
| Stage 2 | 982 | 985 | - |
| Critical Hdwy | 7.17 | 6.5 | 6.37 |
| Critical Hdwy Stg 1 | 6.17 | 5.5 | - |
| Critical Hdwy Stg 2 | 6.17 | 5.5 | - |
| Follow-up Hdwy | 3.563 | 4 | 3.453 |
| Pot Cap-1 Maneuver | 105 | 131 | 568 |
| Stage 1 | 562 | 561 | - |
| Stage 2 | 294 | 329 | - |
| Platoon blocked, \% | 94 | 115 | 568 |
| Mov Cap-1 Maneuver | 94 | 115 | - |
| Mov Cap-2 Maneuver | 498 | 557 | - |
| Stage 1 | 257 | 292 | - |
| Stage 2 |  |  |  |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | 37.5 |
| HCM LOS | E |

## Minor Lane/Major Mvmt

## SITE LAYOUT

## Site: 2017 Total Build NW 319 St and NW 31st Ave Weekday AM

2017 Total Traffic Weekday AM
Roundabout


## MOVEMENT SUMMARY

Site: 2017 Total Build NW 319 St and NW 31st Ave Weekend Peak

## 2017 Total Traffic Weekend Peak

Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| South: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 5 | 25.0 | 0.150 | 8.1 | LOS A | 0.8 | 21.3 | 0.73 | 0.65 | 30.4 |
| 8 | T1 | 15 | 1.0 | 0.150 | 8.1 | LOS A | 0.8 | 21.3 | 0.73 | 0.65 | 33.3 |
| 18 | R2 | 66 | 4.0 | 0.150 | 8.1 | LOS A | 0.8 | 21.3 | 0.73 | 0.65 | 30.1 |
| Appr |  | 86 | 4.7 | 0.150 | 8.1 | LOS A | 0.8 | 21.3 | 0.73 | 0.65 | 30.8 |
| East: NW 319th St |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 77 | 6.0 | 0.395 | 5.7 | LOS A | 3.2 | 80.6 | 0.16 | 0.04 | 33.1 |
| 6 | T1 | 553 | 2.0 | 0.395 | 5.7 | LOS A | 3.2 | 80.6 | 0.16 | 0.04 | 32.3 |
| 16 | R2 | 493 | 1.0 | 0.350 | 5.7 | LOS A | 2.6 | 65.3 | 0.16 | 0.04 | 31.1 |
| Appr |  | 1123 | 1.8 | 0.395 | 5.7 | LOS A | 3.2 | 80.6 | 0.16 | 0.04 | 31.8 |
| North: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 329 | 1.0 | 0.487 | 12.4 | LOS B | 3.5 | 88.1 | 0.78 | 0.81 | 26.3 |
| 4 | T1 | 10 | 1.0 | 0.487 | 12.4 | LOS B | 3.5 | 88.1 | 0.78 | 0.81 | 29.2 |
| 14 | R2 | 1 | 1.0 | 0.487 | 12.4 | LOS B | 3.5 | 88.1 | 0.78 | 0.81 | 27.6 |
| Appr |  | 340 | 1.0 | 0.487 | 12.4 | LOS B | 3.5 | 88.1 | 0.78 | 0.81 | 26.4 |
| West: NW 319th St |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 1 | 1.0 | 0.526 | 12.4 | LOS B | 4.1 | 105.2 | 0.76 | 0.72 | 30.8 |
| 2 | T1 | 387 | 4.0 | 0.526 | 12.4 | LOS B | 4.1 | 105.2 | 0.76 | 0.72 | 28.2 |
| 12 | R2 | 15 | 0.0 | 0.526 | 12.4 | LOS B | 4.1 | 105.2 | 0.76 | 0.72 | 30.3 |
| Approach |  | 403 | 3.8 | 0.526 | 12.4 | LOS B | 4.1 | 105.2 | 0.76 | 0.72 | 28.3 |
| All Vehicles |  | 1952 | 2.2 | 0.526 | 8.4 | LOS A | 4.1 | 105.2 | 0.41 | 0.34 | 29.9 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement LOS $F$ will result if $v / c>1$ irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D). HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^28]
## LANE SUMMARY

## Site: 2017 Total Build NW 319 St and NW 31st Ave Weekend Peak

## 2017 Total Traffic Weekend Peak

Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Cap. veh/h | Deg. Satn v/c | $\begin{aligned} & \text { Lane } \\ & \text { Util. } \\ & \% \end{aligned}$ | Average Delay sec | Level of Service | 95\% Bac Veh | Queue Dist Dist | Lane Config | Lane Length ft | Cap. Adj. \% | Prob. Block. \% |
| South: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 86 | 4.7 | 574 | 0.150 | 100 | 8.1 | LOS A | 0.8 | 21.3 | Full | 1600 | 0.0 | 0.0 |
| Approach | 86 | 4.7 |  | 0.150 |  | 8.1 | LOS A | 0.8 | 21.3 |  |  |  |  |
| East: NW 319th St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 630 | 2.5 | 1595 | 0.395 | 100 | 5.7 | LOS A | 3.2 | 80.6 | Full | 650 | 0.0 | 0.0 |
| Lane 2 | 493 | 1.0 | 1409 | 0.350 | 100 | 5.7 | LOS A | 2.6 | 65.3 | Full | 650 | 0.0 | 0.0 |
| Approach | 1123 | 1.8 |  | 0.395 |  | 5.7 | LOS A | 3.2 | 80.6 |  |  |  |  |
| North: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 340 | 1.0 | 698 | 0.487 | 100 | 12.4 | LOS B | 3.5 | 88.1 | Full | 1400 | 0.0 | 0.0 |
| Approach | 340 | 1.0 |  | 0.487 |  | 12.4 | LOS B | 3.5 | 88.1 |  |  |  |  |
| West: NW 319th St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 403 | 3.8 | 767 | 0.526 | 100 | 12.4 | LOS B | 4.1 | 105.2 | Full | 1300 | 0.0 | 0.0 |
| Approach | 403 | 3.8 |  | 0.526 |  | 12.4 | LOS B | 4.1 | 105.2 |  |  |  |  |
| Intersection | 1952 | 2.2 |  | 0.526 |  | 8.4 | LOS A | 4.1 | 105.2 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes ( $\mathrm{v} / \mathrm{c}$ not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

Processed: Friday, August 29, 2014 11:54:13 AM SIDRA INTERSECTION 6.0.22.4722 www.sidrasolutions.com
Project: H:\projfile\12393 - Cowlitz Reservation Development\Sidra\2014 Analysis\Interchange Roundabouts\102 NW 319th St and NW 31st Avel2017 Analysis\NW 319 St and NW 31st Ave.sip6 8001045, KITTELSON AND ASSOCIATES INC, PLUS / Floating

## SITE LAYOUT

Site: 2017 Total Build NW La Center and SB Ramps Weekday AM
2017 Total Traffic Weekday AM
Roundabout


## MOVEMENT SUMMARY

Site: 2017 Total Build NW La Center and SB Ramps Weekend

## 2017 Total Traffic Weekend Peak

Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \\ & \hline \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles veh | Queue <br> Distance $\qquad$ | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 375 | 2.0 | 0.415 | 6.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 34.7 |
| 6 | T1 | 982 | 1.0 | 0.415 | 5.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 37.2 |
| Appr |  | 1357 | 1.3 | 0.415 | 5.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 36.2 |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 172 | 4.0 | 0.609 | 20.2 | LOS C | 3.3 | 85.3 | 0.78 | 0.90 | 23.1 |
| 4 | T1 | 4 | 0.0 | 0.609 | 20.2 | LOS C | 3.3 | 85.3 | 0.78 | 0.90 | 25.9 |
| 14 | R2 | 141 | 8.0 | 0.609 | 20.2 | LOS C | 3.3 | 85.3 | 0.78 | 0.90 | 22.4 |
| Appr |  | 317 | 5.7 | 0.609 | 20.2 | LOS C | 3.3 | 85.3 | 0.78 | 0.90 | 22.8 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 2 | T1 | 146 | 3.0 | 0.159 | 5.5 | LOS A | 0.9 | 22.7 | 0.61 | 0.49 | 31.6 |
| 12 | R2 | 636 | 2.0 | 0.387 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.9 |
| Appr |  | 782 | 2.2 | 0.387 | 1.0 | LOS A | 0.9 | 22.7 | 0.11 | 0.09 | 35.2 |
| All V |  | 2456 | 2.1 | 0.609 | 6.2 | LOS A | 3.3 | 85.3 | 0.14 | 0.14 | 32.9 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2017 Total Build NW La Center and SB Ramps Weekend

## 2017 Total Traffic Weekend Peak <br> Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{array}{r} \text { lows } \\ \text { HV } \\ \% \\ \hline \end{array}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. $\%$ | Average Delay sec | Level of Service | 95\% Ba <br> Veh | $\begin{array}{r} \text { ueue } \\ \text { Dist } \\ \text { ft } \end{array}$ | Lane Config | Lane Length ft | $\begin{aligned} & \text { Cap. } \\ & \text { Adj. } \\ & \% \end{aligned}$ | Prob. Block. \% |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 628 | 1.6 | 1511 | 0.415 | 100 | 6.1 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 729 | 1.0 | 1757 | 0.415 | 100 | 5.6 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 1357 | 1.3 |  | 0.415 |  | 5.8 | LOS A | 0.0 | 0.0 |  |  |  |  |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 317 | 5.7 | 520 | 0.609 | 100 | 20.2 | LOS C | 3.3 | 85.3 | Full | 1300 | 0.0 | 0.0 |
| Approach | 317 | 5.7 |  | 0.609 |  | 20.2 | LOS C | 3.3 | 85.3 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 146 | 3.0 | 917 | 0.159 | 100 | 5.5 | LOS A | 0.9 | 22.7 | Full | 650 | 0.0 | 0.0 |
| Lane 2 | 636 | 2.0 | 1642 | 0.387 | 100 | 0.0 | LOS A | 0.0 | 0.0 | Short | 200 | 0.0 | 0.0 |
| Approach | 782 | 2.2 |  | 0.387 |  | 1.0 | LOS A | 0.9 | 22.7 |  |  |  |  |
| Intersection | 2456 | 2.1 |  | 0.609 |  | 6.2 | LOS A | 3.3 | 85.3 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

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## SITE LAYOUT

Site: 2017 Total Build NW La Center and NB Ramps Weekday AM

## 2017 Total Traffic Weekday AM

Roundabout


## MOVEMENT SUMMARY

Site: 2017 Total Build NW La Center and NB Ramps Weekend

## 2017 Total Traffic Weekend Peak

Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{gathered} =\text { lows } \\ \text { HV } \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles veh | Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| South: NB Ramp |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 927 | 1.0 | 0.452 | 8.6 | LOS A | 2.8 | 71.0 | 0.57 | 0.45 | 22.0 |
| 8 | T1 | 4 | 0.0 | 0.452 | 8.6 | LOS A | 2.8 | 71.0 | 0.57 | 0.45 | 28.1 |
| 18 | R2 | 564 | 3.0 | 0.501 | 8.9 | LOS A | 3.3 | 85.4 | 0.59 | 0.46 | 28.4 |
| Appr |  | 1495 | 1.8 | 0.501 | 8.7 | LOS A | 3.3 | 85.4 | 0.58 | 0.46 | 24.0 |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 6 | T1 | 430 | 3.0 | 0.546 | 14.2 | LOS B | 3.1 | 79.8 | 0.74 | 0.79 | 19.8 |
| 16 | R2 | 124 | 12.0 | 0.382 | 14.1 | LOS B | 1.7 | 45.1 | 0.70 | 0.73 | 23.8 |
| Approach |  | 554 | 5.0 | 0.546 | 14.2 | LOS B | 3.1 | 79.8 | 0.73 | 0.78 | 20.7 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 74 | 1.0 | 0.200 | 3.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.7 |
| 2 | T1 | 244 | 5.0 | 0.200 | 3.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 36.0 |
| Appr |  | 318 | 4.1 | 0.200 | 3.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.9 |
| All Ve |  | 2367 | 2.8 | 0.546 | 9.3 | LOS A | 3.3 | 85.4 | 0.54 | 0.47 | 24.1 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2017 Total Build NW La Center and NB Ramps Weekend

## 2017 Total Traffic Weekend Peak <br> Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \\ & \hline \end{aligned}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Average Delay sec | Level of Service | $\begin{gathered} 95 \% \mathrm{Ba} \\ \text { Veh } \end{gathered}$ | $\begin{aligned} & \text { ueue } \\ & \text { Dist } \\ & \text { ft } \end{aligned}$ | Lane Config | Lane Length ft | $\begin{aligned} & \text { Cap. } \\ & \text { Adj. } \\ & \% \end{aligned}$ | Prob. Block. $\qquad$ \% |
| South: NB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 465 | 1.0 | 1030 | 0.452 | 100 | 8.6 | LOS A | 2.8 | 71.0 | Full | 1800 | 0.0 | 0.0 |
| Lane 2 | 466 | 1.0 | 1030 | 0.452 | 100 | 8.6 | LOS A | 2.8 | 71.0 | Full | 1800 | 0.0 | 0.0 |
| Lane $3^{\text {d }}$ | 564 | 3.0 | 1126 | 0.501 | 100 | 8.9 | LOS A | 3.3 | 85.4 | Short | 250 | 0.0 | 0.0 |
| Approach | 1495 | 1.8 |  | 0.501 |  | 8.7 | LOS A | 3.3 | 85.4 |  |  |  |  |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 373 | 3.0 | 682 | 0.546 | 100 | 14.2 | LOS B | 3.1 | 79.8 | Full | 600 | 0.0 | 0.0 |
| Lane 2 | 181 | 9.2 | 474 | 0.382 | $70^{7}$ | 14.1 | LOS B | 1.7 | 45.1 | Full | 600 | 0.0 | 0.0 |
| Approach | 554 | 5.0 |  | 0.546 |  | 14.2 | LOS B | 3.1 | 79.8 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 318 | 4.1 | 1589 | 0.200 | 100 | 3.8 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 318 | 4.1 |  | 0.200 |  | 3.8 | LOS A | 0.0 | 0.0 |  |  |  |  |
| Intersection | 2367 | 2.8 |  | 0.546 |  | 9.3 | LOS A | 3.3 | 85.4 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
7 Lane underutilisation specified by user
d Dominant lane on roundabout approach

| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 2.8 |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 82 | 721 | 5 | 5 | 455 | 8 | 10 | 5 | 5 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | 250 | - | - | 200 | - | - | - |  |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 13 | 4 | 17 | 0 | 3 | 17 | 11 | 0 | 50 |
| Mumt Flow | 82 | 721 | 5 | 5 | 455 | 8 | 10 | 5 | 5 |
| Major/Minor | Major1 |  |  | Major2 |  |  | Minor1 |  |  |
| Conflicting Flow All | 463 | 0 | 0 | 726 | 0 | 0 | 1376 | 1361 | 724 |
| Stage 1 | - | - | - | - | - | - | 888 | 888 |  |
| Stage 2 | - | - | - | - | - | - | 488 | 473 |  |
| Critical Hdwy | 4.23 | - | - | 4.1 | - | - | 7.21 | 6.5 | 6.7 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.21 | 5.5 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.21 | 5.5 |  |
| Follow-up Hdwy | 2.317 | - | - | 2.2 | - | - | 3.599 | 4 | 3.75 |
| Pot Cap-1 Maneuver | 1043 | - | - | 886 | - | - | 117 | 150 | 355 |
| Stage 1 | - | - | - | - | - | - | 326 | 365 |  |
| Stage 2 | - | - | - | - | - | - | 545 | 562 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1043 | - | - | 886 | - | - | 101 | 137 | 355 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 101 | 137 |  |
| Stage 1 | - | - | - | - | - | - | 300 | 336 |  |
| Stage 2 |  | - | - | - | - | - | 507 | 559 |  |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0.9 | 0.1 | 36.5 |
| HCM LOS |  |  | E |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 134 | 1043 | - | - | 886 | - | - | 191 |
| HCM Lane V/C Ratio | 0.149 | 0.079 | - | - | 0.006 | - | - | 0.351 |
| HCM Control Delay (s) | 36.5 | 8.7 | - | - | 9.1 | - | - | 33.7 |
| HCM Lane LOS | E | A | - | - | A | - | - | D |
| HCM 95th \%tile Q(veh) | 0.5 | 0.3 | - | - | 0 | - | - | 1.5 |


| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | 30 | 4 | 33 |
| Vol, veh/h | SBT | SBR |  |
| Conflicting Peds, \#/hr | Stop | Stop | Stop |
| Sign Control | - | - | None |
| RT Channelized | - | - | - |
| Storage Length | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | 100 | 100 | 100 |
| Peak Hour Factor | 0 | 0 | 13 |
| Heavy Vehicles, \% | 30 | 4 | 33 |
| Mvmt Flow |  |  |  |


| Major/Minor | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Conflicting Flow All | 1362 | 1359 | 459 |
| Stage 1 | 469 | 469 | - |
| Stage 2 | 893 | 890 | - |
| Critical Hdwy | 7.1 | 6.5 | 6.33 |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - |
| Follow-up Hdwy | 3.5 | 4 | 3.417 |
| Pot Cap-1 Maneuver | 126 | 150 | 580 |
| Stage 1 | 579 | 564 | - |
| Stage 2 | 339 | 364 | - |
| Platoon blocked, \% |  |  |  |
| Mov Cap-1 Maneuver | 113 | 137 | 580 |
| Mov Cap-2 Maneuver | 113 | 137 | - |
| Stage 1 | 533 | 561 | - |
| Stage 2 | 303 | 335 | - |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | 33.7 |
| HCM LOS | D |

[^29]Appendix W 2017 Trip Distribution Sensitivity Analysis Worksheets for 85/15 Split

## SITE LAYOUT

Site: 2017 Total Build NW 319 St and NW 31st Ave Weekday AM 85/15 Split
2017 Total Traffic Weekday AM
85/15 Split Sensitivity Analysis
Roundabout


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Project: H:\projfile\12393 - Cowlitz Reservation Development\Sidra\2014 Analysis\Interchange Roundabouts\102 NW 319th St and NW 31st Avel2017 AnalysisINW 319 St and NW 31st Ave 85_15.sip6 8001045, KITTELSON AND ASSOCIATES INC, PLUS / Floating

## MOVEMENT SUMMARY

Site: 2017 Total Build NW 319 St and NW 31st Ave Weekday AM 85/15 Split
2017 Total Traffic Weekday AM
85/15 Split Sensitivity Analysis
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | Flows HV $\%$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles <br> veh | Queue <br> Distance <br> ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| South: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 5 | 0.0 | 0.117 | 6.0 | LOS A | 0.5 | 15.8 | 0.46 | 0.33 | 34.4 |
| 8 | T1 | 5 | 1.0 | 0.117 | 6.0 | LOS A | 0.5 | 15.8 | 0.46 | 0.33 | 34.4 |
| 18 | R2 | 78 | 23.0 | 0.117 | 6.0 | LOS A | 0.5 | 15.8 | 0.46 | 0.33 | 30.2 |
| Appr |  | 88 | 20.4 | 0.117 | 6.0 | LOS A | 0.5 | 15.8 | 0.46 | 0.33 | 30.7 |
| East: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 49 | 11.0 | 0.108 | 3.7 | LOS A | 0.6 | 14.5 | 0.08 | 0.02 | 33.4 |
| 6 | T1 | 89 | 2.0 | 0.108 | 3.7 | LOS A | 0.6 | 14.5 | 0.08 | 0.02 | 32.9 |
| 16 | R2 | 249 | 1.0 | 0.153 | 3.4 | LOS A | 0.9 | 21.5 | 0.07 | 0.01 | 32.7 |
| Appr |  | 387 | 2.5 | 0.153 | 3.5 | LOS A | 0.9 | 21.5 | 0.07 | 0.01 | 32.8 |
| North: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 187 | 1.0 | 0.182 | 5.0 | LOS A | 0.9 | 22.5 | 0.33 | 0.19 | 30.1 |
| 4 | T1 | 5 | 1.0 | 0.182 | 5.0 | LOS A | 0.9 | 22.5 | 0.33 | 0.19 | 32.3 |
| 14 | R2 | 1 | 1.0 | 0.182 | 5.0 | LOS A | 0.9 | 22.5 | 0.33 | 0.19 | 30.7 |
| Appr |  | 193 | 1.0 | 0.182 | 5.0 | LOS A | 0.9 | 22.5 | 0.33 | 0.19 | 30.1 |
| West: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 1 | 1.0 | 0.101 | 4.8 | LOS A | 0.5 | 12.3 | 0.42 | 0.27 | 35.0 |
| 2 | T1 | 78 | 4.0 | 0.101 | 4.8 | LOS A | 0.5 | 12.3 | 0.42 | 0.27 | 33.2 |
| 12 | R2 | 15 | 0.0 | 0.101 | 4.8 | LOS A | 0.5 | 12.3 | 0.42 | 0.27 | 34.1 |
| Approach |  | 94 | 3.3 | 0.101 | 4.8 | LOS A | 0.5 | 12.3 | 0.42 | 0.27 | 33.4 |
| All Vehicles |  | 762 | 4.3 | 0.182 | 4.3 | LOS A | 0.9 | 22.5 | 0.23 | 0.13 | 31.9 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement LOS $F$ will result if $v / c>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^30]
## LANE SUMMARY

## Site: 2017 Total Build NW 319 St and NW 31st Ave Weekday AM 85/15 Split

```
2017 Total Traffic Weekday AM
85/15 Split Sensitivity Analysis
Roundabout
```

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand <br> Total veh/h | $\begin{aligned} & \text { Flows } \\ & \text { HV } \\ & \% \end{aligned}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. $\%$ | Average Delay sec | Level of Service | 95\% Bac Veh | $\begin{aligned} & \text { ueue } \\ & \text { Dist } \\ & \text { ft } \end{aligned}$ | Lane Config | Lane Length ft | Cap. Adj. \% | Prob. Block. \% |
| South: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 88 | 20.4 | 755 | 0.117 | 100 | 6.0 | LOS A | 0.5 | 15.8 | Full | 1600 | 0.0 | 0.0 |
| Approach | 88 | 20.4 |  | 0.117 |  | 6.0 | LOS A | 0.5 | 15.8 |  |  |  |  |
| East: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 138 | 5.2 | 1280 | 0.108 | 100 | 3.7 | LOS A | 0.6 | 14.5 | Full | 650 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 249 | 1.0 | 1623 | 0.153 | 100 | 3.4 | LOS A | 0.9 | 21.5 | Full | 650 | 0.0 | 0.0 |
| Approach | 387 | 2.5 |  | 0.153 |  | 3.5 | LOS A | 0.9 | 21.5 |  |  |  |  |
| North: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 193 | 1.0 | 1063 | 0.182 | 100 | 5.0 | LOS A | 0.9 | 22.5 | Full | 1400 | 0.0 | 0.0 |
| Approach | 193 | 1.0 |  | 0.182 |  | 5.0 | LOS A | 0.9 | 22.5 |  |  |  |  |
| West: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 94 | 3.3 | 934 | 0.101 | 100 | 4.8 | LOS A | 0.5 | 12.3 | Full | 1300 | 0.0 | 0.0 |
| Approach | 94 | 3.3 |  | 0.101 |  | 4.8 | LOS A | 0.5 | 12.3 |  |  |  |  |
| Intersection | 762 | 4.3 |  | 0.182 |  | 4.3 | LOS A | 0.9 | 22.5 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D),
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation
d Dominant lane on roundabout approach

## SITE LAYOUT

## Site: 2017 Total Build NW La Center and SB Ramps Weekday AM 85_15 Split

2017 Total Traffic Weekday AM
Roundabout


## MOVEMENT SUMMARY

Site: 2017 Total Build NW La Center and SB Ramps Weekday AM 85_15 Split
2017 Total Traffic Weekday AM
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{gathered} \text { =lows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles <br> veh | Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 535 | 4.0 | 0.361 | 5.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 32.9 |
| 6 | T1 | 361 | 2.0 | 0.361 | 4.4 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 36.6 |
| Appr |  | 896 | 3.2 | 0.361 | 4.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 34.0 |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 118 | 13.0 | 0.273 | 10.5 | LOS B | 1.0 | 27.7 | 0.61 | 0.61 | 26.4 |
| 4 | T1 | 4 | 50.0 | 0.273 | 10.5 | LOS B | 1.0 | 27.7 | 0.61 | 0.61 | 28.6 |
| 14 | R2 | 25 | 8.0 | 0.273 | 10.5 | LOS B | 1.0 | 27.7 | 0.61 | 0.61 | 25.8 |
| Appr |  | 147 | 13.2 | 0.273 | 10.5 | LOS B | 1.0 | 27.7 | 0.61 | 0.61 | 26.4 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 2 | T1 | 118 | 20.0 | 0.172 | 7.2 | LOS A | 0.9 | 26.3 | 0.67 | 0.60 | 29.0 |
| 12 | R2 | 225 | 2.0 | 0.137 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.9 |
| Approach |  | 343 | 8.2 | 0.172 | 2.5 | LOS A | 0.9 | 26.3 | 0.23 | 0.21 | 33.8 |
| All Vehicles |  | 1386 | 5.5 | 0.361 | 4.8 | LOS A | 1.0 | 27.7 | 0.12 | 0.12 | 32.8 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D)
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2017 Total Build NW La Center and SB Ramps Weekday AM 85_15 Split

## 2017 Total Traffic Weekday AM <br> Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \\ \hline \end{gathered}$ | Cap. veh/h | Deg. <br> Satn <br> v/c | Lane Util. $\%$ | Average Delay sec | Level of Service | 95\% Bac Veh | $\begin{aligned} & \text { ueue } \\ & \text { Dist } \\ & \text { ft } \end{aligned}$ | Lane Config | Lane Length ft | $\begin{aligned} & \text { Cap. } \\ & \text { Adj. } \\ & \% \end{aligned}$ | Prob. Block. \% |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 618 | 3.7 | 1710 | 0.361 | 100 | 5.1 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Lane 2 | 278 | 2.0 | 1400 | 0.199 | $55^{7}$ | 4.2 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 896 | 3.2 |  | 0.361 |  | 4.8 | LOS A | 0.0 | 0.0 |  |  |  |  |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 147 | 13.2 | 539 | 0.273 | 100 | 10.5 | LOS B | 1.0 | 27.7 | Full | 1300 | 0.0 | 0.0 |
| Approach | 147 | 13.2 |  | 0.273 |  | 10.5 | LOS B | 1.0 | 27.7 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 118 | 20.0 | 688 | 0.172 | 100 | 7.2 | LOS A | 0.9 | 26.3 | Full | 650 | 0.0 | 0.0 |
| Lane 2 | 225 | 2.0 | 1642 | 0.137 | 100 | 0.0 | LOS A | 0.0 | 0.0 | Short | 200 | 0.0 | 0.0 |
| Approach | 343 | 8.2 |  | 0.172 |  | 2.5 | LOS A | 0.9 | 26.3 |  |  |  |  |
| Intersection | 1386 | 5.5 |  | 0.361 |  | 4.8 | LOS A | 1.0 | 27.7 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
7 Lane underutilisation specified by user
d Dominant lane on roundabout approach

## SITE LAYOUT

Site: 2017 Total Build NW La Center and NB Ramps Weekday AM 85/15 Split
2017 Total Traffic Weekday AM
85/15 Split Sensitivity Analysis
Roundabout


## MOVEMENT SUMMARY

Site: 2017 Total Build NW La Center and NB Ramps Weekday AM 85/15 Split

```
2017 Total Traffic Weekday AM
85/15 Split Sensitivity Analysis
Roundabout
```

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \text { ID } \end{gathered}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue <br> Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| South: NB Ramp |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 292 | 1.0 | 0.231 | 5.7 | LOS A | 1.2 | 29.7 | 0.44 | 0.31 | 24.8 |
| 8 | T1 | 4 | 50.0 | 0.231 | 5.7 | LOS A | 1.2 | 29.7 | 0.44 | 0.31 | 29.0 |
| 18 | R2 | 321 | 7.0 | 0.292 | 6.1 | LOS A | 1.6 | 41.8 | 0.46 | 0.33 | 29.7 |
| Appro |  | 617 | 4.4 | 0.292 | 5.9 | LOS A | 1.6 | 41.8 | 0.45 | 0.32 | 27.1 |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 6 | T1 | 604 | 4.0 | 0.566 | 11.3 | LOS B | 3.7 | 96.7 | 0.61 | 0.57 | 21.1 |
| 16 | R2 | 156 | 17.0 | 0.351 | 10.4 | LOS B | 1.6 | 43.5 | 0.55 | 0.52 | 25.7 |
| Appro |  | 760 | 6.7 | 0.566 | 11.1 | LOS B | 3.7 | 96.7 | 0.60 | 0.56 | 22.1 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 77 | 17.0 | 0.167 | 3.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 34.7 |
| 2 | T1 | 159 | 17.0 | 0.167 | 3.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 34.5 |
| Appro |  | 236 | 17.0 | 0.167 | 3.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 34.5 |
| All Ve |  | 1613 | 7.3 | 0.566 | 8.1 | LOS A | 3.7 | 96.7 | 0.45 | 0.39 | 25.6 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2017 Total Build NW La Center and NB Ramps Weekday AM 85/15 Split

```
2017 Total Traffic Weekday AM
85/15 Split Sensitivity Analysis
Roundabout
```

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. Util. \% | Average Delay sec | Level of Service | 95\% Bac Veh | $\begin{aligned} & \text { ueue } \\ & \text { Dist } \\ & \text { ft } \end{aligned}$ | Lane Config | Lane Length ft | Cap. Adj. \% | Prob. Block. \% |
| South: NB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 57 | 1.0 | 712 | 0.081 | $35^{7}$ | 5.9 | LOS A | 0.3 | 8.8 | Full | 1800 | 0.0 | 0.0 |
| Lane 2 | 239 | 1.8 | 1034 | 0.231 | 100 | 5.7 | LOS A | 1.2 | 29.7 | Full | 1800 | 0.0 | 0.0 |
| Lane $3^{\text {d }}$ | 321 | 7.0 | 1098 | 0.292 | 100 | 6.1 | LOS A | 1.6 | 41.8 | Short | 250 | 0.0 | 0.0 |
| Approach | 617 | 4.4 |  | 0.292 |  | 5.9 | LOS A | 1.6 | 41.8 |  |  |  |  |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 537 | 4.0 | 949 | 0.566 | 100 | 11.4 | LOS B | 3.7 | 96.7 | Full | 600 | 0.0 | 0.0 |
| Lane 2 | 223 | 13.1 | 637 | 0.351 | $62^{7}$ | 10.4 | LOS B | 1.6 | 43.5 | Full | 600 | 0.0 | 0.0 |
| Approach | 760 | 6.7 |  | 0.566 |  | 11.1 | LOS B | 3.7 | 96.7 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 236 | 17.0 | 1413 | 0.167 | 100 | 3.9 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 236 | 17.0 |  | 0.167 |  | 3.9 | LOS A | 0.0 | 0.0 |  |  |  |  |
| Intersection | 1613 | 7.3 |  | 0.566 |  | 8.1 | LOS A | 3.7 | 96.7 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D)
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

7 Lane underutilisation specified by user
d Dominant lane on roundabout approach

## SITE LAYOUT

Site: 2017 Total Build NW 319 St and NW 31st Ave Weekday AM 85/15 Split
2017 Total Traffic Weekday AM
85/15 Split Sensitivity Analysis
Roundabout


Copyright © 2000-2014 Akcelik and Associates Pty Ltd www.sidrasolutions.com
Project: H:\projfile\12393 - Cowlitz Reservation Development\Sidra\2014 Analysis\Interchange Roundabouts\102 NW 319th St and NW 31st Avel2017 AnalysisINW 319 St and NW 31st Ave 85_15.sip6 8001045, KITTELSON AND ASSOCIATES INC, PLUS / Floating

## MOVEMENT SUMMARY

Site: 2017 Total Build NW 319 St and NW 31st Ave Weekday PM 85/15 Split

```
2017 Total Traffic Weekday AM
85/15 Split Sensitivity Analysis
Roundabout
```

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles <br> veh | Queue <br> Distance <br> ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| South: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 17 | 0.0 | 0.216 | 9.1 | LOS A | 1.2 | 32.3 | 0.74 | 0.69 | 32.4 |
| 8 | T1 | 10 | 10.0 | 0.216 | 9.1 | LOS A | 1.2 | 32.3 | 0.74 | 0.69 | 32.3 |
| 18 | R2 | 96 | 7.0 | 0.216 | 9.1 | LOS A | 1.2 | 32.3 | 0.74 | 0.69 | 29.1 |
| Appr |  | 123 | 6.3 | 0.216 | 9.1 | LOS A | 1.2 | 32.3 | 0.74 | 0.69 | 29.9 |
| East: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 97 | 2.0 | 0.252 | 5.3 | LOS A | 1.6 | 42.5 | 0.17 | 0.06 | 32.7 |
| 6 | T1 | 200 | 9.0 | 0.252 | 5.3 | LOS A | 1.6 | 42.5 | 0.17 | 0.06 | 31.5 |
| 16 | R2 | 641 | 1.0 | 0.403 | 5.8 | LOS A | 3.3 | 82.4 | 0.18 | 0.06 | 31.0 |
| Appr |  | 938 | 2.8 | 0.403 | 5.6 | LOS A | 3.3 | 82.4 | 0.18 | 0.06 | 31.3 |
| North: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 524 | 1.0 | 0.581 | 12.1 | LOS B | 4.7 | 119.6 | 0.69 | 0.61 | 26.4 |
| 4 | T1 | 10 | 10.0 | 0.581 | 12.1 | LOS B | 4.7 | 119.6 | 0.69 | 0.61 | 29.1 |
| 14 | R2 | 1 | 0.0 | 0.581 | 12.1 | LOS B | 4.7 | 119.6 | 0.69 | 0.61 | 27.7 |
| Appr |  | 535 | 1.2 | 0.581 | 12.1 | LOS B | 4.7 | 119.6 | 0.69 | 0.61 | 26.5 |
| West: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 1 | 0.0 | 0.272 | 9.2 | LOS A | 1.6 | 41.3 | 0.74 | 0.69 | 32.6 |
| 2 | T1 | 165 | 3.0 | 0.272 | 9.2 | LOS A | 1.6 | 41.3 | 0.74 | 0.69 | 30.2 |
| 12 | R2 | 5 | 0.0 | 0.272 | 9.2 | LOS A | 1.6 | 41.3 | 0.74 | 0.69 | 31.8 |
| Approach |  | 171 | 2.9 | 0.272 | 9.2 | LOS A | 1.6 | 41.3 | 0.74 | 0.69 | 30.3 |
| All Vehicles |  | 1767 | 2.6 | 0.581 | 8.2 | LOS A | 4.7 | 119.6 | 0.43 | 0.33 | 29.4 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement LOS $F$ will result if $v / c>1$ irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies. Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D). HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

[^31]
## LANE SUMMARY

## Site: 2017 Total Build NW 319 St and NW 31st Ave Weekday PM 85/15 Split

```
2017 Total Traffic Weekday AM
85/15 Split Sensitivity Analysis
Roundabout
```

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Average Delay sec | Level of Service | $\begin{gathered} 95 \% \text { Bac } \\ \text { Veh } \end{gathered}$ | $\begin{aligned} & \text { Queue } \\ & \text { Dist } \\ & \mathrm{ft} \end{aligned}$ | Lane Config | Lane Length ft | Cap. Adj. \% | Prob. Block. \% |
| South: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 123 | 6.3 | 569 | 0.216 | 100 | 9.1 | LOS A | 1.2 | 32.3 | Full | 1600 | 0.0 | 0.0 |
| Approach | 123 | 6.3 |  | 0.216 |  | 9.1 | LOS A | 1.2 | 32.3 |  |  |  |  |
| East: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 297 | 6.7 | 1180 | 0.252 | 100 | 5.3 | LOS A | 1.6 | 42.5 | Full | 650 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 641 | 1.0 | 1591 | 0.403 | 100 | 5.8 | LOS A | 3.3 | 82.4 | Full | 650 | 0.0 | 0.0 |
| Approach | 938 | 2.8 |  | 0.403 |  | 5.6 | LOS A | 3.3 | 82.4 |  |  |  |  |
| North: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1{ }^{\text {d }}$ | 535 | 1.2 | 920 | 0.581 | 100 | 12.1 | LOS B | 4.7 | 119.6 | Full | 1400 | 0.0 | 0.0 |
| Approach | 535 | 1.2 |  | 0.581 |  | 12.1 | LOS B | 4.7 | 119.6 |  |  |  |  |
| West: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 171 | 2.9 | 629 | 0.272 | 100 | 9.2 | LOS A | 1.6 | 41.3 | Full | 1300 | 0.0 | 0.0 |
| Approach | 171 | 2.9 |  | 0.272 |  | 9.2 | LOS A | 1.6 | 41.3 |  |  |  |  |
| Intersection | 1767 | 2.6 |  | 0.581 |  | 8.2 | LOS A | 4.7 | 119.6 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D),
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation
d Dominant lane on roundabout approach

## SITE LAYOUT

## Site: 2017 Total Build NW La Center and SB Ramps Weekday AM 85_15 Split

2017 Total Traffic Weekday AM
Roundabout


## MOVEMENT SUMMARY

Site: 2017 Total Build NW La Center and SB Ramps Weekday PM 85_15 Split
2017 Total Traffic Weekday PM
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{array}{r} \text { Flows } \\ \text { HV } \\ \% \\ \hline \end{array}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 374 | 5.0 | 0.369 | 5.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 33.7 |
| 6 | T1 | 824 | 2.0 | 0.369 | 5.3 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 37.2 |
| Appr |  | 1198 | 2.9 | 0.377 | 5.4 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.7 |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 165 | 10.0 | 0.532 | 16.8 | LOS B | 2.6 | 68.2 | 0.73 | 0.81 | 24.2 |
| 4 | T1 | 4 | 50.0 | 0.532 | 16.8 | LOS B | 2.6 | 68.2 | 0.73 | 0.81 | 26.6 |
| 14 | R2 | 114 | 2.0 | 0.532 | 16.8 | LOS B | 2.6 | 68.2 | 0.73 | 0.81 | 23.8 |
| Appr |  | 283 | 7.3 | 0.532 | 16.8 | LOS B | 2.6 | 68.2 | 0.73 | 0.81 | 24.1 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 2 | T1 | 185 | 7.0 | 0.214 | 6.4 | LOS A | 1.2 | 32.0 | 0.64 | 0.54 | 30.5 |
| 12 | R2 | 600 | 1.0 | 0.362 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.9 |
| Appr |  | 785 | 2.4 | 0.362 | 1.5 | LOS A | 1.2 | 32.0 | 0.15 | 0.13 | 34.8 |
| All V |  | 2266 | 3.3 | 0.532 | 5.5 | LOS A | 2.6 | 68.2 | 0.14 | 0.14 | 33.0 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2017 Total Build NW La Center and SB Ramps Weekday PM 85_15 Split

## 2017 Total Traffic Weekday PM <br> Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{array}{r} \text { lows } \\ \text { HV } \\ \% \\ \hline \end{array}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Average Delay sec | Level of Service | $\begin{gathered} 95 \% \mathrm{Ba} \\ \text { Veh } \end{gathered}$ | ueue Dist ft | Lane Config | Lane Length ft | Cap. Adj. \% | Prob. Block. \% |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 543 | 4.1 | 1471 | 0.369 | $98^{7}$ | 5.7 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 655 | 2.0 | 1739 | 0.377 | 100 | 5.2 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 1198 | 2.9 |  | 0.377 |  | 5.4 | LOS A | 0.0 | 0.0 |  |  |  |  |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 283 | 7.3 | 532 | 0.532 | 100 | 16.8 | LOS B | 2.6 | 68.2 | Full | 1300 | 0.0 | 0.0 |
| Approach | 283 | 7.3 |  | 0.532 |  | 16.8 | LOS B | 2.6 | 68.2 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1{ }^{\text {d }}$ | 185 | 7.0 | 864 | 0.214 | 100 | 6.4 | LOS A | 1.2 | 32.0 | Full | 650 | 0.0 | 0.0 |
| Lane 2 | 600 | 1.0 | 1658 | 0.362 | 100 | 0.0 | LOS A | 0.0 | 0.0 | Short | 200 | 0.0 | 0.0 |
| Approach | 785 | 2.4 |  | 0.362 |  | 1.5 | LOS A | 1.2 | 32.0 |  |  |  |  |
| Intersection | 2266 | 3.3 |  | 0.532 |  | 5.5 | LOS A | 2.6 | 68.2 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
7 Lane underutilisation specified by user
d Dominant lane on roundabout approach

## SITE LAYOUT

Site: 2017 Total Build NW La Center and NB Ramps Weekday AM 85/15 Split
2017 Total Traffic Weekday AM
85/15 Split Sensitivity Analysis
Roundabout


## MOVEMENT SUMMARY

Site: 2017 Total Build NW La Center and NB Ramps Weekday PM 85/15 Split

```
2017 Total Traffic Weekday PM
85/15 Split Sensitivity Analysis
Roundabout
```

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \text { ID } \end{gathered}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| South: NB Ramp |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 747 | 1.0 | 0.561 | 9.7 | LOS A | 4.3 | 109.2 | 0.63 | 0.54 | 23.5 |
| 8 | T1 | 8 | 50.0 | 0.561 | 10.1 | LOS B | 4.3 | 109.2 | 0.65 | 0.55 | 27.3 |
| 18 | R2 | 591 | 3.0 | 0.591 | 11.6 | LOS B | 4.9 | 125.7 | 0.69 | 0.63 | 27.2 |
| Appro |  | 1346 | 2.2 | 0.591 | 10.6 | LOS B | 4.9 | 125.7 | 0.66 | 0.58 | 25.0 |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 6 | T1 | 451 | 4.0 | 0.535 | 13.4 | LOS B | 3.5 | 89.6 | 0.76 | 0.80 | 20.1 |
| 16 | R2 | 119 | 5.0 | 0.358 | 11.8 | LOS B | 1.8 | 45.5 | 0.70 | 0.72 | 25.1 |
| Appro |  | 570 | 4.2 | 0.535 | 13.0 | LOS B | 3.5 | 89.6 | 0.75 | 0.79 | 21.2 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 69 | 4.0 | 0.229 | 4.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.8 |
| 2 | T1 | 281 | 9.0 | 0.229 | 4.2 | LOSA | 0.0 | 0.0 | 0.00 | 0.00 | 36.0 |
| Appro |  | 350 | 8.0 | 0.229 | 4.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.9 |
| All Ve |  | 2266 | 3.6 | 0.591 | 10.2 | LOS B | 4.9 | 125.7 | 0.58 | 0.54 | 25.0 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2017 Total Build NW La Center and NB Ramps Weekday PM 85/15 Split

```
2017 Total Traffic Weekday PM
85/15 Split Sensitivity Analysis
Roundabout
```

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Average Delay sec | Level of Service | 95\% Back <br> Veh | Queue Dist ft | Lane Config | Lane Length ft | Cap. <br> Adj. <br> \% | Prob. Block. \% |
| South: NB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 134 | 1.0 | 657 | 0.205 | $37^{7}$ | 7.9 | LOS A | 1.0 | 24.3 | Full | 1800 | 0.0 | 0.0 |
| Lane $2{ }^{\text {d }}$ | 621 | 1.6 | 1106 | 0.561 | 100 | 10.1 | LOS B | 4.3 | 109.2 | Full | 1800 | 0.0 | 0.0 |
| Lane 3 | 591 | 3.0 | 1000 | 0.591 | 100 | 11.6 | LOS B | 4.9 | 125.7 | Short | 250 | 0.0 | 0.0 |
| Approach | 1346 | 2.2 |  | 0.591 |  | 10.6 | LOS B | 4.9 | 125.7 |  |  |  |  |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 371 | 4.0 | 693 | 0.535 | 100 | 13.7 | LOS B | 3.5 | 89.6 | Full | 600 | 0.0 | 0.0 |
| Lane 2 | 199 | 4.6 | 557 | 0.358 | $67^{7}$ | 11.8 | LOS B | 1.8 | 45.5 | Full | 600 | 0.0 | 0.0 |
| Approach | 570 | 4.2 |  | 0.535 |  | 13.0 | LOS B | 3.5 | 89.6 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 350 | 8.0 | 1531 | 0.229 | 100 | 4.2 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 350 | 8.0 |  | 0.229 |  | 4.2 | LOS A | 0.0 | 0.0 |  |  |  |  |
| Intersection | 2266 | 3.6 |  | 0.591 |  | 10.2 | LOS B | 4.9 | 125.7 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

7 Lane underutilisation specified by user
d Dominant lane on roundabout approach

## SITE LAYOUT

Site: 2017 Total Build NW 319 St and NW 31st Ave Weekday AM 85/15 Split
2017 Total Traffic Weekday AM
85/15 Split Sensitivity Analysis
Roundabout


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Project: H:\projfile\12393 - Cowlitz Reservation Development\Sidra\2014 Analysis\Interchange Roundabouts\102 NW 319th St and NW 31st Avel2017 AnalysisINW 319 St and NW 31st Ave 85_15.sip6 8001045, KITTELSON AND ASSOCIATES INC, PLUS / Floating

## MOVEMENT SUMMARY

Site: 2017 Total Build NW 319 St and NW 31st Ave Weekend Peak 85/15 Split

```
2017 Total Traffic Weekend Peak 85/15 Split Sensitivity Analysis
```

Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{array}{r} \text { Flows } \\ \text { HV } \\ \% \\ \hline \end{array}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue <br> Distance <br> ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| South: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 5 | 25.0 | 0.153 | 8.3 | LOS A | 0.9 | 22.2 | 0.74 | 0.66 | 30.4 |
| 8 | T1 | 15 | 1.0 | 0.153 | 8.3 | LOS A | 0.9 | 22.2 | 0.74 | 0.66 | 33.2 |
| 18 | R2 | 66 | 4.0 | 0.153 | 8.3 | LOS A | 0.9 | 22.2 | 0.74 | 0.66 | 30.0 |
| Appr |  | 86 | 4.7 | 0.153 | 8.3 | LOS A | 0.9 | 22.2 | 0.74 | 0.66 | 30.7 |
| East: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 77 | 6.0 | 0.244 | 5.4 | LOS A | 1.5 | 39.6 | 0.15 | 0.05 | 32.8 |
| 6 | T1 | 203 | 2.0 | 0.244 | 5.4 | LOS A | 1.5 | 39.6 | 0.15 | 0.05 | 31.9 |
| 16 | R2 | 839 | 1.0 | 0.513 | 7.1 | LOS A | 4.9 | 123.7 | 0.18 | 0.05 | 30.2 |
| Appr |  | 1119 | 1.5 | 0.513 | 6.6 | LOS A | 4.9 | 123.7 | 0.17 | 0.05 | 30.7 |
| North: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 559 | 1.0 | 0.590 | 11.9 | LOS B | 4.8 | 121.3 | 0.67 | 0.56 | 26.5 |
| 4 | T1 | 10 | 1.0 | 0.590 | 11.9 | LOS B | 4.8 | 121.3 | 0.67 | 0.56 | 29.3 |
| 14 | R2 | 1 | 1.0 | 0.590 | 11.9 | LOS B | 4.8 | 121.3 | 0.67 | 0.56 | 27.7 |
| Appr |  | 570 | 1.0 | 0.590 | 11.9 | LOS B | 4.8 | 121.3 | 0.67 | 0.56 | 26.6 |
| West: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 1 | 1.0 | 0.283 | 9.6 | LOS A | 1.7 | 43.5 | 0.76 | 0.71 | 32.2 |
| 2 | T1 | 157 | 4.0 | 0.283 | 9.6 | LOS A | 1.7 | 43.5 | 0.76 | 0.71 | 29.8 |
| 12 | R2 | 15 | 0.0 | 0.283 | 9.6 | LOS A | 1.7 | 43.5 | 0.76 | 0.71 | 31.6 |
| Appr |  | 173 | 3.6 | 0.283 | 9.6 | LOS A | 1.7 | 43.5 | 0.76 | 0.71 | 30.1 |
| All V |  | 1948 | 1.7 | 0.590 | 8.5 | LOS A | 4.9 | 123.7 | 0.39 | 0.28 | 29.3 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2017 Total Build NW 319 St and NW 31st Ave Weekend Peak 85/15 Split

2017 Total Traffic Weekend Peak 85/15 Split Sensitivity Analysis

Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Cap. veh/h | Deg. Satn v/c | $\begin{aligned} & \text { Lane } \\ & \text { Util. } \\ & \% \end{aligned}$ | Average Delay sec | Level of Service | $\begin{gathered} 95 \% \mathrm{Bac} \\ \text { Veh } \end{gathered}$ | $\begin{aligned} & \text { Queue } \\ & \text { Dist } \\ & \mathrm{ft} \end{aligned}$ | Lane Config | Lane Length ft | $\begin{gathered} \hline \text { Cap. } \\ \text { Adj. } \\ \% \end{gathered}$ | Prob. Block. \% |
| South: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane ${ }^{\text {d }}$ | 86 | 4.7 | 564 | 0.153 | 100 | 8.3 | LOS A | 0.9 | 22.2 | Full | 1600 | 0.0 | 0.0 |
| Approach | 86 | 4.7 |  | 0.153 |  | 8.3 | LOS A | 0.9 | 22.2 |  |  |  |  |
| East: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 280 | 3.1 | 1146 | 0.244 | 100 | 5.4 | LOS A | 1.5 | 39.6 | Full | 650 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 839 | 1.0 | 1636 | 0.513 | 100 | 7.1 | LOS A | 4.9 | 123.7 | Full | 650 | 0.0 | 0.0 |
| Approach | 1119 | 1.5 |  | 0.513 |  | 6.6 | LOS A | 4.9 | 123.7 |  |  |  |  |
| North: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 570 | 1.0 | 967 | 0.590 | 100 | 11.9 | LOS B | 4.8 | 121.3 | Full | 1400 | 0.0 | 0.0 |
| Approach | 570 | 1.0 |  | 0.590 |  | 11.9 | LOS B | 4.8 | 121.3 |  |  |  |  |
| West: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 173 | 3.6 | 611 | 0.283 | 100 | 9.6 | LOS A | 1.7 | 43.5 | Full | 1300 | 0.0 | 0.0 |
| Approach | 173 | 3.6 |  | 0.283 |  | 9.6 | LOS A | 1.7 | 43.5 |  |  |  |  |
| Intersection | 1948 | 1.7 |  | 0.590 |  | 8.5 | LOS A | 4.9 | 123.7 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

Processed: Friday, August 29, 2014 12:20:51 PM
SIDRA INTERSECTION 6.0.22.4722

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Project: H:\projfile\12393 - Cowlitz Reservation Development\Sidra\2014 Analysis\Interchange Roundabouts\102 NW 319th St and NW 31st Avel2017 Analysis\NW 319 St and NW 31st Ave 85_15.sip6 8001045, KITTELSON AND ASSOCIATES INC, PLUS / Floating

## SITE LAYOUT

## Site: 2017 Total Build NW La Center and SB Ramps Weekday AM 85_15 Split

2017 Total Traffic Weekday AM
Roundabout


## MOVEMENT SUMMARY

Site: 2017 Total Build NW La Center and SB Ramps Weekend 85_15 Split

## 2017 Total Traffic Weekend Peak

Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dem Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed $\qquad$ mph |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 375 | 2.0 | 0.370 | 5.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 34.2 |
| 6 | T1 | 982 | 1.0 | 0.370 | 6.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 37.5 |
| Appr |  | 1357 | 1.3 | 0.462 | 5.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 36.2 |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 172 | 4.0 | 0.625 | 21.3 | LOS C | 3.5 | 92.8 | 0.79 | 0.92 | 22.7 |
| 4 | T1 | 4 | 0.0 | 0.625 | 21.3 | LOS C | 3.5 | 92.8 | 0.79 | 0.92 | 25.5 |
| 14 | R2 | 141 | 8.0 | 0.625 | 21.3 | LOS C | 3.5 | 92.8 | 0.79 | 0.92 | 22.0 |
| Appr |  | 317 | 5.7 | 0.625 | 21.3 | LOS C | 3.5 | 92.8 | 0.79 | 0.92 | 22.4 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 2 | T1 | 146 | 3.0 | 0.159 | 5.5 | LOS A | 0.9 | 22.7 | 0.61 | 0.49 | 31.6 |
| 12 | R2 | 636 | 2.0 | 0.387 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.9 |
| Approach |  | 782 | 2.2 | 0.387 | 1.0 | LOS A | 0.9 | 22.7 | 0.11 | 0.09 | 35.2 |
| All V |  | 2456 | 2.1 | 0.625 | 6.4 | LOS A | 3.5 | 92.8 | 0.14 | 0.15 | 32.8 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2017 Total Build NW La Center and SB Ramps Weekend 85_15 Split

## 2017 Total Traffic Weekend Peak <br> Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Average Delay sec | Level of Service | $\begin{gathered} 95 \% \mathrm{Ba} \\ \text { Veh } \end{gathered}$ | $\begin{aligned} & \text { ueue } \\ & \text { Dist } \\ & \text { ft } \end{aligned}$ | Lane Config | Lane Length ft | $\begin{aligned} & \text { Cap. } \\ & \text { Adj. } \\ & \% \end{aligned}$ | Prob. Block. \% |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 545 | 1.7 | 1476 | 0.370 | $80^{7}$ | 5.7 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 812 | 1.0 | 1757 | 0.462 | 100 | 6.1 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 1357 | 1.3 |  | 0.462 |  | 5.9 | LOS A | 0.0 | 0.0 |  |  |  |  |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 317 | 5.7 | 507 | 0.625 | 100 | 21.3 | LOS C | 3.5 | 92.8 | Full | 1300 | 0.0 | 0.0 |
| Approach | 317 | 5.7 |  | 0.625 |  | 21.3 | LOS C | 3.5 | 92.8 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 146 | 3.0 | 916 | 0.159 | 100 | 5.5 | LOS A | 0.9 | 22.7 | Full | 650 | 0.0 | 0.0 |
| Lane 2 | 636 | 2.0 | 1642 | 0.387 | 100 | 0.0 | LOS A | 0.0 | 0.0 | Short | 200 | 0.0 | 0.0 |
| Approach | 782 | 2.2 |  | 0.387 |  | 1.0 | LOS A | 0.9 | 22.7 |  |  |  |  |
| Intersection | 2456 | 2.1 |  | 0.625 |  | 6.4 | LOS A | 3.5 | 92.8 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
7 Lane underutilisation specified by user
d Dominant lane on roundabout approach

## SITE LAYOUT

Site: 2017 Total Build NW La Center and NB Ramps Weekday AM 85/15 Split
2017 Total Traffic Weekday AM
85/15 Split Sensitivity Analysis
Roundabout


## MOVEMENT SUMMARY

Site: 2017 Total Build NW La Center and NB Ramps Weekend 85/15 Split

2017 Total Traffic Weekend<br>85/15 Split Sensitivity Analysis<br>Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | Flows HV $\%$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles <br> veh | Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| South: NB Ramp |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 927 | 1.0 | 0.670 | 11.7 | LOS B | 6.6 | 167.5 | 0.67 | 0.58 | 21.2 |
| 8 | T1 | 4 | 0.0 | 0.670 | 12.4 | LOS B | 6.6 | 167.5 | 0.70 | 0.61 | 26.7 |
| 18 | R2 | 564 | 3.0 | 0.574 | 11.3 | LOS B | 4.5 | 114.5 | 0.65 | 0.57 | 27.3 |
| Appr |  | 1495 | 1.8 | 0.670 | 11.6 | LOS B | 6.6 | 167.5 | 0.67 | 0.58 | 23.1 |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 6 | T1 | 430 | 3.0 | 0.617 | 17.9 | LOS B | 4.5 | 116.1 | 0.85 | 0.93 | 18.3 |
| 16 | R2 | 124 | 12.0 | 0.425 | 16.7 | LOS B | 2.2 | 59.6 | 0.78 | 0.81 | 22.6 |
| Appr |  | 554 | 5.0 | 0.617 | 17.7 | LOS B | 4.5 | 116.1 | 0.83 | 0.90 | 19.3 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 74 | 1.0 | 0.200 | 3.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.7 |
| 2 | T1 | 244 | 5.0 | 0.200 | 3.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 36.0 |
| Approach |  | 318 | 4.1 | 0.200 | 3.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.9 |
| All Vehicles |  | 2367 | 2.8 | 0.670 | 12.0 | LOS B | 6.6 | 167.5 | 0.62 | 0.57 | 23.1 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement
LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2017 Total Build NW La Center and NB Ramps Weekend 85/15 Split

2017 Total Traffic Weekend 85/15 Split Sensitivity Analysis<br>Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Average Delay sec | Level of Service | $\begin{gathered} 95 \% \text { Ba } \\ \text { Veh } \end{gathered}$ | $\begin{aligned} & \text { Queue } \\ & \text { Dist } \end{aligned}$ | Lane Config | Lane Length ft | $\begin{aligned} & \text { Cap. } \\ & \text { Adj. } \\ & \% \end{aligned}$ | Prob. Block. \% |
| South: NB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 146 | 1.0 | 681 | 0.215 | $32^{7}$ | 7.8 | LOS A | 1.0 | 25.7 | Full | 1800 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 785 | 1.0 | 1171 | 0.670 | 100 | 12.4 | LOS B | 6.6 | 167.5 | Full | 1800 | 0.0 | 0.0 |
| Lane 3 | 564 | 3.0 | 983 | 0.574 | 100 | 11.3 | LOS B | 4.5 | 114.5 | Short | 250 | 0.0 | 0.0 |
| Approach | 1495 | 1.8 |  | 0.670 |  | 11.6 | LOS B | 6.6 | 167.5 |  |  |  |  |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 373 | 3.0 | 605 | 0.617 | 100 | 18.1 | LOS B | 4.5 | 116.1 | Full | 600 | 0.0 | 0.0 |
| Lane 2 | 181 | 9.2 | 426 | 0.425 | $69^{7}$ | 16.7 | LOS B | 2.2 | 59.6 | Full | 600 | 0.0 | 0.0 |
| Approach | 554 | 5.0 |  | 0.617 |  | 17.7 | LOS B | 4.5 | 116.1 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 318 | 4.1 | 1589 | 0.200 | 100 | 3.8 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 318 | 4.1 |  | 0.200 |  | 3.8 | LOS A | 0.0 | 0.0 |  |  |  |  |
| Intersection | 2367 | 2.8 |  | 0.670 |  | 12.0 | LOS B | 6.6 | 167.5 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

7 Lane underutilisation specified by user
d Dominant lane on roundabout approach

# Appendix X 2037 Total Traffic Conditions Worksheets - Freeway Mainline 














## Appendix Y 2037 Total Traffic Conditions Worksheets - Merge/Diverge Locations




















## Appendix Z 2037 Total Traffic Conditions (No Build) Worksheets - Study Intersections

## SITE LAYOUT

Site: 2037 Total NoBuild NW 319 St and NW 31st Ave Weekday AM
2037 No Build Weekday AM
Roundabout


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Project: H:\projfile\12393 - Cowlitz Reservation Development\Sidra\2014 Analysis\Interchange Roundabouts\102 NW 319th St and NW 31st Avel2037 Analysis - UpdatelNW 319 St and NW 31st Ave_2037 NB.sip6 8001045, KITTELSON AND ASSOCIATES INC, PLUS / Floating

## MOVEMENT SUMMARY

Site: 2037 Total NoBuild NW 319 St and NW 31st Ave Weekday AM
2037 No Build Weekday AM
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dem Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| South: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 5 | 0.0 | 0.226 | 7.0 | LOS A | 1.2 | 34.8 | 0.54 | 0.43 | 33.9 |
| 8 | T1 | 5 | 1.0 | 0.226 | 7.0 | LOS A | 1.2 | 34.8 | 0.54 | 0.43 | 33.9 |
| 18 | R2 | 168 | 23.0 | 0.226 | 7.0 | LOS A | 1.2 | 34.8 | 0.54 | 0.43 | 29.7 |
| Appr |  | 178 | 21.7 | 0.226 | 7.0 | LOS A | 1.2 | 34.8 | 0.54 | 0.43 | 29.9 |
| East: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 193 | 11.0 | 0.258 | 4.2 | LOS A | 1.6 | 43.2 | 0.08 | 0.02 | 32.7 |
| 6 | T1 | 234 | 2.0 | 0.258 | 4.2 | LOS A | 1.6 | 43.2 | 0.08 | 0.02 | 32.1 |
| 16 | R2 | 146 | 1.0 | 0.114 | 3.7 | LOS A | 0.6 | 15.2 | 0.08 | 0.02 | 32.5 |
| Appr |  | 573 | 4.8 | 0.258 | 4.1 | LOS A | 1.6 | 43.2 | 0.08 | 0.02 | 32.4 |
| North: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 110 | 1.0 | 0.124 | 5.0 | LOS A | 0.6 | 15.6 | 0.52 | 0.40 | 30.1 |
| 4 | T1 | 5 | 1.0 | 0.124 | 5.0 | LOS A | 0.6 | 15.6 | 0.52 | 0.40 | 32.4 |
| 14 | R2 | 1 | 1.0 | 0.124 | 5.0 | LOS A | 0.6 | 15.6 | 0.52 | 0.40 | 30.7 |
| Approach |  | 116 | 1.0 | 0.124 | 5.0 | LOS A | 0.6 | 15.6 | 0.52 | 0.40 | 30.3 |
| West: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 1 | 0.0 | 0.232 | 5.9 | LOS A | 1.2 | 31.8 | 0.50 | 0.38 | 34.5 |
| 2 | T1 | 211 | 4.0 | 0.232 | 5.9 | LOS A | 1.2 | 31.8 | 0.50 | 0.38 | 32.4 |
| 12 | R2 | 15 | 0.0 | 0.232 | 5.9 | LOS A | 1.2 | 31.8 | 0.50 | 0.38 | 33.5 |
| Appr |  | 227 | 3.7 | 0.232 | 5.9 | LOS A | 1.2 | 31.8 | 0.50 | 0.38 | 32.5 |
| All V |  | 1094 | 6.9 | 0.258 | 5.1 | LOS A | 1.6 | 43.2 | 0.29 | 0.20 | 31.7 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement LOS $F$ will result if $v / c>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Processed: Tuesday, February 17, 2015 8:13:48 AM SIDRA INTERSECTION 6.0.22.4722
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## LANE SUMMARY

## Site: 2037 Total NoBuild NW 319 St and NW 31st Ave Weekday AM

## 2037 No Build Weekday AM

Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Cap. veh/h | Deg. Satn v/c | $\begin{aligned} & \text { Lane } \\ & \text { Util. } \\ & \% \end{aligned}$ | Average Delay sec | Level of Service | 95\% Back Veh | $\begin{gathered} \text { ueue } \\ \text { Dist } \\ \text { ft } \end{gathered}$ | Lane Config | Lane Length ft | Cap. Adj. \% | Prob. Block. \% |
| South: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 178 | 21.7 | 786 | 0.226 | 100 | 7.0 | LOS A | 1.2 | 34.8 | Full | 1600 | 0.0 | 0.0 |
| Approach | 178 | 21.7 |  | 0.226 |  | 7.0 | LOS A | 1.2 | 34.8 |  |  |  |  |
| East: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 427 | 6.1 | 1655 | 0.258 | 100 | 4.2 | LOS A | 1.6 | 43.2 | Full | 650 | 0.0 | 0.0 |
| Lane 2 | 146 | 1.0 | 1282 | 0.114 | 100 | 3.7 | LOS A | 0.6 | 15.2 | Full | 650 | 0.0 | 0.0 |
| Approach | 573 | 4.8 |  | 0.258 |  | 4.1 | LOS A | 1.6 | 43.2 |  |  |  |  |
| North: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 116 | 1.0 | 932 | 0.124 | 100 | 5.0 | LOS A | 0.6 | 15.6 | Full | 1400 | 0.0 | 0.0 |
| Approach | 116 | 1.0 |  | 0.124 |  | 5.0 | LOS A | 0.6 | 15.6 |  |  |  |  |
| West: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 227 | 3.7 | 980 | 0.232 | 100 | 5.9 | LOS A | 1.2 | 31.8 | Full | 1300 | 0.0 | 0.0 |
| Approach | 227 | 3.7 |  | 0.232 |  | 5.9 | LOS A | 1.2 | 31.8 |  |  |  |  |
| Intersection | 1094 | 6.9 |  | 0.258 |  | 5.1 | LOS A | 1.6 | 43.2 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation
d Dominant lane on roundabout approach

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## SITE LAYOUT

Site: 2037 Total NoBuild NW La Center and SB Ramps Weekday AM
2037 No Build Weekday AM
Roundabout


## MOVEMENT SUMMARY

Site: 2037 Total NoBuild NW La Center and SB Ramps Weekday AM
2037 No Build Weekday AM
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h |  | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue <br> Distance | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 627 | 4.0 | 0.413 | 6.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 32.2 |
| 6 | T1 | 445 | 2.0 | 0.324 | 5.5 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 38.5 |
| Appr |  | 1072 | 3.2 | 0.413 | 5.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 34.0 |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 177 | 13.0 | 0.501 | 14.1 | LOS B | 2.5 | 67.1 | 0.69 | 0.76 | 25.3 |
| 4 | T1 | 3 | 50.0 | 0.501 | 14.1 | LOS B | 2.5 | 67.1 | 0.69 | 0.76 | 27.6 |
| 14 | R2 | 127 | 8.0 | 0.501 | 14.1 | LOS B | 2.5 | 67.1 | 0.69 | 0.76 | 24.7 |
| Appro |  | 307 | 11.3 | 0.501 | 14.1 | LOS B | 2.5 | 67.1 | 0.69 | 0.76 | 25.0 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 2 | T1 | 225 | 20.0 | 0.329 | 9.5 | LOS A | 2.1 | 60.0 | 0.80 | 0.76 | 27.1 |
| 12 | R2 | 264 | 2.0 | 0.161 | 0.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.00 | 35.9 |
| Approach |  | 489 | 10.3 | 0.329 | 4.4 | LOS A | 2.1 | 60.0 | 0.37 | 0.35 | 32.0 |
| All Vehicles |  | 1868 | 6.4 | 0.501 | 6.8 | LOS A | 2.5 | 67.1 | 0.21 | 0.22 | 31.4 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement
LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2037 Total NoBuild NW La Center and SB Ramps Weekday AM

## 2037 No Build Weekday AM

Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Average Delay sec | Level of Service | 95\% Back Veh | ueue Dist ft | Lane Config | Lane Length ft | Cap. Adj. \% | Prob. Block. \% |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 627 | 4.0 | 1518 | 0.413 | 100 | 6.1 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Lane 2 | 445 | 2.0 | 1375 | 0.324 | $78{ }^{5}$ | 5.5 | LOSA | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 1072 | 3.2 |  | 0.413 |  | 5.8 | LOS A | 0.0 | 0.0 |  |  |  |  |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 307 | 11.3 | 613 | 0.501 | 100 | 14.1 | LOS B | 2.5 | 67.1 | Full | 1300 | 0.0 | 0.0 |
| Approach | 307 | 11.3 |  | 0.501 |  | 14.1 | LOS B | 2.5 | 67.1 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 225 | 20.0 | 683 | 0.329 | 100 | 9.5 | LOS A | 2.1 | 60.0 | Full | 650 | 0.0 | 0.0 |
| Lane 2 | 264 | 2.0 | 1642 | 0.161 | 100 | 0.0 | LOSA | 0.0 | 0.0 | Short | 200 | 0.0 | 0.0 |
| Approach | 489 | 10.3 |  | 0.329 |  | 4.4 | LOS A | 2.1 | 60.0 |  |  |  |  |
| Intersection | 1868 | 6.4 |  | 0.501 |  | 6.8 | LOS A | 2.5 | 67.1 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

5 Lane underutilisation determined by program
d Dominant lane on roundabout approach

## SITE LAYOUT

## Site: 2037 Total NoBuild NW La Center and NB Ramps Weekday AM

2037 No Build Weekday AM
Roundabout


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## MOVEMENT SUMMARY

## Site: 2037 Total NoBuild NW La Center and NB Ramps Weekday AM

2037 No Build Weekday AM
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \mathrm{Mov} \\ & \mathrm{ID} \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \\ \hline \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| South: NB Ramp |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 346 | 1.0 | 0.200 | 6.2 | LOS A | 1.0 | 25.5 | 0.55 | 0.45 | 24.7 |
| 8 | T1 | 2 | 50.0 | 0.200 | 6.2 | LOS A | 1.0 | 25.5 | 0.55 | 0.45 | 28.8 |
| 18 | R2 | 408 | 7.0 | 0.375 | 7.2 | LOS A | 2.3 | 59.8 | 0.60 | 0.49 | 29.2 |
| Appr |  | 756 | 4.4 | 0.375 | 6.7 | LOS A | 2.3 | 59.8 | 0.58 | 0.47 | 26.8 |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 6 | T1 | 727 | 4.0 | 0.667 | 13.5 | LOS B | 5.2 | 135.1 | 0.69 | 0.70 | 20.1 |
| 16 | R2 | 227 | 17.0 | 0.420 | 11.5 | LOS B | 2.0 | 57.0 | 0.60 | 0.61 | 25.0 |
| Appr |  | 954 | 7.1 | 0.667 | 13.0 | LOS B | 5.2 | 135.1 | 0.67 | 0.68 | 21.3 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 106 | 17.0 | 0.274 | 4.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.0 |
| 2 | T1 | 297 | 17.0 | 0.274 | 4.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 34.9 |
| Approach |  | 403 | 17.0 | 0.274 | 4.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.0 |
| All Vehicles |  | 2113 | 8.0 | 0.667 | 9.2 | LOS A | 5.2 | 135.1 | 0.51 | 0.48 | 25.4 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2037 Total NoBuild NW La Center and NB Ramps Weekday AM

## 2037 No Build Weekday AM

Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Cap. veh/h | Deg. Satn v/c | $\begin{aligned} & \text { Lane } \\ & \text { Util. } \\ & \% \\ & \hline \end{aligned}$ | Average Delay sec | Level of Service | 95\% Bac Veh | $\begin{array}{r} \text { Queue } \\ \text { Dist } \\ \mathrm{ft} \end{array}$ | Lane Config | Lane Length ft | Cap. Adj. \% | Prob. Block. \% |
| South: NB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 175 | 1.0 | 876 | 0.200 | 100 | 6.1 | LOS A | 1.0 | 25.5 | Full | 1800 | 0.0 | 0.0 |
| Lane 2 | 173 | 1.6 | 866 | 0.200 | 100 | 6.2 | LOS A | 1.0 | 25.5 | Full | 1800 | 0.0 | 0.0 |
| Lane $3^{\text {d }}$ | 408 | 7.0 | 1088 | 0.375 | 100 | 7.2 | LOS A | 2.3 | 59.8 | Short | 250 | 0.0 | 0.0 |
| Approach | 756 | 4.4 |  | 0.375 |  | 6.7 | LOS A | 2.3 | 59.8 |  |  |  |  |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 679 | 4.0 | 1019 | 0.667 | 100 | 13.6 | LOS B | 5.2 | 135.1 | Full | 600 | 0.0 | 0.0 |
| Lane 2 | 275 | 14.7 | 655 | 0.420 | $63^{7}$ | 11.5 | LOS B | 2.0 | 57.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 954 | 7.1 |  | 0.667 |  | 13.0 | LOS B | 5.2 | 135.1 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 403 | 17.0 | 1468 | 0.274 | 100 | 4.7 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 403 | 17.0 |  | 0.274 |  | 4.7 | LOS A | 0.0 | 0.0 |  |  |  |  |
| Intersection | 2113 | 8.0 |  | 0.667 |  | 9.2 | LOS A | 5.2 | 135.1 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
7 Lane underutilisation specified by user
d Dominant lane on roundabout approach

| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 104.8 |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 96 | 439 | 170 | 147 | 728 | 11 | 78 | 2 | 52 |
| Conflicting Peds, \#hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | 250 | - | - | 200 | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 42 | 13 | 0 | 25 | 3 | 20 | 14 | 0 | 25 |
| Mvmt Flow | 96 | 439 | 170 | 147 | 728 | 11 | 78 | 2 | 52 |
| Major/Minor | Major1 |  |  | Major2 |  |  | Minor1 |  |  |
| Conflicting Flow All | 739 | 0 | 0 | 609 | 0 | 0 | 1786 | 1749 | 524 |
| Stage 1 | - | - | - | - | - | - | 716 | 716 |  |
| Stage 2 | - | - | - | - | - | - | 1070 | 1033 |  |
| Critical Hdwy | 4.52 | - | - | 4.35 | - | - | 7.24 | 6.5 | 6.45 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.24 | 5.5 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.24 | 5.5 |  |
| Follow-up Hdwy | 2.578 | - | - | 2.425 | - | - | 3.626 | 4 | 3.525 |
| Pot Cap-1 Maneuver | 711 | - | - | 867 | - | - | $\sim 59$ | 87 | 511 |
| Stage 1 | - | - | - | - | - | - | 403 | 437 | - |
| Stage 2 | - | - | - | - | - | - | 254 | 312 | - |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 711 | - | - | 867 | - | - | ~32 | 62 | 511 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | $\sim 32$ | 62 |  |
| Stage 1 | - | - | - | - | - | - | 349 | 378 |  |
| Stage 2 | - | - | - | - | - | - | 162 | 259 |  |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 1.5 | 1.7 | $\$ 891.1$ |
| HCM LOS |  |  | F |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 51 | 711 | - | - | 867 | - | - | 68 |
| HCM Lane V/C Ratio | 2.588 | 0.135 | - | - | 0.17 | - | - | 1.926 |
| HCM Control Delay (s) | $\$ 891.1$ | 10.9 | - | - | 10 | - | $-\$ 565.3$ |  |
| HCM Lane LOS | F | B | - | - | A | - | - | F |
| HCM 95th \%tile Q(veh) | 13.7 | 0.5 | - | - | 0.6 | - | - | 12 |

Notes
~: Volume exceeds capacity $\quad \$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ *: All major volume in platoon

| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | SBL | SBT | SBR |
| Vol, veh/h | 0 | 5 | 79 |
| Conflicting Peds, \#/hr | Stop | Stop | Stop |
| Sign Control | - | - | None |
| RT Channelized | - | - | - |
| Storage Length | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | 100 | 100 | 100 |
| Peak Hour Factor | 69 | 100 | 30 |
| Heavy Vehicles, \% | 47 | 5 | 79 |
| Mvmt Flow |  |  |  |


| Major/Minor | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Conflicting Flow All | 1771 | 1829 | 734 |
| Stage 1 | 1028 | 1028 | - |
| $\quad$ Stage 2 | 743 | 801 | - |
| Critical Hdwy | 7.79 | 7.5 | 6.5 |
| Critical Hdwy Stg 1 | 6.79 | 6.5 | - |
| Critical Hdwy Stg 2 | 6.79 | 6.5 | - |
| Follow-up Hdwy | 4.121 | 4.9 | 3.57 |
| Pot Cap-1 Maneuver | $\sim 44$ | 44 | 377 |
| $\quad$ Stage 1 | 214 | 213 | - |
| $\quad 319$ | 284 | - |  |
| Stage 2 |  |  |  |
| Motoon blocked, \% Cap-1 Maneuver | $\sim 30$ | 32 | 377 |
| Mov Cap-2 Maneuver | $\sim 30$ | 32 | - |
| Stage 1 | 185 | 177 | - |
| Stage 2 | 247 | 246 | - |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | $\$ 565.3$ |
| HCM LOS | F |

[^32]
## SITE LAYOUT

Site: 2037 Total NoBuild NW 319 St and NW 31st Ave Weekday AM
2037 No Build Weekday AM
Roundabout


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Project: H:\projfile\12393 - Cowlitz Reservation Development\Sidra\2014 Analysis\Interchange Roundabouts\102 NW 319th St and NW 31st Avel2037 Analysis - UpdatelNW 319 St and NW 31st Ave_2037 NB.sip6 8001045, KITTELSON AND ASSOCIATES INC, PLUS / Floating

## MOVEMENT SUMMARY

Site: 2037 Total NoBuild NW 319 St and NW 31st Ave Weekday PM
2037 No Build Weekday PM
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \mathrm{Mov} \\ & \mathrm{ID} \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dem Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles veh | Queue <br> Distance | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| South: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 17 | 0.0 | 0.373 | 10.5 | LOS B | 2.4 | 62.0 | 0.79 | 0.76 | 31.9 |
| 8 | T1 | 10 | 10.0 | 0.373 | 10.5 | LOS B | 2.4 | 62.0 | 0.79 | 0.76 | 31.8 |
| 18 | R2 | 219 | 7.0 | 0.373 | 10.5 | LOS B | 2.4 | 62.0 | 0.79 | 0.76 | 28.6 |
| Appr |  | 246 | 6.6 | 0.373 | 10.5 | LOS B | 2.4 | 62.0 | 0.79 | 0.76 | 29.0 |
| East: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 183 | 2.0 | 0.423 | 6.0 | LOS A | 3.6 | 94.4 | 0.19 | 0.06 | 32.4 |
| 6 | T1 | 487 | 9.0 | 0.423 | 6.0 | LOS A | 3.6 | 94.4 | 0.19 | 0.06 | 31.2 |
| 16 | R2 | 377 | 1.0 | 0.275 | 5.0 | LOS A | 1.9 | 47.5 | 0.17 | 0.05 | 31.5 |
| Appr |  | 1047 | 4.9 | 0.423 | 5.7 | LOS A | 3.6 | 94.4 | 0.18 | 0.06 | 31.6 |
| North: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 308 | 1.0 | 0.433 | 10.7 | LOS B | 3.0 | 75.4 | 0.79 | 0.79 | 27.1 |
| 4 | T1 | 10 | 10.0 | 0.433 | 10.7 | LOS B | 3.0 | 75.4 | 0.79 | 0.79 | 29.7 |
| 14 | R2 | 1 | 0.0 | 0.433 | 10.7 | LOS B | 3.0 | 75.4 | 0.79 | 0.79 | 28.2 |
| Appr |  | 319 | 1.3 | 0.433 | 10.7 | LOS B | 3.0 | 75.4 | 0.79 | 0.79 | 27.2 |
| West: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 1 | 0.0 | 0.474 | 10.6 | LOS B | 3.4 | 87.8 | 0.75 | 0.69 | 31.9 |
| 2 | T1 | 386 | 3.0 | 0.474 | 10.6 | LOS B | 3.4 | 87.8 | 0.75 | 0.69 | 29.4 |
| 12 | R2 | 4 | 0.0 | 0.474 | 10.6 | LOS B | 3.4 | 87.8 | 0.75 | 0.69 | 31.2 |
| Approach |  | 391 | 3.0 | 0.474 | 10.6 | LOS B | 3.4 | 87.8 | 0.75 | 0.69 | 29.4 |
| All Vehicles |  | 2003 | 4.2 | 0.474 | 8.0 | LOS A | 3.6 | 94.4 | 0.46 | 0.38 | 30.0 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2037 Total NoBuild NW 319 St and NW 31st Ave Weekday PM

## 2037 No Build Weekday PM <br> Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \end{gathered}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Average Delay sec | Level of Service | 95\% Bac Veh | $\begin{aligned} & \text { ueue } \\ & \text { Dist } \\ & \text { ft } \end{aligned}$ | Lane Config | Lane Length ft | Cap. Adj. \% | Prob. Block. \% |
| South: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 246 | 6.6 | 660 | 0.373 | 100 | 10.5 | LOS B | 2.4 | 62.0 | Full | 1600 | 0.0 | 0.0 |
| Approach | 246 | 6.6 |  | 0.373 |  | 10.5 | LOS B | 2.4 | 62.0 |  |  |  |  |
| East: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 670 | 7.1 | 1585 | 0.423 | 100 | 6.0 | LOS A | 3.6 | 94.4 | Full | 650 | 0.0 | 0.0 |
| Lane 2 | 377 | 1.0 | 1369 | 0.275 | 100 | 5.0 | LOS A | 1.9 | 47.5 | Full | 650 | 0.0 | 0.0 |
| Approach | 1047 | 4.9 |  | 0.423 |  | 5.7 | LOS A | 3.6 | 94.4 |  |  |  |  |
| North: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 319 | 1.3 | 736 | 0.433 | 100 | 10.7 | LOS B | 3.0 | 75.4 | Full | 1400 | 0.0 | 0.0 |
| Approach | 319 | 1.3 |  | 0.433 |  | 10.7 | LOS B | 3.0 | 75.4 |  |  |  |  |
| West: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 391 | 3.0 | 826 | 0.474 | 100 | 10.6 | LOS B | 3.4 | 87.8 | Full | 1300 | 0.0 | 0.0 |
| Approach | 391 | 3.0 |  | 0.474 |  | 10.6 | LOS B | 3.4 | 87.8 |  |  |  |  |
| Intersection | 2003 | 4.2 |  | 0.474 |  | 8.0 | LOS A | 3.6 | 94.4 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

## SITE LAYOUT

Site: 2037 Total NoBuild NW La Center and SB Ramps Weekday AM
2037 No Build Weekday AM
Roundabout


## MOVEMENT SUMMARY

Site: 2037 Total NoBuild NW La Center and SB Ramps Weekday PM
2037 No Build Weekday PM

Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue <br> Distance $\qquad$ | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 564 | 5.0 | 0.499 | 7.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 33.0 |
| 6 | T1 | 902 | 2.0 | 0.499 | 7.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 37.4 |
| Appr |  | 1466 | 3.2 | 0.499 | 7.4 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.1 |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 217 | 10.0 | 0.631 | 19.4 | LOS B | 3.6 | 95.2 | 0.79 | 0.92 | 23.2 |
| 4 | T1 | 3 | 50.0 | 0.631 | 19.4 | LOS B | 3.6 | 95.2 | 0.79 | 0.92 | 25.6 |
| 14 | R2 | 145 | 2.0 | 0.631 | 19.4 | LOS B | 3.6 | 95.2 | 0.79 | 0.92 | 22.8 |
| Appr |  | 365 | 7.2 | 0.631 | 19.4 | LOS B | 3.6 | 95.2 | 0.79 | 0.92 | 23.1 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 2 | T1 | 304 | 7.0 | 0.380 | 9.1 | LOS A | 2.6 | 69.4 | 0.82 | 0.76 | 28.0 |
| 12 | R2 | 609 | 1.0 | 0.367 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.9 |
| Appr |  | 913 | 3.0 | 0.380 | 3.1 | LOS A | 2.6 | 69.4 | 0.27 | 0.25 | 33.5 |
| All V |  | 2744 | 3.6 | 0.631 | 7.5 | LOS A | 3.6 | 95.2 | 0.20 | 0.21 | 32.0 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

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## LANE SUMMARY

## Site: 2037 Total NoBuild NW La Center and SB Ramps Weekday PM

2037 No Build Weekday PM

Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \\ \hline \end{gathered}$ | Cap. veh/h | Deg. Satn v/c | $\begin{aligned} & \text { Lane } \\ & \text { Util. } \\ & \% \end{aligned}$ | Average Delay sec | Level of Service | 95\% Bac Veh | $\begin{array}{r} \text { ueue } \\ \text { Dist } \\ \text { ft } \end{array}$ | Lane Config | Lane Length ft | $\begin{aligned} & \text { Cap. } \\ & \text { Adj. } \\ & \% \end{aligned}$ | Prob. Block. \% |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 694 | 4.4 | 1390 | 0.499 | 100 | 7.6 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 772 | 2.0 | 1548 | 0.499 | 100 | 7.1 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 1466 | 3.2 |  | 0.499 |  | 7.4 | LOS A | 0.0 | 0.0 |  |  |  |  |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 365 | 7.2 | 579 | 0.631 | 100 | 19.4 | LOS B | 3.6 | 95.2 | Full | 1300 | 0.0 | 0.0 |
| Approach | 365 | 7.2 |  | 0.631 |  | 19.4 | LOS B | 3.6 | 95.2 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 304 | 7.0 | 800 | 0.380 | 100 | 9.1 | LOS A | 2.6 | 69.4 | Full | 650 | 0.0 | 0.0 |
| Lane 2 | 609 | 1.0 | 1658 | 0.367 | 100 | 0.0 | LOS A | 0.0 | 0.0 | Short | 200 | 0.0 | 0.0 |
| Approach | 913 | 3.0 |  | 0.380 |  | 3.1 | LOS A | 2.6 | 69.4 |  |  |  |  |
| Intersection | 2744 | 3.6 |  | 0.631 |  | 7.5 | LOS A | 3.6 | 95.2 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

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Project: H:\projfile\12393-Cowlitz Reservation Development\Sidra\2014 Analysis\Interchange Roundabouts\103 NW La Center and SB Rampsl2037 Analysis - Updatel103 NW La Center and SB Ramps_2037NB.sip6 8001045, KITTELSON AND ASSOCIATES INC, PLUS / Floating

## SITE LAYOUT

## Site: 2037 Total NoBuild NW La Center and NB Ramps Weekday AM

2037 No Build Weekday AM
Roundabout


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## MOVEMENT SUMMARY

## Site: 2037 Total NoBuild NW La Center and NB Ramps Weekday PM

## 2037 No Build Weekday PM

Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \hline \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{array}{r} \text { =lows } \\ \text { HV } \\ \% \\ \hline \end{array}$ | Deg. <br> Satn <br> v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles <br> veh | Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| South: NB Ramp |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 812 | 1.0 | 0.460 | 9.8 | LOS A | 3.1 | 77.0 | 0.70 | 0.66 | 23.5 |
| 8 | T1 | 4 | 50.0 | 0.460 | 9.8 | LOS A | 3.1 | 77.2 | 0.70 | 0.66 | 27.4 |
| 18 | R2 | 648 | 3.0 | 0.597 | 11.1 | LOS B | 5.5 | 140.8 | 0.76 | 0.75 | 27.4 |
| Appr |  | 1464 | 2.0 | 0.597 | 10.4 | LOS B | 5.5 | 140.8 | 0.73 | 0.70 | 25.0 |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 6 | T1 | 654 | 4.0 | 0.805 | 24.6 | LOS C | 7.5 | 192.3 | 0.88 | 1.03 | 16.2 |
| 16 | R2 | 171 | 5.0 | 0.427 | 14.3 | LOS B | 2.1 | 53.9 | 0.73 | 0.76 | 23.7 |
| Approach |  | 825 | 4.2 | 0.805 | 22.4 | LOS C | 7.5 | 192.3 | 0.85 | 0.97 | 17.6 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 177 | 4.0 | 0.326 | 5.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 34.9 |
| 2 | T1 | 345 | 9.0 | 0.326 | 5.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.00 | 34.8 |
| Appr |  | 522 | 7.3 | 0.326 | 5.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 34.9 |
| All Ve |  | 2811 | 3.6 | 0.805 | 12.9 | LOS B | 7.5 | 192.3 | 0.63 | 0.65 | 23.9 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2037 Total NoBuild NW La Center and NB Ramps Weekday PM

## 2037 No Build Weekday PM <br> Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{array}{r} \text { lows } \\ \text { HV } \\ \% \\ \hline \end{array}$ | Cap. veh/h | Deg. Satn v/c | $\begin{aligned} & \text { Lane } \\ & \text { Util. } \\ & \% \\ & \hline \end{aligned}$ | Average Delay sec | Level of Service | 95\% Bac Veh | $\begin{array}{r} \text { Queue } \\ \text { Dist } \\ \mathrm{ft} \end{array}$ | Lane Config | Lane Length ft | $\begin{aligned} & \text { Cap. } \\ & \text { Adj. } \\ & \% \end{aligned}$ | Prob. Block. \% |
| South: NB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 410 | 1.0 | 891 | 0.460 | 100 | 9.7 | LOS A | 3.1 | 77.0 | Full | 1800 | 0.0 | 0.0 |
| Lane 2 | 406 | 1.5 | 883 | 0.460 | 100 | 9.8 | LOS A | 3.1 | 77.2 | Full | 1800 | 0.0 | 0.0 |
| Lane $3^{\text {d }}$ | 648 | 3.0 | 1085 | 0.597 | 100 | 11.1 | LOS B | 5.5 | 140.8 | Short | 250 | 0.0 | 0.0 |
| Approach | 1464 | 2.0 |  | 0.597 |  | 10.4 | LOS B | 5.5 | 140.8 |  |  |  |  |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 607 | 4.0 | 755 | 0.805 | 100 | 25.3 | LOS C | 7.5 | 192.3 | Full | 600 | 0.0 | 0.0 |
| Lane 2 | 218 | 4.8 | 510 | 0.427 | $53^{7}$ | 14.3 | LOS B | 2.1 | 53.9 | Full | 600 | 0.0 | 0.0 |
| Approach | 825 | 4.2 |  | 0.805 |  | 22.4 | LOS C | 7.5 | 192.3 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 522 | 7.3 | 1601 | 0.326 | 100 | 5.0 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 522 | 7.3 |  | 0.326 |  | 5.0 | LOS A | 0.0 | 0.0 |  |  |  |  |
| Intersection | 2811 | 3.6 |  | 0.805 |  | 12.9 | LOS B | 7.5 | 192.3 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
7 Lane underutilisation specified by user
d Dominant lane on roundabout approach

| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 496.3 |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 120 | 756 | 116 | 101 | 470 | 10 | 215 | 8 | 174 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | 250 | - | - | 200 | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 21 | 4 | 25 | 25 | 2 | 20 | 14 | 0 | 25 |
| Mumt Flow | 120 | 756 | 116 | 101 | 470 | 10 | 215 | 8 | 174 |
| Major/Minor | Major1 |  |  | Major2 |  |  | Minor1 |  |  |
| Conflicting Flow All | 480 | 0 | 0 | 872 | 0 | 0 | 1767 | 1736 | 814 |
| Stage 1 | - | - | - | - | - | - | 1054 | 1054 |  |
| Stage 2 | - | - | - | - | - | - | 713 | 682 |  |
| Critical Hdwy | 4.31 | - | - | 4.35 | - | - | 7.24 | 6.5 | 6.45 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.24 | 5.5 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.24 | 5.5 |  |
| Follow-up Hdwy | 2.389 | - | - | 2.425 | - | - | 3.626 | 4 | 3.525 |
| Pot Cap-1 Maneuver | 990 | - | - | 684 | - | - | ~61 | 88 | 345 |
| Stage 1 | - | - | - | - | - | - | 259 | 305 |  |
| Stage 2 | - | - | - | - | - | - | 404 | 453 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 990 | - | - | 684 | - | - | ~39 | 66 | 345 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | ~39 | 66 |  |
| Stage 1 | - | - | - | - | - | - | 228 | 268 |  |
| Stage 2 | - | - | - | - | - | - | 298 | 386 |  |


| Approach | EB | WB | NB |
| :--- | :--- | :---: | :---: |
| HCM Control Delay, s | 1.1 | 1.9 | $\$ 2423.3$ |
| HCM LOS |  |  | F |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 65 | 990 | - | - | 684 | - | - | 54 |
| HCM Lane V/C Ratio | 6.108 | 0.121 | - | - | 0.148 | - | - | 1.981 |
| HCM Control Delay (s) | $\$ 2423.3$ | 9.1 | - | - | 11.2 | - | $-\$ 621.5$ |  |
| HCM Lane LOS | F | A | - | - | $B$ | - | - | F |
| HCM 95th \%tile Q(veh) | 44.8 | 0.4 | - | - | 0.5 | - | - | 10.5 |
| Notes |  |  |  |  |  |  |  |  |

$\sim$ : Volume exceeds capacity $\quad \$$ : Delay exceeds $300 \mathrm{~s} \quad+$ : Computation Not Defined $\quad *:$ All major volume in platoon

| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
|  | SBL | SBT | SBR |
| Movement | 36 | 5 | 66 |
| Vol, veh/h | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | Stop | Stop | Stop |
| Sign Control | - | - | None |
| RT Channelized | - | - | - |
| Storage Length | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | 100 | 100 | 100 |
| Peak Hour Factor | 7 | 100 | 17 |
| Heavy Vehicles, \% | 36 | 5 | 66 |
| Mvmt Flow |  |  |  |


| Major/Minor | Minor2 |  |  |
| :--- | ---: | ---: | ---: |
| Conflicting Flow All | 1822 | 1789 | 475 |
| Stage 1 | 677 | 677 | - |
| $\quad$ Stage 2 | 1145 | 1112 | - |
| Critical Hdwy | 7.17 | 7.5 | 6.37 |
| Critical Hdwy Stg 1 | 6.17 | 6.5 | - |
| Critical Hdwy Stg 2 | 6.17 | 6.5 | - |
| Follow-up Hdwy | 3.563 | 4.9 | 3.453 |
| Pot Cap-1 Maneuver | 58 | 47 | 560 |
| $\quad$ Stage 1 | 434 | 331 | - |
| $\quad 237$ | 191 | - |  |
| Stage 2 |  |  |  |
| Platoon blocked, \% | $\sim 21$ | 35 | 560 |
| Mov Cap-1 Maneuver | $\sim 21$ | 35 | - |
| Mov Cap-2 Maneuver | 381 | 282 | - |
| Stage 1 | 100 | 168 | - |
| Stage 2 |  |  |  |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | $\$ 621.5$ |
| HCM LOS | F |

[^33]
## SITE LAYOUT

Site: 2037 Total NoBuild NW 319 St and NW 31st Ave Weekday AM
2037 No Build Weekday AM
Roundabout


Copyright © 2000-2014 Akcelik and Associates Pty Ltd www.sidrasolutions.com
Project: H:\projfile\12393 - Cowlitz Reservation Development\Sidra\2014 Analysis\Interchange Roundabouts\102 NW 319th St and NW 31st Avel2037 Analysis - UpdatelNW 319 St and NW 31st Ave_2037 NB.sip6 8001045, KITTELSON AND ASSOCIATES INC, PLUS / Floating

## MOVEMENT SUMMARY

Site: 2037 Total NoBuild NW 319 St and NW 31st Ave Weekend
2037 No Build Weekend Peak
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dem Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue <br> Distance | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| South: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 5 | 25.0 | 0.292 | 9.3 | LOS A | 1.8 | 47.0 | 0.79 | 0.74 | 29.9 |
| 8 | T1 | 15 | 1.0 | 0.292 | 9.3 | LOS A | 1.8 | 47.0 | 0.79 | 0.74 | 32.7 |
| 18 | R2 | 168 | 4.0 | 0.292 | 9.3 | LOS A | 1.8 | 47.0 | 0.79 | 0.74 | 29.5 |
| Appr |  | 188 | 4.3 | 0.292 | 9.3 | LOS A | 1.8 | 47.0 | 0.79 | 0.74 | 29.8 |
| East: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 149 | 6.0 | 0.431 | 5.9 | LOS A | 3.7 | 94.9 | 0.16 | 0.04 | 32.7 |
| 6 | T1 | 573 | 2.0 | 0.431 | 5.9 | LOS A | 3.7 | 94.9 | 0.16 | 0.04 | 31.8 |
| 16 | R2 | 493 | 1.0 | 0.345 | 5.6 | LOS A | 2.6 | 65.1 | 0.16 | 0.04 | 31.2 |
| Appr |  | 1215 | 2.1 | 0.431 | 5.8 | LOS A | 3.7 | 94.9 | 0.16 | 0.04 | 31.7 |
| North: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 329 | 1.0 | 0.463 | 11.4 | LOS B | 3.4 | 84.8 | 0.80 | 0.82 | 26.8 |
| 4 | T1 | 10 | 1.0 | 0.463 | 11.4 | LOS B | 3.4 | 84.8 | 0.80 | 0.82 | 29.6 |
| 14 | R2 | 1 | 1.0 | 0.463 | 11.4 | LOS B | 3.4 | 84.8 | 0.80 | 0.82 | 28.0 |
| Appr |  | 340 | 1.0 | 0.463 | 11.4 | LOS B | 3.4 | 84.8 | 0.80 | 0.82 | 26.9 |
| West: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 1 | 1.0 | 0.518 | 11.7 | LOS B | 4.1 | 105.3 | 0.78 | 0.74 | 31.2 |
| 2 | T1 | 410 | 4.0 | 0.518 | 11.7 | LOS B | 4.1 | 105.3 | 0.78 | 0.74 | 28.7 |
| 12 | R2 | 12 | 0.0 | 0.518 | 11.7 | LOS B | 4.1 | 105.3 | 0.78 | 0.74 | 30.7 |
| Approach |  | 423 | 3.9 | 0.518 | 11.7 | LOS B | 4.1 | 105.3 | 0.78 | 0.74 | 28.8 |
| All Vehicles |  | 2166 | 2.5 | 0.518 | 8.1 | LOS A | 4.1 | 105.3 | 0.44 | 0.36 | 30.0 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2037 Total NoBuild NW 319 St and NW 31st Ave Weekend

## 2037 No Build Weekend Peak

Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Average Delay sec | Level of Service | $\begin{gathered} 95 \% \mathrm{Ba} \\ \text { Veh } \end{gathered}$ | $\begin{aligned} & \text { Queue } \\ & \text { Dist } \end{aligned}$ | Lane Config | Lane Length ft | $\begin{aligned} & \text { Cap. } \\ & \text { Adj. } \\ & \% \end{aligned}$ | Prob. Block. \% |
| South: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 188 | 4.3 | 644 | 0.292 | 100 | 9.3 | LOS A | 1.8 | 47.0 | Full | 1600 | 0.0 | 0.0 |
| Approach | 188 | 4.3 |  | 0.292 |  | 9.3 | LOS A | 1.8 | 47.0 |  |  |  |  |
| East: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 722 | 2.8 | 1677 | 0.431 | 100 | 5.9 | LOS A | 3.7 | 94.9 | Full | 650 | 0.0 | 0.0 |
| Lane 2 | 493 | 1.0 | 1431 | 0.345 | 100 | 5.6 | LOS A | 2.6 | 65.1 | Full | 650 | 0.0 | 0.0 |
| Approach | 1215 | 2.1 |  | 0.431 |  | 5.8 | LOS A | 3.7 | 94.9 |  |  |  |  |
| North: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 340 | 1.0 | 735 | 0.463 | 100 | 11.4 | LOS B | 3.4 | 84.8 | Full | 1400 | 0.0 | 0.0 |
| Approach | 340 | 1.0 |  | 0.463 |  | 11.4 | LOS B | 3.4 | 84.8 |  |  |  |  |
| West: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 423 | 3.9 | 816 | 0.518 | 100 | 11.7 | LOS B | 4.1 | 105.3 | Full | 1300 | 0.0 | 0.0 |
| Approach | 423 | 3.9 |  | 0.518 |  | 11.7 | LOS B | 4.1 | 105.3 |  |  |  |  |
| Intersection | 2166 | 2.5 |  | 0.518 |  | 8.1 | LOS A | 4.1 | 105.3 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

## SITE LAYOUT

Site: 2037 Total NoBuild NW La Center and SB Ramps Weekday AM
2037 No Build Weekday AM
Roundabout


## MOVEMENT SUMMARY

Site: 2037 Total NoBuild NW La Center and SB Ramps Weekend
2037 No Build Weekend Peak
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{array}{r} \text { lows } \\ \text { HV } \\ \% \\ \hline \end{array}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back <br> Vehicles <br> veh | Queue <br> Distance <br> ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 563 | 2.0 | 0.533 | 8.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 34.0 |
| 6 | T1 | 1034 | 1.0 | 0.533 | 7.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 37.2 |
| Appr |  | 1597 | 1.4 | 0.533 | 7.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.7 |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 229 | 4.0 | 0.725 | 24.8 | LOS C | 4.9 | 127.3 | 0.85 | 1.04 | 21.5 |
| 4 | T1 | 3 | 0.0 | 0.725 | 24.8 | LOS C | 4.9 | 127.3 | 0.85 | 1.04 | 24.4 |
| 14 | R2 | 182 | 8.0 | 0.725 | 24.8 | LOS C | 4.9 | 127.3 | 0.85 | 1.04 | 20.9 |
| Appr |  | 414 | 5.7 | 0.725 | 24.8 | LOS C | 4.9 | 127.3 | 0.85 | 1.04 | 21.2 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 2 | T1 | 211 | 3.0 | 0.247 | 6.8 | LOS A | 1.6 | 42.0 | 0.77 | 0.67 | 30.2 |
| 12 | R2 | 697 | 2.0 | 0.425 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.8 |
| Approach |  | 908 | 2.2 | 0.425 | 1.6 | LOS A | 1.6 | 42.0 | 0.18 | 0.16 | 34.7 |
| All Vehicles |  | 2919 | 2.2 | 0.725 | 8.3 | LOS A | 4.9 | 127.3 | 0.18 | 0.20 | 31.8 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
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Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2037 Total NoBuild NW La Center and SB Ramps Weekend

## 2037 No Build Weekend Peak

Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Cap. veh/h | Deg. Satn v/c | $\begin{aligned} & \text { Lane } \\ & \text { Util. } \\ & \% \end{aligned}$ | Average Delay sec | Level of Service | $\begin{aligned} & \text { 95\% Bac } \\ & \text { Veh } \end{aligned}$ | $\begin{aligned} & \text { Queue } \\ & \text { Dist } \\ & \mathrm{ft} \end{aligned}$ | Lane Config | Lane Length ft | Cap. Adj. \% | Prob. Block \% |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 763 | 1.7 | 1431 | 0.533 | 100 | 8.0 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 834 | 1.0 | 1564 | 0.533 | 100 | 7.6 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 1597 | 1.4 |  | 0.533 |  | 7.8 | LOS A | 0.0 | 0.0 |  |  |  |  |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 414 | 5.7 | 571 | 0.725 | 100 | 24.8 | LOS C | 4.9 | 127.3 | Full | 1300 | 0.0 | 0.0 |
| Approach | 414 | 5.7 |  | 0.725 |  | 24.8 | LOS C | 4.9 | 127.3 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 211 | 3.0 | 853 | 0.247 | 100 | 6.8 | LOS A | 1.6 | 42.0 | Full | 650 | 0.0 | 0.0 |
| Lane 2 | 697 | 2.0 | 1642 | 0.425 | 100 | 0.0 | LOS A | 0.0 | 0.0 | Short | 200 | 0.0 | 0.0 |
| Approach | 908 | 2.2 |  | 0.425 |  | 1.6 | LOS A | 1.6 | 42.0 |  |  |  |  |
| Intersection | 2919 | 2.2 |  | 0.725 |  | 8.3 | LOS A | 4.9 | 127.3 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
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Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

## SITE LAYOUT

## Site: 2037 Total NoBuild NW La Center and NB Ramps Weekday AM

2037 No Build Weekday AM
Roundabout


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Project: H:\projfile\12393 - Cowlitz Reservation Development\Sidra\2014 Analysis\Interchange Roundabouts\104 NW La Center and NB Ramps\2037 Analysis - Updatel104 NW La Center and NB Ramps_2037NB.sip6 8001045, KITTELSON AND ASSOCIATES INC, PLUS / Floating

## MOVEMENT SUMMARY

## Site: 2037 Total NoBuild NW La Center and NB Ramps Weekend

## 2037 No Build Weekend Peak

Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{gathered} =\text { lows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| South: NB Ramp |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 968 | 1.0 | 0.489 | 9.5 | LOS A | 3.3 | 83.7 | 0.66 | 0.58 | 21.7 |
| 8 | T1 | 2 | 0.0 | 0.489 | 9.5 | LOS A | 3.3 | 83.7 | 0.66 | 0.58 | 27.7 |
| 18 | R2 | 626 | 3.0 | 0.542 | 9.4 | LOS A | 4.2 | 106.5 | 0.67 | 0.58 | 28.2 |
| Appr |  | 1596 | 1.8 | 0.542 | 9.5 | LOS A | 4.2 | 106.5 | 0.66 | 0.58 | 23.8 |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 6 | T1 | 629 | 3.0 | 0.811 | 25.9 | LOS C | 7.4 | 189.1 | 0.89 | 1.04 | 15.8 |
| 16 | R2 | 173 | 12.0 | 0.470 | 17.6 | LOS B | 2.3 | 61.8 | 0.76 | 0.80 | 22.1 |
| Approach |  | 802 | 4.9 | 0.811 | 24.1 | LOS C | 7.4 | 189.1 | 0.86 | 0.99 | 17.1 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 131 | 1.0 | 0.265 | 4.3 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.3 |
| 2 | T1 | 308 | 5.0 | 0.265 | 4.3 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.4 |
| Appr |  | 439 | 3.8 | 0.265 | 4.3 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.4 |
| All Ve |  | 2837 | 3.0 | 0.811 | 12.8 | LOS B | 7.4 | 189.1 | 0.62 | 0.61 | 22.9 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2037 Total NoBuild NW La Center and NB Ramps Weekend

## 2037 No Build Weekend Peak

Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Cap. veh/h | Deg. Satn v/c | $\begin{aligned} & \text { Lane } \\ & \text { Util. } \\ & \% \\ & \hline \end{aligned}$ | Average Delay sec | Level of Service | 95\% Bac Veh | $\begin{array}{r} \text { Queue } \\ \text { Dist } \\ \mathrm{ft} \end{array}$ | Lane Config | Lane Length ft | $\begin{aligned} & \text { Cap. } \\ & \text { Adj. } \\ & \% \end{aligned}$ | Prob. Block. \% |
| South: NB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 485 | 1.0 | 991 | 0.489 | 100 | 9.5 | LOS A | 3.3 | 83.7 | Full | 1800 | 0.0 | 0.0 |
| Lane 2 | 485 | 1.0 | 991 | 0.489 | 100 | 9.5 | LOS A | 3.3 | 83.7 | Full | 1800 | 0.0 | 0.0 |
| Lane $3^{\text {d }}$ | 626 | 3.0 | 1156 | 0.542 | 100 | 9.4 | LOSA | 4.2 | 106.5 | Short | 250 | 0.0 | 0.0 |
| Approach | 1596 | 1.8 |  | 0.542 |  | 9.5 | LOS A | 4.2 | 106.5 |  |  |  |  |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 595 | 3.0 | 733 | 0.811 | 100 | 26.4 | LOS C | 7.4 | 189.1 | Full | 600 | 0.0 | 0.0 |
| Lane 2 | 207 | 10.5 | 441 | 0.470 | $58^{7}$ | 17.6 | LOS B | 2.3 | 61.8 | Full | 600 | 0.0 | 0.0 |
| Approach | 802 | 4.9 |  | 0.811 |  | 24.1 | LOS C | 7.4 | 189.1 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 439 | 3.8 | 1655 | 0.265 | 100 | 4.3 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 439 | 3.8 |  | 0.265 |  | 4.3 | LOS A | 0.0 | 0.0 |  |  |  |  |
| Intersection | 2837 | 3.0 |  | 0.811 |  | 12.8 | LOS B | 7.4 | 189.1 |  |  |  |  |

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Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
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Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
7 Lane underutilisation specified by user
d Dominant lane on roundabout approach

| Intersection |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 366.6 |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR |
| Vol, veh/h | 91 | 727 | 116 | 101 | 478 | 14 | 215 | 8 | 174 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None |
| Storage Length | 250 | - | - | 200 | - | - | - | - |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 |  |
| Peak Hour Factor | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |
| Heavy Vehicles, \% | 13 | 4 | 17 | 0 | 3 | 17 | 11 | 0 | 50 |
| Mumt Flow | 91 | 727 | 116 | 101 | 478 | 14 | 215 | 8 | 174 |
| Major/Minor | Major1 |  |  | Major2 |  |  | Minor1 |  |  |
| Conflicting Flow All | 492 | 0 | 0 | 843 | 0 | 0 | 1677 | 1661 | 785 |
| Stage 1 | - | - | - | - | - | - | 967 | 967 |  |
| Stage 2 | - | - | - | - | - | - | 710 | 694 |  |
| Critical Hdwy | 4.23 | - | - | 4.1 | - | - | 7.21 | 6.5 | 6.7 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.21 | 5.5 |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.21 | 5.5 |  |
| Follow-up Hdwy | 2.317 | - | - | 2.2 | - | - | 3.599 | 4 | 3.75 |
| Pot Cap-1 Maneuver | 1017 | - | - | 802 | - | - | $\sim 72$ | 98 | 326 |
| Stage 1 | - | - | - | - | - | - | 294 | 335 |  |
| Stage 2 | - | - | - | - | - | - | 410 | 447 |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1017 | - | - | 802 | - | - | $\sim 53$ | 78 | 326 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | $\sim 53$ | 78 |  |
| Stage 1 | - | - | - | - | - | - | 268 | 305 |  |
| Stage 2 | - | - | - | - | - | - | 329 | 391 |  |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0.9 | 1.7 | $\$ 1751.4$ |
| HCM LOS |  |  | F |


| Minor Lane/Major Mvmt | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 85 | 1017 | - | - | 802 | - | - | 51 |
| HCM Lane V/C Ratio | 4.671 | 0.089 | - | - | 0.126 | - | - | 1.588 |
| HCM Control Delay (s) | $\$ 1751.4$ | 8.9 | - | - | 10.1 | - | $-\$ 468.6$ |  |
| HCM Lane LOS | F | A | - | - | $B$ | - | - | F |
| HCM 95th \%tile Q(veh) | 42.5 | 0.3 | - | - | 0.4 | - | - | 7.7 |

## Notes

$\sim$ : Volume exceeds capacity $\quad \$$ : Delay exceeds $300 s \quad+$ : Computation Not Defined $\quad$ *: All major volume in platoon

| Intersection |  |  |  |
| :--- | ---: | ---: | ---: |
| Int Delay, s/veh |  |  |  |
| Movement | 36 | 5 | 40 |
| Vol, veh/h | SBT | SBR |  |
| Conflicting Peds, \#/hr | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop |
| RT Channelized | - | - | None |
| Storage Length | - | - | - |
| Veh in Median Storage, \# | - | 0 | - |
| Grade, \% | - | 0 | - |
| Peak Hour Factor | 100 | 100 | 100 |
| Heavy Vehicles, \% | 0 | 0 | 13 |
| Mvmt Flow | 36 | 5 | 40 |
|  |  |  |  |


| Major/Minor | Minor2 |  |  |  |
| :--- | ---: | ---: | ---: | :---: |
| Conflicting Flow All | 1745 | 1712 | 485 |  |
| Stage 1 | 687 | 687 | - |  |
| Stage 2 | 1058 | 1025 | - |  |
| Critical Hdwy | 7.1 | 6.5 | 6.33 |  |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - |  |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - |  |
| Follow-up Hdwy | 3.5 | 4 | 3.417 |  |
| Pot Cap-1 Maneuver | 68 | 91 | 560 |  |
| $\quad$ Stage 1 | 440 | 450 | - |  |
| Stage 2 | 274 | 315 | - |  |
| Platoon blocked, \% | $\sim 25$ | 72 | 560 |  |
| Mov Cap-1 Maneuver | $\sim 25$ | 72 | - |  |
| Mov Cap-2 Maneuver | 401 | 393 | - |  |
| Stage 1 | 113 | 287 | - |  |
| Stage 2 |  |  |  |  |


| Approach | SB |
| :--- | ---: |
| HCM Control Delay, s | $\$ 468.6$ |
| HCM LOS | F |

[^34]
## Appendix AA 2037 Total Traffic Conditions (Build) Worksheets - Study Intersections

## SITE LAYOUT

Site: 2037 Total Build NW La Center and SB Ramps Weekday AM
2037 Build Weekday AM
Roundabout


## MOVEMENT SUMMARY

Site: 2037 Total Build NW La Center and SB Ramps Weekday AM

## 2037 Build Weekday AM

Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \hline \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h |  | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue <br> Distance | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 627 | 4.0 | 0.413 | 6.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 32.2 |
| 6 | T1 | 445 | 2.0 | 0.324 | 5.5 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 38.5 |
| Appr |  | 1072 | 3.2 | 0.413 | 5.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 34.0 |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 177 | 13.0 | 0.233 | 7.2 | LOS A | 0.9 | 24.2 | 0.58 | 0.58 | 27.7 |
| 4 | T1 | 3 | 50.0 | 0.233 | 7.2 | LOS A | 0.9 | 24.2 | 0.58 | 0.58 | 29.7 |
| 14 | R2 | 127 | 8.0 | 0.187 | 7.5 | LOS A | 0.7 | 17.8 | 0.58 | 0.58 | 29.2 |
| Appro |  | 307 | 11.3 | 0.233 | 7.3 | LOS A | 0.9 | 24.2 | 0.58 | 0.58 | 28.3 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 2 | T1 | 225 | 20.0 | 0.183 | 8.1 | LOS A | 1.1 | 31.1 | 0.74 | 0.69 | 23.6 |
| 12 | R2 | 264 | 2.0 | 0.161 | 0.0 | LOSA | 0.0 | 0.0 | 0.00 | 0.00 | 35.6 |
| Approach |  | 489 | 10.3 | 0.183 | 3.7 | LOS A | 1.1 | 31.1 | 0.34 | 0.32 | 29.9 |
| All Vehicles |  | 1868 | 6.4 | 0.413 | 5.5 | LOS A | 1.1 | 31.1 | 0.18 | 0.18 | 31.8 |

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## LANE SUMMARY

## Site: 2037 Total Build NW La Center and SB Ramps Weekday AM

## 2037 Build Weekday AM

Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | Flows HV $\%$ | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Average Delay sec | Level of Service | 95\% Bac Veh | $\begin{aligned} & \text { ueue } \\ & \text { Dist } \\ & \text { ft } \end{aligned}$ | Lane Config | Lane Length | Cap. Adj. \% | Prob. Block. \% |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 627 | 4.0 | 1518 | 0.413 | 100 | 6.1 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Lane 2 | 445 | 2.0 | 1375 | 0.324 | $78^{5}$ | 5.5 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 1072 | 3.2 |  | 0.413 |  | 5.8 | LOS A | 0.0 | 0.0 |  |  |  |  |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 180 | 13.6 | 771 | 0.233 | 100 | 7.2 | LOS A | 0.9 | 24.2 | Full | 1300 | 0.0 | 0.0 |
| Lane 2 | 127 | 8.0 | 678 | 0.187 | 100 | 7.5 | LOS A | 0.7 | 17.8 | Short | 200 | 0.0 | 0.0 |
| Approach | 307 | 11.3 |  | 0.233 |  | 7.3 | LOS A | 0.9 | 24.2 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 99 | 20.0 | 538 | 0.183 | 100 | 9.1 | LOS A | 1.0 | 28.6 | Full | 650 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 126 | 20.0 | 689 | 0.183 | 100 | 7.3 | LOS A | 1.1 | 31.1 | Full | 650 | 0.0 | 0.0 |
| Lane 3 | 264 | 2.0 | 1642 | 0.161 | 100 | 0.0 | LOS A | 0.0 | 0.0 | Short | 200 | 0.0 | 0.0 |
| Approach | 489 | 10.3 |  | 0.183 |  | 3.7 | LOS A | 1.1 | 31.1 |  |  |  |  |
| Intersection | 1868 | 6.4 |  | 0.413 |  | 5.5 | LOS A | 1.1 | 31.1 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
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HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

5 Lane underutilisation determined by program
d Dominant lane on roundabout approach

## SITE LAYOUT

Site: 2037 Total Build NW La Center and NB Ramps Weekday AM
2037 Build Weekday AM
Roundabout


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Roundabout


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| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \\ \hline \end{gathered}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Average Delay sec | Level of Service | 95\% Back <br> Veh | Queue Dist ft | Lane Config | Lane Length | $\begin{aligned} & \text { Cap. } \\ & \text { Adj. } \\ & \% \end{aligned}$ | Prob. Block. \% |
| South: NB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 175 | 1.0 | 1043 | 0.168 | 100 | 5.0 | LOS A | 0.6 | 14.9 | Full | 1800 | 0.0 | 0.0 |
| Lane 2 | 173 | 1.6 | 1033 | 0.168 | 100 | 5.0 | LOS A | 0.6 | 14.9 | Full | 1800 | 0.0 | 0.0 |
| Lane $3^{\text {d }}$ | 408 | 7.0 | 1290 | 0.316 | 100 | 5.7 | LOS A | 1.3 | 33.8 | Short | 250 | 0.0 | 0.0 |
| Approach | 756 | 4.4 |  | 0.316 |  | 5.4 | LOS A | 1.3 | 33.8 |  |  |  |  |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 679 | 4.0 | 1032 | 0.658 | 100 | 13.2 | LOS B | 5.0 | 129.1 | Full | 600 | 0.0 | 0.0 |
| Lane 2 | 275 | 14.7 | 664 | 0.414 | $63^{7}$ | 11.3 | LOS B | 2.0 | 54.8 | Full | 600 | 0.0 | 0.0 |
| Approach | 954 | 7.1 |  | 0.658 |  | 12.7 | LOS B | 5.0 | 129.1 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 185 | 17.0 | 1335 | 0.139 | 100 | 3.8 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 218 | 17.0 | 1570 | 0.139 | 100 | 3.4 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 403 | 17.0 |  | 0.139 |  | 3.6 | LOS A | 0.0 | 0.0 |  |  |  |  |
| Intersection | 2113 | 8.0 |  | 0.658 |  | 8.3 | LOS A | 5.0 | 129.1 |  |  |  |  |

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HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
7 Lane underutilisation specified by user
d Dominant lane on roundabout approach

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | 性 |  | \% | 个 ${ }_{\text {¢ }}$ |  | \% | F |  | \% | F |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 250 |  | 250 | 200 |  | 0 | 250 |  | 0 | 100 |  | 100 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 100 |  |  | 100 |  |  | 100 |  |  | 100 |  |  |
| Lane Util. Factor | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  | 0.958 |  |  | 0.998 |  |  | 0.856 |  |  | 0.859 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1736 | 3138 | 0 | 1752 | 3489 | 0 | 1752 | 1581 | 0 | 1641 | 1415 | 0 |
| Flt Permitted | 0.370 |  |  | 0.421 |  |  | 0.702 |  |  | 0.722 |  |  |
| Satd. Flow (perm) | 676 | 3138 | 0 | 777 | 3489 | 0 | 1295 | 1581 | 0 | 1247 | 1415 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 107 |  |  | 3 |  |  | 52 |  |  | 79 |  |
| Link Speed (mph) |  | 45 |  |  | 45 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 820 |  |  | 2615 |  |  | 1342 |  |  | 1004 |  |
| Travel Time (s) |  | 12.4 |  |  | 39.6 |  |  | 30.5 |  |  | 22.8 |  |
| Lane Group Flow (vph) | 96 | 609 | 0 | 147 | 739 | 0 | 78 | 54 | 0 | 47 | 84 | 0 |
| v/c Ratio | 0.25 | 0.33 |  | 0.33 | 0.37 |  | 0.24 | 0.12 |  | 0.15 | 0.20 |  |
| Control Delay | 10.2 | 6.5 |  | 11.1 | 7.8 |  | 13.6 | 5.2 |  | 12.6 | 5.3 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 10.2 | 6.5 |  | 11.1 | 7.8 |  | 13.6 | 5.2 |  | 12.6 | 5.3 |  |
| Queue Length 50th (ft) | 9 | 24 |  | 14 | 38 |  | 10 | 0 |  | 6 | 1 |  |
| Queue Length 95th (ft) | 55 | 100 |  | 82 | 141 |  | 45 | 19 |  | 30 | 25 |  |
| Internal Link Dist (ft) |  | 740 |  |  | 2535 |  |  | 1262 |  |  | 924 |  |
| Turn Bay Length (ft) | 250 |  |  | 200 |  |  | 250 |  |  | 100 |  |  |
| Base Capacity (vph) | 650 | 3021 |  | 747 | 3355 |  | 1024 | 1261 |  | 986 | 1135 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.15 | 0.20 |  | 0.20 | 0.22 |  | 0.08 | 0.04 |  | 0.05 | 0.07 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type:
Other

|  | $\rangle$ | $\rightarrow$ | , | $\downarrow$ | $\longleftarrow$ | 4 | 4 | $\dagger$ | $p$ | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | 个 ${ }^{\text {¢ }}$ |  | \% | 个 ${ }^{\text {P }}$ |  | \% | F |  | \% | 1 |  |
| Volume (veh/h) | 96 | 439 | 170 | 147 | 728 | 11 | 78 | 2 | 52 | 47 | 5 | 79 |
| Number | 5 | 2 | 12 | 1 | 6 | 16 | 3 | 8 | 18 | 7 | 4 | 14 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1827 | 1724 | 1900 | 1845 | 1840 | 1900 | 1845 | 1847 | 1900 | 1727 | 1647 | 1900 |
| Adj Flow Rate, veh/h | 96 | 439 | 0 | 147 | 728 | 11 | 78 | 2 | 52 | 47 | 5 | 79 |
| Adj No. of Lanes | 1 | 2 | 0 | 1 | 2 | 0 | 1 | 1 | 0 | 1 | 1 | 0 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh, \% | 4 | 13 | 13 | 3 | 3 | 3 | 3 | 0 | 0 | 10 | 100 | 100 |
| Cap, veh/h | 498 | 1807 | 0 | 644 | 1945 | 29 | 360 | 11 | 276 | 382 | 15 | 241 |
| Arrive On Green | 0.55 | 0.55 | 0.00 | 0.55 | 0.55 | 0.55 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 | 0.18 |
| Sat Flow, veh/h | 703 | 3362 | 0 | 937 | 3526 | 53 | 1296 | 58 | 1520 | 1247 | 84 | 1329 |
| Grp Volume(v), veh/h | 96 | 439 | 0 | 147 | 361 | 378 | 78 | 0 | 54 | 47 | 0 | 84 |
| Grp Sat Flow(s),veh/h/ln | 703 | 1638 | 0 | 937 | 1748 | 1831 | 1296 | 0 | 1578 | 1247 | 0 | 1413 |
| Q Serve(g_s), s | 3.4 | 2.6 | 0.0 | 3.6 | 4.4 | 4.4 | 2.1 | 0.0 | 1.1 | 1.2 | 0.0 | 1.9 |
| Cycle Q Clear(g_c), s | 7.7 | 2.6 | 0.0 | 6.2 | 4.4 | 4.4 | 4.0 | 0.0 | 1.1 | 2.3 | 0.0 | 1.9 |
| Prop In Lane | 1.00 |  | 0.00 | 1.00 |  | 0.03 | 1.00 |  | 0.96 | 1.00 |  | 0.94 |
| Lane Grp Cap(c), veh/h | 498 | 1807 | 0 | 644 | 964 | 1010 | 360 | 0 | 287 | 382 | 0 | 256 |
| V/C Ratio(X) | 0.19 | 0.24 | 0.00 | 0.23 | 0.37 | 0.37 | 0.22 | 0.00 | 0.19 | 0.12 | 0.00 | 0.33 |
| Avail Cap(c_a), veh/h | 1085 | 4545 | 0 | 1427 | 2426 | 2540 | 1093 | 0 | 1179 | 1087 | 0 | 1055 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 6.9 | 4.4 | 0.0 | 6.0 | 4.7 | 4.7 | 15.1 | 0.0 | 13.0 | 14.0 | 0.0 | 13.3 |
| Incr Delay (d2), s/veh | 0.2 | 0.1 | 0.0 | 0.2 | 0.2 | 0.2 | 0.3 | 0.0 | 0.3 | 0.1 | 0.0 | 0.7 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.7 | 1.2 | 0.0 | 0.9 | 2.2 | 2.3 | 0.8 | 0.0 | 0.5 | 0.4 | 0.0 | 0.8 |
| LnGrp Delay(d),s/veh | 7.1 | 4.4 | 0.0 | 6.1 | 5.0 | 5.0 | 15.4 | 0.0 | 13.3 | 14.1 | 0.0 | 14.1 |
| LnGrp LOS | A | A |  | A | A | A | B |  | B | B |  | B |
| Approach Vol, veh/h |  | 535 |  |  | 886 |  |  | 132 |  |  | 131 |  |
| Approach Delay, s/veh |  | 4.9 |  |  | 5.2 |  |  | 14.5 |  |  | 14.1 |  |
| Approach LOS |  | A |  |  | A |  |  | B |  |  | B |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Assigned Phs |  | 2 |  | 4 |  | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), s |  | 25.7 |  | 11.8 |  | 25.7 |  | 11.8 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ) , s |  | 5.0 |  | 5.0 |  | 5.0 |  | 5.0 |  |  |  |  |
| Max Green Setting (Gmax), s |  | 52.0 |  | 28.0 |  | 52.0 |  | 28.0 |  |  |  |  |
| Max Q Clear Time (g_c+l1), s |  | 9.7 |  | 4.3 |  | 8.2 |  | 6.0 |  |  |  |  |
| Green Ext Time (p_c), s |  | 10.9 |  | 1.3 |  | 11.0 |  | 1.2 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 6.5 |  |  |  |  |  |  |  |  |  |
| HCM 2010 LOS |  |  | A |  |  |  |  |  |  |  |  |  |

## SITE LAYOUT

Site: 2037 Total Build NW La Center and SB Ramps Weekday AM
2037 Build Weekday AM
Roundabout


## MOVEMENT SUMMARY

## Site: 2037 Total Build NW La Center and SB Ramps Weekday PM

## 2037 Build Weekday PM

Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{gathered} \text { =lows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. <br> Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 564 | 5.0 | 0.499 | 7.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 33.0 |
| 6 | T1 | 902 | 2.0 | 0.499 | 7.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 37.4 |
| Appro |  | 1466 | 3.2 | 0.499 | 7.4 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.1 |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 217 | 10.0 | 0.298 | 8.4 | LOS A | 1.2 | 32.0 | 0.65 | 0.65 | 27.3 |
| 4 | T1 | 3 | 50.0 | 0.298 | 8.4 | LOS A | 1.2 | 32.0 | 0.65 | 0.65 | 29.1 |
| 14 | R2 | 145 | 2.0 | 0.226 | 8.4 | LOS A | 0.8 | 21.0 | 0.63 | 0.63 | 29.0 |
| Appr |  | 365 | 7.2 | 0.298 | 8.4 | LOS A | 1.2 | 32.0 | 0.64 | 0.65 | 27.9 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 2 | T1 | 304 | 7.0 | 0.209 | 7.3 | LOS A | 1.3 | 34.9 | 0.75 | 0.67 | 24.4 |
| 12 | R2 | 609 | 1.0 | 0.367 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.6 |
| Approach |  | 913 | 3.0 | 0.367 | 2.4 | LOS A | 1.3 | 34.9 | 0.25 | 0.22 | 31.8 |
| All Ve |  | 2744 | 3.6 | 0.499 | 5.9 | LOS A | 1.3 | 34.9 | 0.17 | 0.16 | 32.7 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2037 Total Build NW La Center and SB Ramps Weekday PM

## 2037 Build Weekday PM

Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand <br> Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \end{gathered}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Average Delay sec | Level of Service | $\begin{gathered} 95 \% \mathrm{Ba} \\ \text { Veh } \end{gathered}$ | $\begin{aligned} & \text { ueue } \\ & \text { Dist } \\ & \text { ft } \end{aligned}$ | Lane Config | Lane Length ft | Cap. Adj. \% | Prob. Block. \% |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 694 | 4.4 | 1390 | 0.499 | 100 | 7.6 | LOSA | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 772 | 2.0 | 1548 | 0.499 | 100 | 7.1 | LOSA | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 1466 | 3.2 |  | 0.499 |  | 7.4 | LOS A | 0.0 | 0.0 |  |  |  |  |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 220 | 10.5 | 737 | 0.298 | 100 | 8.4 | LOS A | 1.2 | 32.0 | Full | 1300 | 0.0 | 0.0 |
| Lane 2 | 145 | 2.0 | 641 | 0.226 | 100 | 8.4 | LOS A | 0.8 | 21.0 | Short | 200 | 0.0 | 0.0 |
| Approach | 365 | 7.2 |  | 0.298 |  | 8.4 | LOS A | 1.2 | 32.0 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 134 | 7.0 | 643 | 0.209 | 100 | 8.1 | LOSA | 1.2 | 32.0 | Full | 650 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 170 | 7.0 | 811 | 0.209 | 100 | 6.7 | LOSA | 1.3 | 34.9 | Full | 650 | 0.0 | 0.0 |
| Lane 3 | 609 | 1.0 | 1658 | 0.367 | 100 | 0.0 | LOS A | 0.0 | 0.0 | Short | 200 | 0.0 | 0.0 |
| Approach | 913 | 3.0 |  | 0.367 |  | 2.4 | LOS A | 1.3 | 34.9 |  |  |  |  |
| Intersection | 2744 | 3.6 |  | 0.499 |  | 5.9 | LOS A | 1.3 | 34.9 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D)
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

## SITE LAYOUT

Site: 2037 Total Build NW La Center and NB Ramps Weekday AM
2037 Build Weekday AM
Roundabout


## MOVEMENT SUMMARY

## Site: 2037 Total Build NW La Center and NB Ramps Weekday PM

## 2037 Build Weekday PM

Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \hline \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{array}{r} \text { =lows } \\ \text { HV } \\ \% \\ \hline \end{array}$ | $\begin{aligned} & \text { Deg. } \\ & \text { Satn } \\ & \text { v/c } \end{aligned}$ | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| South: NB Ramp ft en er men men |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 812 | 1.0 | 0.381 | 7.3 | LOS A | 1.6 | 40.0 | 0.49 | 0.45 | 24.4 |
| 8 | T1 | 4 | 50.0 | 0.381 | 7.4 | LOSA | 1.6 | 40.1 | 0.49 | 0.45 | 28.4 |
| 18 | R2 | 648 | 3.0 | 0.489 | 7.7 | LOSA | 2.5 | 62.8 | 0.51 | 0.47 | 29.1 |
| Appr |  | 1464 | 2.0 | 0.489 | 7.5 | LOS A | 2.5 | 62.8 | 0.50 | 0.46 | 26.2 |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 6 | T1 | 654 | 4.0 | 0.761 | 20.6 | LOS C | 6.4 | 166.1 | 0.84 | 0.96 | 17.4 |
| 16 | R2 | 171 | 5.0 | 0.403 | 13.1 | LOS B | 1.9 | 48.5 | 0.70 | 0.73 | 24.3 |
| Approach |  | 825 | 4.2 | 0.761 | 19.0 | LOS B | 6.4 | 166.1 | 0.81 | 0.91 | 18.7 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 52 | L2 | $\begin{aligned} & 177 \\ & 345 \end{aligned}$ | $\begin{aligned} & 4.0 \\ & 9.0 \end{aligned}$ | $\begin{aligned} & 0.165 \\ & 0.165 \end{aligned}$ | $\begin{aligned} & 3.7 \\ & 3.4 \end{aligned}$ | $\begin{aligned} & \operatorname{LOS} A \\ & \operatorname{LOS} A \end{aligned}$ | 0.00.0 | 0.0 | 0.00 | 0.00 | 33.0 |
|  | T1 |  |  |  |  |  |  | 0.0 | 0.00 | 0.00 | 32.8 |
| Approach |  | 522 | 7.3 | 0.165 | 3.5 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 32.8 |
| All Ve |  | 2811 | 3.6 | 0.761 | 10.1 | LOS B | 6.4 | 166.1 | 0.50 | 0.51 | 24.9 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2037 Total Build NW La Center and NB Ramps Weekday PM

## 2037 Build Weekday PM

Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Average Delay sec | Level of Service | 95\% Bac Veh | $\begin{aligned} & \text { Queue } \\ & \text { Dist } \\ & \text { ft } \end{aligned}$ | Lane Config | Lane Length ft | $\begin{gathered} \text { Cap. } \\ \text { Adj. } \\ \% \end{gathered}$ | Prob. Block \% |
| South: NB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 410 | 1.0 | 1074 | 0.381 | 100 | 7.3 | LOS A | 1.6 | 40.0 | Full | 1800 | 0.0 | 0.0 |
| Lane 2 | 406 | 1.5 | 1065 | 0.381 | 100 | 7.4 | LOS A | 1.6 | 40.1 | Full | 1800 | 0.0 | 0.0 |
| Lane $3^{\text {d }}$ | 648 | 3.0 | 1325 | 0.489 | 100 | 7.7 | LOS A | 2.5 | 62.8 | Short | 250 | 0.0 | 0.0 |
| Approach | 1464 | 2.0 |  | 0.489 |  | 7.5 | LOS A | 2.5 | 62.8 |  |  |  |  |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 607 | 4.0 | 798 | 0.761 | 100 | 21.1 | LOS C | 6.4 | 166.1 | Full | 600 | 0.0 | 0.0 |
| Lane 2 | 218 | 4.8 | 540 | 0.403 | $53^{7}$ | 13.1 | LOS B | 1.9 | 48.5 | Full | 600 | 0.0 | 0.0 |
| Approach | 825 | 4.2 |  | 0.761 |  | 19.0 | LOS B | 6.4 | 166.1 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 245 | 5.4 | 1485 | 0.165 | 100 | 3.7 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 277 | 9.0 | 1685 | 0.165 | 100 | 3.4 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 522 | 7.3 |  | 0.165 |  | 3.5 | LOS A | 0.0 | 0.0 |  |  |  |  |
| Intersection | 2811 | 3.6 |  | 0.761 |  | 10.1 | LOS B | 6.4 | 166.1 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D)
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
7 Lane underutilisation specified by user
d Dominant lane on roundabout approach

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | 性 |  | \% | 虾 |  | \% | F |  | ${ }^{7}$ | F |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 250 |  | 200 | 300 |  | 0 | 350 |  | 0 | 100 |  | 100 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 100 |  |  | 100 |  |  | 100 |  |  | 100 |  |  |
| Lane Util. Factor | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  | 0.980 |  |  | 0.997 |  |  | 0.857 |  |  | 0.861 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1492 | 3406 | 0 | 1752 | 3516 | 0 | 1752 | 1581 | 0 | 1687 | 1413 | 0 |
| Flt Permitted | 0.478 |  |  | 0.275 |  |  | 0.711 |  |  | 0.643 |  |  |
| Satd. Flow (perm) | 751 | 3406 | 0 | 507 | 3516 | 0 | 1312 | 1581 | 0 | 1142 | 1413 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 30 |  |  | 4 |  |  | 174 |  |  | 66 |  |
| Link Speed (mph) |  | 45 |  |  | 45 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 825 |  |  | 2615 |  |  | 1342 |  |  | 1004 |  |
| Travel Time (s) |  | 12.5 |  |  | 39.6 |  |  | 30.5 |  |  | 22.8 |  |
| Lane Group Flow (vph) | 120 | 872 | 0 | 101 | 480 | 0 | 215 | 182 | 0 | 36 | 71 | 0 |
| v/c Ratio | 0.35 | 0.56 |  | 0.44 | 0.30 |  | 0.53 | 0.30 |  | 0.10 | 0.15 |  |
| Control Delay | 12.8 | 10.7 |  | 17.1 | 8.8 |  | 19.0 | 4.5 |  | 12.9 | 5.3 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 12.8 | 10.7 |  | 17.1 | 8.8 |  | 19.0 | 4.5 |  | 12.9 | 5.3 |  |
| Queue Length 50th (ft) | 16 | 66 |  | 14 | 32 |  | 40 | 1 |  | 6 | 1 |  |
| Queue Length 95th (ft) | 66 | 168 |  | 67 | 87 |  | 117 | 36 |  | 26 | 24 |  |
| Internal Link Dist (ft) |  | 745 |  |  | 2535 |  |  | 1262 |  |  | 924 |  |
| Turn Bay Length (ft) | 250 |  |  | 300 |  |  | 350 |  |  | 100 |  |  |
| Base Capacity (vph) | 715 | 3244 |  | 483 | 3347 |  | 932 | 1173 |  | 811 | 1023 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.17 | 0.27 |  | 0.21 | 0.14 |  | 0.23 | 0.16 |  | 0.04 | 0.07 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type:
Other

|  | 4 | $\rightarrow$ | $\nabla$ | $\checkmark$ | $\leftarrow$ | 4 | 4 | 4 | $p$ | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | 个 ${ }^{\text {a }}$ |  | * | 性 |  | * | F |  | \% | F |  |
| Volume (veh/h) | 120 | 756 | 116 | 101 | 470 | 10 | 215 | 8 | 174 | 36 | 5 | 66 |
| Number | 5 | 2 | 12 | 1 | 6 | 16 | 3 | 8 | 18 | 7 | 4 | 14 |
| Initial Q $(\mathrm{Qb})$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1570 | 1829 | 1900 | 1845 | 1856 | 1900 | 1845 | 1845 | 1900 | 1776 | 1641 | 1900 |
| Adj Flow Rate, veh/h | 120 | 756 | 0 | 101 | 470 | 10 | 215 | 8 | 174 | 36 | 5 | 66 |
| Adj No. of Lanes | 1 | 2 | 0 | 1 | 2 | 0 | 1 | 1 | 0 | 1 | 1 | 0 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh, \% | 21 | 4 | 4 | 3 | 2 | 2 | 3 | 3 | 3 | 7 | 0 | 0 |
| Cap, veh/h | 489 | 1802 | 0 | 416 | 1831 | 39 | 460 | 19 | 417 | 356 | 27 | 362 |
| Arrive On Green | 0.52 | 0.52 | 0.00 | 0.52 | 0.52 | 0.52 | 0.28 | 0.28 | 0.28 | 0.28 | 0.28 | 0.28 |
| Sat Flow, veh/h | 768 | 3567 | 0 | 698 | 3531 | 75 | 1311 | 69 | 1509 | 1141 | 99 | 1310 |
| Grp Volume(v), veh/h | 120 | 756 | 0 | 101 | 234 | 246 | 215 | 0 | 182 | 36 | 0 | 71 |
| Grp Sat Flow(s), veh/h/ln | 768 | 1738 | 0 | 698 | 1763 | 1843 | 1311 | 0 | 1578 | 1141 | 0 | 1410 |
| Q Serve(g_s), s | 5.0 | 6.5 | 0.0 | 5.1 | 3.6 | 3.6 | 7.3 | 0.0 | 4.6 | 1.3 | 0.0 | 1.9 |
| Cycle Q Clear(g_c), s | 8.6 | 6.5 | 0.0 | 11.6 | 3.6 | 3.6 | 9.2 | 0.0 | 4.6 | 5.9 | 0.0 | 1.9 |
| Prop In Lane | 1.00 |  | 0.00 | 1.00 |  | 0.04 | 1.00 |  | 0.96 | 1.00 |  | 0.93 |
| Lane Grp Cap(c), veh/h | 489 | 1802 | 0 | 416 | 914 | 955 | 460 | 0 | 436 | 356 | 0 | 390 |
| V/C Ratio(X) | 0.25 | 0.42 | 0.00 | 0.24 | 0.26 | 0.26 | 0.47 | 0.00 | 0.42 | 0.10 | 0.00 | 0.18 |
| Avail Cap(c_a), veh/h | 878 | 3564 | 0 | 771 | 1808 | 1890 | 904 | 0 | 971 | 742 | 0 | 867 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 8.9 | 7.2 | 0.0 | 10.8 | 6.5 | 6.5 | 16.9 | 0.0 | 14.4 | 16.8 | 0.0 | 13.4 |
| Incr Delay (d2), s/veh | 0.3 | 0.2 | 0.0 | 0.3 | 0.1 | 0.1 | 0.7 | 0.0 | 0.6 | 0.1 | 0.0 | 0.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 1.1 | 3.1 | 0.0 | 1.0 | 1.7 | 1.8 | 2.7 | 0.0 | 2.0 | 0.4 | 0.0 | 0.8 |
| LnGrp Delay(d),s/veh | 9.2 | 7.4 | 0.0 | 11.1 | 6.7 | 6.7 | 17.7 | 0.0 | 15.1 | 17.0 | 0.0 | 13.7 |
| LnGrp LOS | A | A |  | B | A | A | B |  | B | B |  | B |
| Approach Vol, veh/h |  | 876 |  |  | 581 |  |  | 397 |  |  | 107 |  |
| Approach Delay, s/veh |  | 7.6 |  |  | 7.4 |  |  | 16.5 |  |  | 14.8 |  |
| Approach LOS |  | A |  |  | A |  |  | B |  |  | B |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Assigned Phs |  | 2 |  | 4 |  | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), $s$ |  | 30.3 |  | 18.5 |  | 30.3 |  | 18.5 |  |  |  |  |
| Change Period (Y+Rc), s |  | 5.0 |  | 5.0 |  | 5.0 |  | 5.0 |  |  |  |  |
| Max Green Setting (Gmax), s |  | 50.0 |  | 30.0 |  | 50.0 |  | 30.0 |  |  |  |  |
| Max Q Clear Time (g_c+l1), s |  | 10.6 |  | 7.9 |  | 13.6 |  | 11.2 |  |  |  |  |
| Green Ext Time (p_c), s |  | 11.9 |  | 2.4 |  | 11.7 |  | 2.3 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 9.8 |  |  |  |  |  |  |  |  |  |
| HCM 2010 LOS |  |  | A |  |  |  |  |  |  |  |  |  |

## SITE LAYOUT

Site: 2037 Total Build NW La Center and SB Ramps Weekday AM
2037 Build Weekday AM
Roundabout


## MOVEMENT SUMMARY

## Site: 2037 Total Build NW La Center and SB Ramps Weekend

## 2037 Build Weekend Peak

Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \mathrm{Mov} \\ & \mathrm{ID} \end{aligned}$ | OD <br> Mov | Dema Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 563 | 2.0 | 0.533 | 8.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 34.0 |
| 6 | T1 | 1034 | 1.0 | 0.533 | 7.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 37.2 |
| Appr |  | 1597 | 1.4 | 0.533 | 7.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.7 |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 229 | 4.0 | 0.295 | 8.0 | LOS A | 1.2 | 31.1 | 0.66 | 0.66 | 27.8 |
| 4 | T1 | 3 | 0.0 | 0.295 | 8.0 | LOS A | 1.2 | 31.1 | 0.66 | 0.66 | 30.0 |
| 14 | R2 | 182 | 8.0 | 0.318 | 10.8 | LOS B | 1.3 | 33.5 | 0.69 | 0.71 | 27.3 |
| Approach |  | 414 | 5.7 | 0.318 | 9.2 | LOS A | 1.3 | 33.5 | 0.67 | 0.68 | 27.6 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 2 | T1 | 211 | 3.0 | 0.135 | 6.0 | LOS A | 0.8 | 21.5 | 0.72 | 0.61 | 25.3 |
| 12 | R2 | 697 | 2.0 | 0.425 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.6 |
| Appr |  | 908 | 2.2 | 0.425 | 1.4 | LOS A | 0.8 | 21.5 | 0.17 | 0.14 | 33.2 |
| All Ve |  | 2919 | 2.2 | 0.533 | 6.0 | LOS A | 1.3 | 33.5 | 0.15 | 0.14 | 33.3 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2037 Total Build NW La Center and SB Ramps Weekend

## 2037 Build Weekend Peak

Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{array}{r} \text { lows } \\ \text { HV } \\ \% \\ \hline \end{array}$ | Cap. veh/h | Deg. Satn v/c | $\begin{aligned} & \text { Lane } \\ & \text { Util. } \end{aligned}$ | Average Delay sec | Level of Service | 95\% Bac Veh | $\begin{array}{r} \text { ueue } \\ \text { Dist } \\ \text { ft } \end{array}$ | Lane Config | Lane Length ft | Cap. Adj. \% | Prob. Block. \% |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 763 | 1.7 | 1431 | 0.533 | 100 | 8.0 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 834 | 1.0 | 1564 | 0.533 | 100 | 7.6 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 1597 | 1.4 |  | 0.533 |  | 7.8 | LOS A | 0.0 | 0.0 |  |  |  |  |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 232 | 3.9 | 786 | 0.295 | 100 | 8.0 | LOS A | 1.2 | 31.1 | Full | 1300 | 0.0 | 0.0 |
| Lane 2 | 182 | 8.0 | 573 | 0.318 | 100 | 10.8 | LOS B | 1.3 | 33.5 | Short | 200 | 0.0 | 0.0 |
| Approach | 414 | 5.7 |  | 0.318 |  | 9.2 | LOS A | 1.3 | 33.5 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 94 | 3.0 | 692 | 0.135 | 100 | 6.7 | LOS A | 0.8 | 19.8 | Full | 650 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 117 | 3.0 | 867 | 0.135 | 100 | 5.5 | LOS A | 0.8 | 21.5 | Full | 650 | 0.0 | 0.0 |
| Lane 3 | 697 | 2.0 | 1642 | 0.425 | 100 | 0.0 | LOS A | 0.0 | 0.0 | Short | 200 | 0.0 | 0.0 |
| Approach | 908 | 2.2 |  | 0.425 |  | 1.4 | LOS A | 0.8 | 21.5 |  |  |  |  |
| Intersection | 2919 | 2.2 |  | 0.533 |  | 6.0 | LOS A | 1.3 | 33.5 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

## SITE LAYOUT

Site: 2037 Total Build NW La Center and NB Ramps Weekday AM
2037 Build Weekday AM
Roundabout


## MOVEMENT SUMMARY

## Site: 2037 Total Build NW La Center and NB Ramps Weekend

## 2037 Build Weekend Peak

Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \mathrm{Mov} \\ & \mathrm{ID} \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{gathered} \text { lows } \\ \text { HV } \\ \% \\ \hline \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| South: NB Ramp |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 968 | 1.0 | 0.425 | 7.6 | LOS A | 1.9 | 47.2 | 0.47 | 0.41 | 22.3 |
| 8 | T1 | 2 | 0.0 | 0.425 | 7.6 | LOS A | 1.9 | 47.2 | 0.47 | 0.41 | 28.5 |
| 18 | R2 | 626 | 3.0 | 0.461 | 7.2 | LOS A | 2.1 | 54.9 | 0.46 | 0.39 | 29.4 |
| Appr |  | 1596 | 1.8 | 0.461 | 7.4 | LOS A | 2.1 | 54.9 | 0.47 | 0.40 | 24.5 |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 6 | T1 | 629 | 3.0 | 0.763 | 21.3 | LOS C | 6.3 | 161.7 | 0.85 | 0.97 | 17.2 |
| 16 | R2 | 173 | 12.0 | 0.442 | 15.8 | LOS B | 2.1 | 55.6 | 0.73 | 0.77 | 22.9 |
| Appr |  | 802 | 4.9 | 0.763 | 20.1 | LOS C | 6.3 | 161.7 | 0.82 | 0.93 | 18.4 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 131 | 1.0 | 0.134 | 3.4 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 33.5 |
| 2 | T1 | 308 | 5.0 | 0.134 | 3.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 32.9 |
| Approach |  | 439 | 3.8 | 0.134 | 3.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 33.1 |
| All Vehicles |  | 2837 | 3.0 | 0.763 | 10.4 | LOS B | 6.3 | 161.7 | 0.50 | 0.49 | 23.7 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
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HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2037 Total Build NW La Center and NB Ramps Weekend

## 2037 Build Weekend Peak

Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \\ \hline \end{gathered}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Average Delay sec | Level of Service | 95\% Back <br> Veh | Queue Dist ft | Lane Config | Lane Length | $\begin{aligned} & \text { Cap. } \\ & \text { Adj. } \\ & \% \end{aligned}$ | Prob. Block. \% |
| South: NB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 485 | 1.0 | 1142 | 0.425 | 100 | 7.6 | LOS A | 1.9 | 47.2 | Full | 1800 | 0.0 | 0.0 |
| Lane 2 | 485 | 1.0 | 1143 | 0.425 | 100 | 7.6 | LOS A | 1.9 | 47.2 | Full | 1800 | 0.0 | 0.0 |
| Lane $3^{\text {d }}$ | 626 | 3.0 | 1357 | 0.461 | 100 | 7.2 | LOS A | 2.1 | 54.9 | Short | 250 | 0.0 | 0.0 |
| Approach | 1596 | 1.8 |  | 0.461 |  | 7.4 | LOS A | 2.1 | 54.9 |  |  |  |  |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 595 | 3.0 | 780 | 0.763 | 100 | 21.6 | LOS C | 6.3 | 161.7 | Full | 600 | 0.0 | 0.0 |
| Lane 2 | 207 | 10.5 | 469 | 0.442 | $58^{7}$ | 15.8 | LOS B | 2.1 | 55.6 | Full | 600 | 0.0 | 0.0 |
| Approach | 802 | 4.9 |  | 0.763 |  | 20.1 | LOS C | 6.3 | 161.7 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 205 | 2.4 | 1527 | 0.134 | 100 | 3.4 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 234 | 5.0 | 1749 | 0.134 | 100 | 3.0 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 439 | 3.8 |  | 0.134 |  | 3.2 | LOS A | 0.0 | 0.0 |  |  |  |  |
| Intersection | 2837 | 3.0 |  | 0.763 |  | 10.4 | LOS B | 6.3 | 161.7 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
7 Lane underutilisation specified by user
d Dominant lane on roundabout approach

| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | 中 ${ }^{\text {P }}$ |  | \% | 性 |  | \% | F |  | ${ }^{7}$ | F |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ft) | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| Grade (\%) |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Storage Length (ft) | 250 |  | 250 | 200 |  | 0 | 250 |  | 0 | 100 |  | 100 |
| Storage Lanes | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 100 |  |  | 100 |  |  | 100 |  |  | 100 |  |  |
| Lane Util. Factor | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  | 0.979 |  |  | 0.996 |  |  | 0.857 |  |  | 0.867 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 1597 | 3403 | 0 | 1752 | 3477 | 0 | 1752 | 1583 | 0 | 1805 | 1477 | 0 |
| Flt Permitted | 0.472 |  |  | 0.289 |  |  | 0.728 |  |  | 0.643 |  |  |
| Satd. Flow (perm) | 794 | 3403 | 0 | 533 | 3477 | 0 | 1343 | 1583 | 0 | 1222 | 1477 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 31 |  |  | 5 |  |  | 174 |  |  | 40 |  |
| Link Speed (mph) |  | 45 |  |  | 45 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 826 |  |  | 2615 |  |  | 1342 |  |  | 1004 |  |
| Travel Time (s) |  | 12.5 |  |  | 39.6 |  |  | 30.5 |  |  | 22.8 |  |
| Lane Group Flow (vph) | 91 | 843 | 0 | 101 | 492 | 0 | 215 | 182 | 0 | 36 | 45 | 0 |
| v/c Ratio | 0.26 | 0.55 |  | 0.42 | 0.32 |  | 0.52 | 0.30 |  | 0.10 | 0.09 |  |
| Control Delay | 11.2 | 10.7 |  | 16.5 | 9.0 |  | 17.9 | 4.3 |  | 12.1 | 5.7 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 11.2 | 10.7 |  | 16.5 | 9.0 |  | 17.9 | 4.3 |  | 12.1 | 5.7 |  |
| Queue Length 50th (ft) | 11 | 63 |  | 14 | 33 |  | 39 | 1 |  | 6 | 1 |  |
| Queue Length 95th (ft) | 50 | 162 |  | 66 | 90 |  | 112 | 35 |  | 25 | 18 |  |
| Internal Link Dist (ft) |  | 746 |  |  | 2535 |  |  | 1262 |  |  | 924 |  |
| Turn Bay Length (ft) | 250 |  |  | 200 |  |  | 250 |  |  | 100 |  |  |
| Base Capacity (vph) | 756 | 3243 |  | 508 | 3312 |  | 1007 | 1231 |  | 917 | 1118 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.12 | 0.26 |  | 0.20 | 0.15 |  | 0.21 | 0.15 |  | 0.04 | 0.04 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Area Type:
Other

|  | $\rangle$ | $\rightarrow$ | 7 | $\checkmark$ | 4 | 4 | 4 | $\dagger$ | $>$ | $\checkmark$ | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | 个 ${ }^{\text {P }}$ |  | \% | 个t |  | \% | F |  | \% | F |  |
| Volume (veh/h) | 91 | 727 | 116 | 101 | 478 | 14 | 215 | 8 | 174 | 36 | 5 | 40 |
| Number | 5 | 2 | 12 | 1 | 6 | 16 | 3 | 8 | 18 | 7 | 4 | 14 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1681 | 1829 | 1900 | 1845 | 1838 | 1900 | 1845 | 1847 | 1900 | 1900 | 1703 | 1900 |
| Adj Flow Rate, veh/h | 91 | 727 | 0 | 101 | 478 | 14 | 215 | 8 | 174 | 36 | 5 | 40 |
| Adj No. of Lanes | 1 | 2 | 0 | 1 | 2 | 0 | 1 | 1 | 0 | 1 | 1 | 0 |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Percent Heavy Veh, \% | 13 | 4 | 4 | 3 | 3 | 3 | 3 | 0 | 0 | 0 | 0 | 0 |
| Cap, veh/h | 517 | 1796 | 0 | 439 | 1790 | 52 | 479 | 18 | 394 | 361 | 43 | 342 |
| Arrive On Green | 0.52 | 0.52 | 0.00 | 0.52 | 0.52 | 0.52 | 0.26 | 0.26 | 0.26 | 0.26 | 0.26 | 0.26 |
| Sat Flow, veh/h | 813 | 3567 | 0 | 718 | 3464 | 101 | 1342 | 69 | 1511 | 1221 | 164 | 1309 |
| Grp Volume(v), veh/h | 91 | 727 | 0 | 101 | 241 | 251 | 215 | 0 | 182 | 36 | 0 | 45 |
| Grp Sat Flow(s),veh/h/ln | 813 | 1738 | 0 | 718 | 1746 | 1820 | 1342 | 0 | 1580 | 1221 | 0 | 1472 |
| Q Serve(g_s), s | 3.2 | 5.8 | 0.0 | 4.5 | 3.5 | 3.5 | 6.5 | 0.0 | 4.3 | 1.1 | 0.0 | 1.0 |
| Cycle Q Clear(g_c), s | 6.7 | 5.8 | 0.0 | 10.3 | 3.5 | 3.5 | 7.6 | 0.0 | 4.3 | 5.5 | 0.0 | 1.0 |
| Prop In Lane | 1.00 |  | 0.00 | 1.00 |  | 0.06 | 1.00 |  | 0.96 | 1.00 |  | 0.89 |
| Lane Grp Cap(c), veh/h | 517 | 1796 | 0 | 439 | 902 | 940 | 479 | 0 | 413 | 361 | 0 | 384 |
| V/C Ratio(X) | 0.18 | 0.40 | 0.00 | 0.23 | 0.27 | 0.27 | 0.45 | 0.00 | 0.44 | 0.10 | 0.00 | 0.12 |
| Avail Cap(c_a), veh/h | 982 | 3783 | 0 | 849 | 1900 | 1981 | 1053 | 0 | 1088 | 883 | 0 | 1014 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 8.0 | 6.6 | 0.0 | 9.8 | 6.1 | 6.1 | 15.6 | 0.0 | 13.9 | 16.2 | 0.0 | 12.7 |
| Incr Delay (d2), s/veh | 0.2 | 0.1 | 0.0 | 0.3 | 0.2 | 0.2 | 0.7 | 0.0 | 0.7 | 0.1 | 0.0 | 0.1 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.7 | 2.8 | 0.0 | 0.9 | 1.7 | 1.8 | 2.5 | 0.0 | 2.0 | 0.4 | 0.0 | 0.4 |
| LnGrp Delay(d),s/veh | 8.1 | 6.8 | 0.0 | 10.0 | 6.3 | 6.2 | 16.2 | 0.0 | 14.6 | 16.3 | 0.0 | 12.8 |
| LnGrp LOS | A | A |  | B | A | A | B |  | B | B |  | B |
| Approach Vol, veh/h |  | 818 |  |  | 593 |  |  | 397 |  |  | 81 |  |
| Approach Delay, s/veh |  | 6.9 |  |  | 6.9 |  |  | 15.5 |  |  | 14.4 |  |
| Approach LOS |  | A |  |  | A |  |  | B |  |  | B |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Assigned Phs |  | 2 |  | 4 |  | 6 |  | 8 |  |  |  |  |
| Phs Duration ( $G+Y+R \mathrm{c}$ ), $s$ |  | 28.3 |  | 16.8 |  | 28.3 |  | 16.8 |  |  |  |  |
| Change Period ( $\mathrm{Y}+\mathrm{Rc}$ ) , s |  | 5.0 |  | 5.0 |  | 5.0 |  | 5.0 |  |  |  |  |
| Max Green Setting (Gmax), s |  | 49.0 |  | 31.0 |  | 49.0 |  | 31.0 |  |  |  |  |
| Max Q Clear Time (g_ctl1), s |  | 8.7 |  | 7.5 |  | 12.3 |  | 9.6 |  |  |  |  |
| Green Ext Time (p_c), s |  | 11.2 |  | 2.2 |  | 11.0 |  | 2.2 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 9.0 |  |  |  |  |  |  |  |  |  |
| HCM 2010 LOS |  |  | A |  |  |  |  |  |  |  |  |  |

# Appendix BB 2037 Trip Distribution Sensitivity Analysis Worksheets for 85/15 Split 

## SITE LAYOUT

Site: 2037 Total NoBuild NW 319 St and NW 31st Ave Weekday AM
2037 No Build Weekday AM
Roundabout


Copyright © 2000-2014 Akcelik and Associates Pty Ltd www.sidrasolutions.com
Project: H:\projfile\12393 - Cowlitz Reservation Development\Sidra\2014 Analysis\Interchange Roundabouts\102 NW 319th St and NW 31st Avel2037 Analysis - UpdatelNW 319 St and NW 31st Ave_2037 NB.sip6 8001045, KITTELSON AND ASSOCIATES INC, PLUS / Floating

## MOVEMENT SUMMARY

Site: 2037 Total NoBuild NW 319 St and NW 31st Ave Weekday AM
2037 No Build Weekday AM
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dem Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| South: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 5 | 0.0 | 0.226 | 7.0 | LOS A | 1.2 | 34.8 | 0.54 | 0.43 | 33.9 |
| 8 | T1 | 5 | 1.0 | 0.226 | 7.0 | LOS A | 1.2 | 34.8 | 0.54 | 0.43 | 33.9 |
| 18 | R2 | 168 | 23.0 | 0.226 | 7.0 | LOS A | 1.2 | 34.8 | 0.54 | 0.43 | 29.7 |
| Appr |  | 178 | 21.7 | 0.226 | 7.0 | LOS A | 1.2 | 34.8 | 0.54 | 0.43 | 29.9 |
| East: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 193 | 11.0 | 0.258 | 4.2 | LOS A | 1.6 | 43.2 | 0.08 | 0.02 | 32.7 |
| 6 | T1 | 234 | 2.0 | 0.258 | 4.2 | LOS A | 1.6 | 43.2 | 0.08 | 0.02 | 32.1 |
| 16 | R2 | 146 | 1.0 | 0.114 | 3.7 | LOS A | 0.6 | 15.2 | 0.08 | 0.02 | 32.5 |
| Appr |  | 573 | 4.8 | 0.258 | 4.1 | LOS A | 1.6 | 43.2 | 0.08 | 0.02 | 32.4 |
| North: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 110 | 1.0 | 0.124 | 5.0 | LOS A | 0.6 | 15.6 | 0.52 | 0.40 | 30.1 |
| 4 | T1 | 5 | 1.0 | 0.124 | 5.0 | LOS A | 0.6 | 15.6 | 0.52 | 0.40 | 32.4 |
| 14 | R2 | 1 | 1.0 | 0.124 | 5.0 | LOS A | 0.6 | 15.6 | 0.52 | 0.40 | 30.7 |
| Approach |  | 116 | 1.0 | 0.124 | 5.0 | LOS A | 0.6 | 15.6 | 0.52 | 0.40 | 30.3 |
| West: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 1 | 0.0 | 0.232 | 5.9 | LOS A | 1.2 | 31.8 | 0.50 | 0.38 | 34.5 |
| 2 | T1 | 211 | 4.0 | 0.232 | 5.9 | LOS A | 1.2 | 31.8 | 0.50 | 0.38 | 32.4 |
| 12 | R2 | 15 | 0.0 | 0.232 | 5.9 | LOS A | 1.2 | 31.8 | 0.50 | 0.38 | 33.5 |
| Appr |  | 227 | 3.7 | 0.232 | 5.9 | LOS A | 1.2 | 31.8 | 0.50 | 0.38 | 32.5 |
| All V |  | 1094 | 6.9 | 0.258 | 5.1 | LOS A | 1.6 | 43.2 | 0.29 | 0.20 | 31.7 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement LOS $F$ will result if $v / c>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

Processed: Tuesday, February 17, 2015 8:13:48 AM SIDRA INTERSECTION 6.0.22.4722
Project: H:\projfile\12393 - Cowlitz Reservation Development\Sidra\2014 Analysis\Interchange Roundabouts\102 NW 319th St and NW 31st Avel2037 Analysis - UpdatelNW 319 St and NW 31st Ave_2037 NB.sip6 8001045, KITTELSON AND ASSOCIATES INC, PLUS / Floating

## LANE SUMMARY

## Site: 2037 Total Build NW 319 St and NW 31st Ave Weekday AM 85_15 Split

2037 Build Total Traffic Weekday AM
85/15 Split Sensitivity Analysis
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand F Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Cap. veh/h | Deg. Satn v/c | $\begin{aligned} & \text { Lane } \\ & \text { Util. } \\ & \% \end{aligned}$ | Average Delay sec | Level of Service | 95\% Back <br> Veh | $\begin{gathered} \text { ueue } \\ \text { Dist } \\ \text { ft } \end{gathered}$ | Lane Config | Lane Length ft | $\begin{aligned} & \text { Cap. } \\ & \text { Adj. } \\ & \% \end{aligned}$ | Prob. Block. \% |
| South: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 178 | 21.7 | 792 | 0.225 | 100 | 7.0 | LOS A | 1.2 | 34.2 | Full | 1600 | 0.0 | 0.0 |
| Approach | 178 | 21.7 |  | 0.225 |  | 7.0 | LOS A | 1.2 | 34.2 |  |  |  |  |
| East: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 325 | 7.3 | 1624 | 0.200 | 100 | 3.8 | LOS A | 1.2 | 31.6 | Full | 650 | 0.0 | 0.0 |
| Lane 2 | 248 | 1.0 | 1469 | 0.169 | 100 | 3.8 | LOS A | 1.0 | 24.2 | Full | 650 | 0.0 | 0.0 |
| Approach | 573 | 4.6 |  | 0.200 |  | 3.8 | LOS A | 1.2 | 31.6 |  |  |  |  |
| North: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 193 | 1.0 | 1004 | 0.192 | 100 | 5.4 | LOS A | 1.0 | 24.7 | Full | 1400 | 0.0 | 0.0 |
| Approach | 193 | 1.0 |  | 0.192 |  | 5.4 | LOS A | 1.0 | 24.7 |  |  |  |  |
| West: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 150 | 3.6 | 922 | 0.163 | 100 | 5.5 | LOS A | 0.8 | 21.7 | Full | 1300 | 0.0 | 0.0 |
| Approach | 150 | 3.6 |  | 0.163 |  | 5.5 | LOS A | 0.8 | 21.7 |  |  |  |  |
| Intersection | 1094 | 6.6 |  | 0.225 |  | 4.8 | LOS A | 1.2 | 34.2 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

Processed: Tuesday, February 17, 2015 8:57:24 AM
SIDRA INTERSECTION 6.0.22.4722
Project: H:\projfile\12393 - Cowlitz Reservation Development\Sidra\2014 Analysis\Interchange Roundabouts\102
NW 319th St and NW 31st Avel2037 Analysis - UpdatelNW 319 St and NW 31st Ave 85_15.sip6
8001045, KITTELSON AND ASSOCIATES INC, PLUS / Floating

## SITE LAYOUT

Site: 2037 Total Build NW La Center and SB Ramps Weekday AM 85_15 Split
2037 Build Weekday AM
Roundabout


## MOVEMENT SUMMARY

Site: 2037 Total Build NW La Center and SB Ramps Weekday AM 85_15 Split

## 2037 Build Weekday AM

Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mov OD  <br> ID Mov | Dema Total veh/h | $\begin{gathered} \text { =lows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue <br> Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| East: NW La Center Rd 0 |  |  |  |  |  |  |  |  |  |  |
| 1 L 2 | 627 | 4.0 | 0.439 | 6.4 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 32.6 |
| $6 \quad$ T1 | 445 | 2.0 | 0.439 | 5.5 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 37.7 |
| Approach | 1072 | 3.2 | 0.439 | 6.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 34.0 |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |
| 7 L2 | 177 | 13.0 | 0.236 | 7.3 | LOS A | 0.9 | 25.0 | 0.59 | 0.59 | 27.7 |
| 4 T1 | 3 | 50.0 | 0.236 | 7.3 | LOS A | 0.9 | 25.0 | 0.59 | 0.59 | 29.6 |
| 14 R2 | 127 | 8.0 | 0.189 | 7.6 | LOS A | 0.7 | 18.3 | 0.58 | 0.58 | 29.2 |
| Approach | 307 | 11.3 | 0.236 | 7.4 | LOS A | 0.9 | 25.0 | 0.59 | 0.59 | 28.3 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |
| 2 T1 | 225 | 20.0 | 0.183 | 8.1 | LOS A | 1.1 | 31.2 | 0.74 | 0.69 | 23.6 |
| 12 R2 | 264 | 2.0 | 0.161 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.6 |
| Approach | 489 | 10.3 | 0.183 | 3.7 | LOS A | 1.1 | 31.2 | 0.34 | 0.32 | 29.9 |
| All Vehicles | 1868 | 6.4 | 0.439 | 5.6 | LOS A | 1.1 | 31.2 | 0.19 | 0.18 | 31.8 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement
LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2037 Total Build NW La Center and SB Ramps Weekday AM 85_15 Split

## 2037 Build Weekday AM

Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Average Delay sec | Level of Service | 95\% Back <br> Veh | ueue Dist $\mathrm{ft}$ | Lane Config | Lane Length ft | Cap. <br> Adj. <br> \% | Prob. Block. \% |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 667 | 3.9 | 1520 | 0.439 | 100 | 6.4 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Lane 2 | 405 | 2.0 | 1339 | 0.303 | $69^{7}$ | 5.4 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 1072 | 3.2 |  | 0.439 |  | 6.0 | LOS A | 0.0 | 0.0 |  |  |  |  |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 180 | 13.6 | 763 | 0.236 | 100 | 7.3 | LOS A | 0.9 | 25.0 | Full | 1300 | 0.0 | 0.0 |
| Lane 2 | 127 | 8.0 | 671 | 0.189 | 100 | 7.6 | LOS A | 0.7 | 18.3 | Short | 200 | 0.0 | 0.0 |
| Approach | 307 | 11.3 |  | 0.236 |  | 7.4 | LOS A | 0.9 | 25.0 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 99 | 20.0 | 538 | 0.183 | 100 | 9.1 | LOS A | 1.0 | 28.6 | Full | 650 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 126 | 20.0 | 689 | 0.183 | 100 | 7.3 | LOS A | 1.1 | 31.2 | Full | 650 | 0.0 | 0.0 |
| Lane 3 | 264 | 2.0 | 1642 | 0.161 | 100 | 0.0 | LOS A | 0.0 | 0.0 | Short | 200 | 0.0 | 0.0 |
| Approach | 489 | 10.3 |  | 0.183 |  | 3.7 | LOS A | 1.1 | 31.2 |  |  |  |  |
| Intersection | 1868 | 6.4 |  | 0.439 |  | 5.6 | LOS A | 1.1 | 31.2 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

7 Lane underutilisation specified by user
d Dominant lane on roundabout approach

## SITE LAYOUT

Site: 2037 Total Build NW La Center and NB Ramps Weekday AM 85_15 Split
2037 Total Traffic Weekday AM
85/15 Split Sensitivity Analysis
Roundabout


## MOVEMENT SUMMARY

## Site: 2037 Total Build NW La Center and NB Ramps Weekday AM 85_15 Split

2037 Total Traffic Weekday AM
85/15 Split Sensitivity Analysis
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \hline \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h |  | $\begin{aligned} & \text { Deg. } \\ & \text { Satn } \\ & \text { v/c } \end{aligned}$ | Average Delay sec | Level of Service | 95\% Back <br> Vehicles veh | Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| South: NB Ramp |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 346 | 1.0 | 0.243 | 5.3 | LOS A | 0.9 | 23.1 | 0.41 | 0.34 | 25.0 |
| 8 | T1 | 2 | 50.0 | 0.243 | 5.5 | LOS A | 0.9 | 23.1 | 0.41 | 0.35 | 29.1 |
| 18 | R2 | 408 | 7.0 | 0.316 | 5.7 | LOS A | 1.3 | 33.8 | 0.42 | 0.35 | 30.0 |
| Appr |  | 756 | 4.4 | 0.316 | 5.5 | LOS A | 1.3 | 33.8 | 0.41 | 0.34 | 27.4 |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 6 | T1 | 727 | 4.0 | 0.664 | 13.4 | LOS B | 5.4 | 139.7 | 0.69 | 0.69 | 20.2 |
| 16 | R2 | 227 | 17.0 | 0.418 | 11.4 | LOS B | 2.1 | 57.7 | 0.60 | 0.61 | 25.1 |
| Appro |  | 954 | 7.1 | 0.664 | 12.9 | LOS B | 5.4 | 139.7 | 0.67 | 0.67 | 21.3 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 106 | 17.0 | 0.139 | 3.8 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 33.4 |
| 2 | T1 | 297 | 17.0 | 0.139 | 3.5 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 32.4 |
| Approach |  | 403 | 17.0 | 0.139 | 3.6 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 32.7 |
| All Vehicles |  | 2113 | 8.0 | 0.664 | 8.5 | LOS A | 5.4 | 139.7 | 0.45 | 0.43 | 25.5 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement
LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2037 Total Build NW La Center and NB Ramps Weekday AM 85_15 Split

2037 Total Traffic Weekday AM
85/15 Split Sensitivity Analysis
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Cap. veh/h | Deg. Satn v/c | $\begin{aligned} & \text { Lane } \\ & \text { Util. } \\ & \% \end{aligned}$ | Average Delay sec | Level of Service | 95\% Bac <br> Veh | $\begin{aligned} & \text { Queue } \\ & \text { Dist } \\ & \mathrm{ft} \end{aligned}$ | Lane Config | Lane Length ft | $\begin{array}{r} \text { Cap. } \\ \text { Adj. } \\ \% \end{array}$ | Prob. Block \% |
| South: NB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 78 | 1.0 | 919 | 0.085 | $35^{7}$ | 4.7 | LOS A | 0.3 | 7.1 | Short | 200 | 0.0 | 0.0 |
| Lane 2 | 270 | 1.4 | 1109 | 0.243 | 100 | 5.5 | LOS A | 0.9 | 23.1 | Full | 1800 | 0.0 | 0.0 |
| Lane $3^{\text {d }}$ | 408 | 7.0 | 1290 | 0.316 | 100 | 5.7 | LOS A | 1.3 | 33.8 | Short | 250 | 0.0 | 0.0 |
| Approach | 756 | 4.4 |  | 0.316 |  | 5.5 | LOS A | 1.3 | 33.8 |  |  |  |  |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 677 | 4.0 | 1021 | 0.664 | 100 | 13.5 | LOS B | 5.4 | 139.7 | Full | 600 | 0.0 | 0.0 |
| Lane 2 | 277 | 14.7 | 661 | 0.418 | $63^{7}$ | 11.4 | LOS B | 2.1 | 57.7 | Full | 600 | 0.0 | 0.0 |
| Approach | 954 | 7.1 |  | 0.664 |  | 12.9 | LOS B | 5.4 | 139.7 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 185 | 17.0 | 1335 | 0.139 | 100 | 3.8 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 218 | 17.0 | 1570 | 0.139 | 100 | 3.4 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 403 | 17.0 |  | 0.139 |  | 3.6 | LOS A | 0.0 | 0.0 |  |  |  |  |
| Intersection | 2113 | 8.0 |  | 0.664 |  | 8.5 | LOS A | 5.4 | 139.7 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

7 Lane underutilisation specified by user
d Dominant lane on roundabout approach

## SITE LAYOUT

Site: 2037 Total NoBuild NW 319 St and NW 31st Ave Weekday AM
2037 No Build Weekday AM
Roundabout


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Project: H:\projfile\12393 - Cowlitz Reservation Development\Sidra\2014 Analysis\Interchange Roundabouts\102 NW 319th St and NW 31st Avel2037 Analysis - UpdatelNW 319 St and NW 31st Ave_2037 NB.sip6 8001045, KITTELSON AND ASSOCIATES INC, PLUS / Floating

## MOVEMENT SUMMARY

Site: 2037 Total Build NW 319 St and NW 31st Ave Weekday PM 85_15 Split
2037 Build Total Traffic Weekday PM
85/15 Split Sensitivity Analysis
Roundabout


Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement
LOS F will result if v/c>1 irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2037 Total Build NW 319 St and NW 31st Ave Weekday PM 85_15 Split

2037 Build Total Traffic Weekday PM
85/15 Split Sensitivity Analysis
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. $\%$ | Average Delay sec | Level of Service | $\begin{gathered} \text { 95\% Bac } \\ \text { Veh } \end{gathered}$ | $\begin{aligned} & \text { Queue } \\ & \text { Dist } \\ & \mathrm{ft} \end{aligned}$ | Lane Config | Lane Length ft | $\begin{aligned} & \text { Cap. } \\ & \text { Adj. } \\ & \% \end{aligned}$ | Prob. Block. \% |
| South: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 246 | 6.6 | 642 | 0.383 | 100 | 11.0 | LOS B | 2.5 | 66.2 | Full | 1600 | 0.0 | 0.0 |
| Approach | 246 | 6.6 |  | 0.383 |  | 11.0 | LOS B | 2.5 | 66.2 |  |  |  |  |
| East: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 406 | 5.8 | 1329 | 0.305 | 100 | 5.4 | LOS A | 2.2 | 56.6 | Full | 650 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 641 | 1.0 | 1677 | 0.382 | 100 | 5.4 | LOS A | 3.1 | 78.4 | Full | 650 | 0.0 | 0.0 |
| Approach | 1047 | 2.9 |  | 0.382 |  | 5.4 | LOS A | 3.1 | 78.4 |  |  |  |  |
| North: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 535 | 1.2 | 930 | 0.575 | 100 | 11.9 | LOS B | 4.8 | 121.5 | Full | 1400 | 0.0 | 0.0 |
| Approach | 535 | 1.2 |  | 0.575 |  | 11.9 | LOS B | 4.8 | 121.5 |  |  |  |  |
| West: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 175 | 2.9 | 661 | 0.265 | 100 | 8.7 | LOS A | 1.7 | 42.6 | Full | 1300 | 0.0 | 0.0 |
| Approach | 175 | 2.9 |  | 0.265 |  | 8.7 | LOS A | 1.7 | 42.6 |  |  |  |  |
| Intersection | 2003 | 2.9 |  | 0.575 |  | 8.1 | LOS A | 4.8 | 121.5 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

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SIDRA INTERSECTION 6.0.22.4722

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Project: H:\projfile\12393 - Cowlitz Reservation Development\Sidral2014 Analysis\Interchange Roundabouts\102 NW 319th St and NW 31st Ave\2037 Analysis - UpdatelNW 319 St and NW 31st Ave 85_15.sip6 8001045, KITTELSON AND ASSOCIATES INC, PLUS / Floating

## SITE LAYOUT

Site: 2037 Total Build NW La Center and SB Ramps Weekday AM 85_15 Split
2037 Build Weekday AM
Roundabout


## MOVEMENT SUMMARY

Site: 2037 Total Build NW La Center and SB Ramps Weekday PM 85_15 Split
2037 Build Weekday PM
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \hline \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | Flows HV $\%$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 564 | 5.0 | 0.487 | 7.5 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 32.9 |
| 6 | T1 | 902 | 2.0 | 0.487 | 7.3 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 37.5 |
| Appr |  | 1466 | 3.2 | 0.513 | 7.4 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.1 |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 217 | 10.0 | 0.301 | 8.5 | LOS A | 1.2 | 32.8 | 0.65 | 0.66 | 27.2 |
| 4 | T1 | 3 | 50.0 | 0.301 | 8.5 | LOS A | 1.2 | 32.8 | 0.65 | 0.66 | 29.1 |
| 14 | R2 | 145 | 2.0 | 0.228 | 8.5 | LOS A | 0.8 | 21.5 | 0.64 | 0.64 | 29.0 |
| Appr |  | 365 | 7.2 | 0.301 | 8.5 | LOS A | 1.2 | 32.8 | 0.65 | 0.65 | 27.9 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 2 | T1 | 304 | 7.0 | 0.209 | 7.3 | LOS A | 1.3 | 35.0 | 0.75 | 0.67 | 24.4 |
| 12 | R2 | 609 | 1.0 | 0.367 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.6 |
| Approach |  | 913 | 3.0 | 0.367 | 2.4 | LOS A | 1.3 | 35.0 | 0.25 | 0.22 | 31.8 |
| All Vehicles |  | 2744 | 3.6 | 0.513 | 5.9 | LOS A | 1.3 | 35.0 | 0.17 | 0.16 | 32.7 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
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HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2037 Total Build NW La Center and SB Ramps Weekday PM 85_15 Split

## 2037 Build Weekday PM

Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \end{gathered}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Average Delay sec | Level of Service | 95\% Bac Veh | $\begin{aligned} & \text { ueue } \\ & \text { Dist } \\ & \text { ft } \end{aligned}$ | Lane Config | Lane Length ft | Cap. Adj. \% | Prob. Block. \% |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 672 | 4.5 | 1378 | 0.487 | $95^{7}$ | 7.5 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 794 | 2.0 | 1548 | 0.513 | 100 | 7.3 | LOSA | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 1466 | 3.2 |  | 0.513 |  | 7.4 | LOS A | 0.0 | 0.0 |  |  |  |  |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 220 | 10.5 | 731 | 0.301 | 100 | 8.5 | LOS A | 1.2 | 32.8 | Full | 1300 | 0.0 | 0.0 |
| Lane 2 | 145 | 2.0 | 635 | 0.228 | 100 | 8.5 | LOSA | 0.8 | 21.5 | Short | 200 | 0.0 | 0.0 |
| Approach | 365 | 7.2 |  | 0.301 |  | 8.5 | LOS A | 1.2 | 32.8 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 134 | 7.0 | 642 | 0.209 | 100 | 8.1 | LOS A | 1.2 | 32.0 | Full | 650 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 170 | 7.0 | 811 | 0.209 | 100 | 6.7 | LOSA | 1.3 | 35.0 | Full | 650 | 0.0 | 0.0 |
| Lane 3 | 609 | 1.0 | 1658 | 0.367 | 100 | 0.0 | LOSA | 0.0 | 0.0 | Short | 200 | 0.0 | 0.0 |
| Approach | 913 | 3.0 |  | 0.367 |  | 2.4 | LOS A | 1.3 | 35.0 |  |  |  |  |
| Intersection | 2744 | 3.6 |  | 0.513 |  | 5.9 | LOS A | 1.3 | 35.0 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
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7 Lane underutilisation specified by user
d Dominant lane on roundabout approach

## SITE LAYOUT

Site: 2037 Total Build NW La Center and NB Ramps Weekday AM 85_15 Split
2037 Total Traffic Weekday AM
85/15 Split Sensitivity Analysis
Roundabout


## MOVEMENT SUMMARY

## Site: 2037 Total Build NW La Center and NB Ramps Weekday PM 85_15 Split

2037 Total Traffic Weekday PM
85/15 Split Sensitivity Analysis
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { Mov } \\ \text { ID } \end{gathered}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue <br> Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| South: NB Ramp |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 812 | 1.0 | 0.579 | 9.5 | LOS A | 3.5 | 87.5 | 0.55 | 0.56 | 23.7 |
| 8 | T1 | 4 | 50.0 | 0.579 | 10.4 | LOS B | 3.5 | 87.5 | 0.58 | 0.60 | 27.3 |
| 18 | R2 | 648 | 3.0 | 0.489 | 7.7 | LOS A | 2.5 | 62.8 | 0.51 | 0.47 | 29.1 |
| Appro |  | 1464 | 2.0 | 0.579 | 8.7 | LOS A | 3.5 | 87.5 | 0.53 | 0.52 | 25.7 |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 6 | T1 | 654 | 4.0 | 0.830 | 27.3 | LOS C | 9.6 | 247.4 | 0.93 | 1.14 | 15.5 |
| 16 | R2 | 171 | 5.0 | 0.440 | 15.0 | LOS B | 2.3 | 60.6 | 0.76 | 0.80 | 23.4 |
| Appro |  | 825 | 4.2 | 0.830 | 24.7 | LOS C | 9.6 | 247.4 | 0.90 | 1.07 | 16.9 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 177 | 4.0 | 0.165 | 3.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 33.0 |
| 2 | T1 | 345 | 9.0 | 0.165 | 3.4 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 32.8 |
| Appro |  | 522 | 7.3 | 0.165 | 3.5 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 32.8 |
| All Ve |  | 2811 | 3.6 | 0.830 | 12.4 | LOS B | 9.6 | 247.4 | 0.54 | 0.58 | 23.9 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
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Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2037 Total Build NW La Center and NB Ramps Weekday PM 85_15 Split

2037 Total Traffic Weekday PM
85/15 Split Sensitivity Analysis
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Average Delay sec | Level of Service | $\begin{aligned} & \text { 95\% Bac } \\ & \text { Veh } \end{aligned}$ | $\begin{aligned} & \text { Queue } \\ & \text { Dist } \\ & \mathrm{ft} \end{aligned}$ | Lane Config | Lane Length ft | $\begin{aligned} & \text { Cap. } \\ & \text { Adj. } \\ & \% \end{aligned}$ | Prob. Block. \% |
| South: NB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 169 | 1.0 | 913 | 0.185 | $32^{7}$ | 5.8 | LOS A | 0.7 | 16.4 | Short | 200 | 0.0 | 0.0 |
| Lane 2 | 647 | 1.3 | 1118 | 0.579 | 100 | 10.4 | LOS B | 3.5 | 87.5 | Full | 1800 | 0.0 | 0.0 |
| Lane $3^{\text {d }}$ | 648 | 3.0 | 1325 | 0.489 | 100 | 7.7 | LOS A | 2.5 | 62.8 | Short | 250 | 0.0 | 0.0 |
| Approach | 1464 | 2.0 |  | 0.579 |  | 8.7 | LOS A | 3.5 | 87.5 |  |  |  |  |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 607 | 4.0 | 731 | 0.830 | 100 | 28.2 | LOS C | 9.6 | 247.4 | Full | 600 | 0.0 | 0.0 |
| Lane 2 | 218 | 4.8 | 496 | 0.440 | $53^{7}$ | 15.0 | LOS B | 2.3 | 60.6 | Full | 600 | 0.0 | 0.0 |
| Approach | 825 | 4.2 |  | 0.830 |  | 24.7 | LOS C | 9.6 | 247.4 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 245 | 5.4 | 1485 | 0.165 | 100 | 3.7 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 277 | 9.0 | 1685 | 0.165 | 100 | 3.4 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 522 | 7.3 |  | 0.165 |  | 3.5 | LOS A | 0.0 | 0.0 |  |  |  |  |
| Intersection | 2811 | 3.6 |  | 0.830 |  | 12.4 | LOS B | 9.6 | 247.4 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

7 Lane underutilisation specified by user
d Dominant lane on roundabout approach

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Project: H:\projfile\12393 - Cowlitz Reservation Development\Sidra\2014 Analysis\Interchange Roundabouts\104 NW La Center and NB Ramps\2037 Analysis - Update\104 NW La Center and NB Ramps 85_15.sip6 8001045, KITTELSON AND ASSOCIATES INC, PLUS / Floating

## SITE LAYOUT

Site: 2037 Total NoBuild NW 319 St and NW 31st Ave Weekday AM
2037 No Build Weekday AM
Roundabout


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Project: H:\projfile\12393 - Cowlitz Reservation Development\Sidra\2014 Analysis\Interchange Roundabouts\102 NW 319th St and NW 31st Avel2037 Analysis - UpdatelNW 319 St and NW 31st Ave_2037 NB.sip6 8001045, KITTELSON AND ASSOCIATES INC, PLUS / Floating

## MOVEMENT SUMMARY

Site: 2037 Total Build NW 319 St and NW 31st Ave Weekend 85_15 Split
2037 Build Total Traffic Weekend Peak
85/15 Split Sensitivity Analysis
Roundabout


Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement
LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2037 Total Build NW 319 St and NW 31st Ave Weekend 85_15 Split

## 2037 Build Total Traffic Weekend Peak

85/15 Split Sensitivity Analysis
Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Cap. veh/h | Deg. Satn v/c | $\begin{aligned} & \text { Lane } \\ & \text { Util. } \\ & \% \end{aligned}$ | Average Delay sec | Level of Service | $\begin{gathered} 95 \% \mathrm{Bac} \\ \text { Veh } \end{gathered}$ | $\begin{aligned} & \text { Queue } \\ & \text { Dist } \\ & \text { ft } \end{aligned}$ | Lane Config | Lane Length ft | Cap. <br> Adj. \% | Prob. Block. \% |
| South: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane ${ }^{\text {d }}$ | 188 | 4.3 | 632 | 0.297 | 100 | 9.6 | LOS A | 1.9 | 48.9 | Full | 1600 | 0.0 | 0.0 |
| Approach | 188 | 4.3 |  | 0.297 |  | 9.6 | LOS A | 1.9 | 48.9 |  |  |  |  |
| East: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 377 | 3.6 | 1309 | 0.288 | 100 | 5.3 | LOS A | 2.0 | 51.2 | Full | 650 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 838 | 1.0 | 1714 | 0.489 | 100 | 6.5 | LOS A | 4.6 | 116.4 | Full | 650 | 0.0 | 0.0 |
| Approach | 1215 | 1.8 |  | 0.489 |  | 6.2 | LOS A | 4.6 | 116.4 |  |  |  |  |
| North: NW 31st Ave |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 569 | 1.0 | 978 | 0.582 | 100 | 11.6 | LOS B | 4.9 | 122.6 | Full | 1400 | 0.0 | 0.0 |
| Approach | 569 | 1.0 |  | 0.582 |  | 11.6 | LOS B | 4.9 | 122.6 |  |  |  |  |
| West: NW 319 St |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 194 | 3.7 | 648 | 0.299 | 100 | 9.4 | LOS A | 1.9 | 49.2 | Full | 1300 | 0.0 | 0.0 |
| Approach | 194 | 3.7 |  | 0.299 |  | 9.4 | LOS A | 1.9 | 49.2 |  |  |  |  |
| Intersection | 2166 | 2.0 |  | 0.582 |  | 8.2 | LOS A | 4.9 | 122.6 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and v/c ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
d Dominant lane on roundabout approach

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## SITE LAYOUT

Site: 2037 Total Build NW La Center and SB Ramps Weekday AM 85_15 Split
2037 Build Weekday AM
Roundabout


## MOVEMENT SUMMARY

Site: 2037 Total Build NW La Center and SB Ramps Weekend 85_15 Split

## 2037 Build Weekend Peak

Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \mathrm{Mov} \\ & \mathrm{ID} \end{aligned}$ | OD <br> Mov | Dema Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \end{aligned}$ | Deg. Satn v/c | Average Delay sec | Level of Service | 95\% Back Vehicles veh | Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 1 | L2 | 563 | 2.0 | 0.503 | 7.7 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 33.6 |
| 6 | T1 | 1034 | 1.0 | 0.503 | 8.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 37.6 |
| Appr |  | 1597 | 1.4 | 0.571 | 7.9 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.7 |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |
| 7 | L2 | 229 | 4.0 | 0.304 | 8.3 | LOS A | 1.3 | 33.4 | 0.68 | 0.68 | 27.7 |
| 4 | T1 | 3 | 0.0 | 0.304 | 8.3 | LOS A | 1.3 | 33.4 | 0.68 | 0.68 | 29.9 |
| 14 | R2 | 182 | 8.0 | 0.326 | 11.2 | LOS B | 1.3 | 35.7 | 0.70 | 0.72 | 27.1 |
| Appr |  | 414 | 5.7 | 0.326 | 9.5 | LOS A | 1.3 | 35.7 | 0.69 | 0.70 | 27.4 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 2 | T1 | 211 | 3.0 | 0.136 | 6.0 | LOS A | 0.8 | 21.6 | 0.72 | 0.61 | 25.3 |
| 12 | R2 | 697 | 2.0 | 0.425 | 0.0 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 35.6 |
| Approach |  | 908 | 2.2 | 0.425 | 1.4 | LOS A | 0.8 | 21.6 | 0.17 | 0.14 | 33.2 |
| All Vehicles |  | 2919 | 2.2 | 0.571 | 6.1 | LOS A | 1.3 | 35.7 | 0.15 | 0.14 | 33.2 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per movement LOS F will result if $\mathrm{v} / \mathrm{c}>1$ irrespective of movement delay value (does not apply for approaches and intersection). Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010). Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2037 Total Build NW La Center and SB Ramps Weekend 85_15 Split

## 2037 Build Weekend Peak

Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{aligned} & \text { lows } \\ & \text { HV } \\ & \% \\ & \hline \end{aligned}$ | Cap. veh/h | Deg. Satn v/c | $\begin{aligned} & \text { Lane } \\ & \text { Util. } \\ & \% \\ & \hline \end{aligned}$ | Average Delay sec | Level of Service | 95\% Bac Veh | $\begin{array}{r} \text { ueue } \\ \text { Dist } \\ \text { ft } \end{array}$ | Lane Config | Lane Length ft | $\begin{aligned} & \text { Cap. } \\ & \text { Adj. } \\ & \% \end{aligned}$ | Prob. Block. \% |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 704 | 1.8 | 1400 | 0.503 | $88^{7}$ | 7.7 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 893 | 1.0 | 1564 | 0.571 | 100 | 8.2 | LOSA | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 1597 | 1.4 |  | 0.571 |  | 7.9 | LOS A | 0.0 | 0.0 |  |  |  |  |
| North: SB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 232 | 3.9 | 764 | 0.304 | 100 | 8.3 | LOS A | 1.3 | 33.4 | Full | 1300 | 0.0 | 0.0 |
| Lane 2 | 182 | 8.0 | 559 | 0.326 | 100 | 11.2 | LOS B | 1.3 | 35.7 | Short | 200 | 0.0 | 0.0 |
| Approach | 414 | 5.7 |  | 0.326 |  | 9.5 | LOS A | 1.3 | 35.7 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 94 | 3.0 | 690 | 0.136 | 100 | 6.7 | LOS A | 0.8 | 19.8 | Full | 650 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 117 | 3.0 | 866 | 0.136 | 100 | 5.5 | LOS A | 0.8 | 21.6 | Full | 650 | 0.0 | 0.0 |
| Lane 3 | 697 | 2.0 | 1642 | 0.425 | 100 | 0.0 | LOS A | 0.0 | 0.0 | Short | 200 | 0.0 | 0.0 |
| Approach | 908 | 2.2 |  | 0.425 |  | 1.4 | LOS A | 0.8 | 21.6 |  |  |  |  |
| Intersection | 2919 | 2.2 |  | 0.571 |  | 6.1 | LOS A | 1.3 | 35.7 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
LOS F will result if $\mathrm{v} / \mathrm{c}>$ irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D)
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.
7 Lane underutilisation specified by user
d Dominant lane on roundabout approach

## SITE LAYOUT

Site: 2037 Total Build NW La Center and NB Ramps Weekday AM 85_15 Split
2037 Total Traffic Weekday AM
85/15 Split Sensitivity Analysis
Roundabout


## MOVEMENT SUMMARY

## Site: 2037 Total Build NW La Center and NB Ramps Weekend 85_15 Split

2037 Total Traffic Weekend 85/15 Split Sensitivity Analysis
Roundabout

| Movement Performance - Vehicles |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Mov } \\ & \hline \text { ID } \end{aligned}$ | $\begin{aligned} & \text { OD } \\ & \text { Mov } \end{aligned}$ | Dema Total veh/h |  | $\begin{aligned} & \text { Deg. } \\ & \text { Satn } \\ & \text { v/c } \end{aligned}$ | Average Delay sec | Level of Service | 95\% Back <br> Vehicles veh | Queue Distance ft | Prop. Queued | Effective Stop Rate per veh | Average Speed mph |
| South: NB Ramp |  |  |  |  |  |  |  |  |  |  |  |
| 3 | L2 | 968 | 1.0 | 0.574 | 8.3 | LOS A | 3.4 | 84.9 | 0.49 | 0.44 | 22.1 |
| 8 | T1 | 2 | 0.0 | 0.574 | 8.9 | LOS A | 3.4 | 84.9 | 0.51 | 0.46 | 28.0 |
| 18 | R2 | 626 | 3.0 | 0.561 | 10.1 | LOS B | 3.3 | 83.2 | 0.55 | 0.53 | 28.0 |
| Appr |  | 1596 | 1.8 | 0.574 | 9.0 | LOS A | 3.4 | 84.9 | 0.51 | 0.47 | 24.0 |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 6 | T1 | 629 | 3.0 | 0.850 | 30.7 | LOS C | 10.6 | 271.9 | 0.96 | 1.22 | 14.6 |
| 16 | R2 | 173 | 12.0 | 0.493 | 18.7 | LOS B | 2.7 | 74.1 | 0.79 | 0.86 | 21.7 |
| Appr |  | 802 | 4.9 | 0.850 | 28.1 | LOS C | 10.6 | 271.9 | 0.92 | 1.14 | 16.0 |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |
| 5 | L2 | 131 | 1.0 | 0.134 | 3.4 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 33.5 |
| 2 | T1 | 308 | 5.0 | 0.134 | 3.1 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 32.9 |
| Approach |  | 439 | 3.8 | 0.134 | 3.2 | LOS A | 0.0 | 0.0 | 0.00 | 0.00 | 33.1 |
| All Vehicles |  | 2837 | 3.0 | 0.850 | 13.5 | LOS B | 10.6 | 271.9 | 0.55 | 0.59 | 22.5 |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Vehicle movement LOS values are based on average delay and v/c ratio (degree of saturation) per movement
LOS F will result if v/c > 1 irrespective of movement delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all movements (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

## LANE SUMMARY

## Site: 2037 Total Build NW La Center and NB Ramps Weekend 85_15 Split

2037 Total Traffic Weekend 85/15 Split Sensitivity Analysis<br>Roundabout

| Lane Use and Performance |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand Total veh/h | $\begin{gathered} \text { Flows } \\ \text { HV } \\ \% \end{gathered}$ | Cap. veh/h | Deg. Satn v/c | Lane Util. \% | Average Delay sec | Level of Service | 95\% Back <br> Veh | Queue Dist ft | Lane Config | Lane Length ft | Cap. <br> Adj. <br> \% | Prob. Block. \% |
| South: NB Ramp |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 169 | 1.0 | 923 | 0.184 | $32^{7}$ | 5.7 | LOS A | 0.6 | 16.4 | Short | 200 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 801 | 1.0 | 1396 | 0.574 | 100 | 8.9 | LOS A | 3.4 | 84.9 | Full | 1800 | 0.0 | 0.0 |
| Lane 3 | 626 | 3.0 | 1116 | 0.561 | 100 | 10.1 | LOS B | 3.3 | 83.2 | Short | 250 | 0.0 | 0.0 |
| Approach | 1596 | 1.8 |  | 0.574 |  | 9.0 | LOS A | 3.4 | 84.9 |  |  |  |  |
| East: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane $1^{\text {d }}$ | 590 | 3.0 | 694 | 0.850 | 100 | 31.5 | LOS C | 10.6 | 271.9 | Full | 600 | 0.0 | 0.0 |
| Lane 2 | 212 | 10.3 | 430 | 0.493 | $58^{7}$ | 18.7 | LOS B | 2.7 | 74.1 | Full | 600 | 0.0 | 0.0 |
| Approach | 802 | 4.9 |  | 0.850 |  | 28.1 | LOS C | 10.6 | 271.9 |  |  |  |  |
| West: NW La Center Rd |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane 1 | 205 | 2.4 | 1527 | 0.134 | 100 | 3.4 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Lane $2^{\text {d }}$ | 234 | 5.0 | 1749 | 0.134 | 100 | 3.0 | LOS A | 0.0 | 0.0 | Full | 600 | 0.0 | 0.0 |
| Approach | 439 | 3.8 |  | 0.134 |  | 3.2 | LOS A | 0.0 | 0.0 |  |  |  |  |
| Intersection | 2837 | 3.0 |  | 0.850 |  | 13.5 | LOS B | 10.6 | 271.9 |  |  |  |  |

Level of Service (LOS) Method: Delay \& v/c (HCM 2010).
Roundabout LOS Method: Same as Signalised Intersections.
Lane LOS values are based on average delay and $\mathrm{v} / \mathrm{c}$ ratio (degree of saturation) per lane.
LOS F will result if v/c > irrespective of lane delay value (does not apply for approaches and intersection).
Intersection and Approach LOS values are based on average delay for all lanes (v/c not used as specified in HCM 2010).
Roundabout Capacity Model: SIDRA Standard.
HCM Delay Formula option is used. Control Delay does not include Geometric Delay since Exclude Geometric Delay option applies.
Gap-Acceptance Capacity: SIDRA Standard (Akçelik M3D).
HV (\%) values are calculated for All Movement Classes of All Heavy Vehicle Model Designation.

7 Lane underutilisation specified by user
d Dominant lane on roundabout approach

# Appendix CC NW La Center Road/I-5 Interchange IJR Methods \& Assumptions Supplement Collision Analysis 

NW La Center Road/I-5 Interchange IJR Methods \& Assumptions Supplement - Collision Analysis

September 15, 2014
Project \#: 12393

To: $\quad$ Rick Keniston, John Tevis, Barb De Ste. Croix; WSDOT Don Peterson, FHWA

From: Kelly Laustsen; Marc Butorac, PE, PTOE
Copy: Project Team (i.e., CH2MHILL, Olson Engineering, and BergerABAM)

This memorandum documents the methods and assumptions for the Collision Analysis conducted as part of Policy Point 3 for the NW La Center Road/Interstate 5 (I-5) Interchange Justification Report (IJR). It serves to supplement the IJR Methods \& Assumptions document approved in October 2013 and provide more specific information related to the collision analysis.

## BACKGROUND

The Washington Department of Transportation (WSDOT) Design Manual (Reference 1) provides relevant guidance in Section 550.04(3), which details the components of Policy Point 3 for an IJR. As listed in the manual, the following are included:

- Collision Analysis - "Observed collision history": Document the observed collision history, for the most current data years, of the existing limited access freeway and the affected local roadway system. The support team will determine the number of years as well as the scope and detail of this section.
- Collision Analysis - "Proposal(s)": A collision analysis should be performed for the year of opening and design year of the existing limited access freeway and the affected local roadway system for the "no-build," "build," and possibly other scenarios as determined by the support team. The support team will also determine the year of opening and design year as well as the scope and detail of this section.

The intent of the collision analysis is to document the safety effect of the proposed interchange modifications.

## OBSERVED COLLISION HISTORY

The first part of the collision analysis documents the "observed collision history." The methods and assumptions used to document the observed collision history are listed below.

## Methods

- Collision data will be provided by the WSDOT Statewide Travel \& Collision Data Office in excel form, containing basic information about reported crashes. The information received about each crash is listed in Attachment A.
- The collisions will be mapped using the following:
- Primary trafficway (see diagram with roadway identification in Attachment B)
- Milepost
- Vehicle compass direction from/to and impact location (to assess side of roadway)
- Vehicle action (e.g. going wrong way)
- Collisions on the mainline will be associated with the ramp merge/diverge locations based on:
- Milepost
- Vehicle action (if listed as merging or exiting)
- Collision on the ramps will be associated with the ramp terminals based on:
- Junction relationship (if listed as being at an intersection)
- Collision types will be grouped in the following categories (WSDOT classification shown in parenthesis):
- Animal (e.g., domestic animal, vehicle strikes deer, vehicle strikes all other nondomestic animal)
- Fixed object (e.g., bridge rail, cable barrier, concrete barrier/jersey barrier, fence, guardrail, retaining wall, street light pole or base, tree or stump, wood sign post, other object)
- Rear-end (from some direction - rear-end)
- Sideswipe (from same or opposite direction - rear-end)
- Vehicle overturned
- Other
- Collisions will be summarized in tabular form by year, severity, type, and location.
- Where helpful to show observed trends, collisions will be graphed by type, severity, roadway surface condition, weather, lighting conditions, time, and/or date.


## Assumptions

- Five years ( $1 / 1 / 09$ through $12 / 31 / 13$ ) of crash data will be assessed based on the Highway Safety Manual recommendation to use 3 to 5 years of historical crash data for predictive assessments.
- Crashes will be evaluated at the following locations, consistent with the locations for operations assessment:
- I-5 mainline within a half-mile north and south of the NW La Center Road interchange striped ramp gores to capture the influence of the interchange
- I-5 mainline within a half-mile north and south of the truck weigh station south of NW La Center Road
- NW La Center Road/I-5 on- and off-ramp segments
- IJR study intersections:
- NW 31 ${ }^{\text {st }}$ Avenue/NW 319 ${ }^{\text {th }}$ Street;
- I-5 Southbound Ramp/NW La Center Road;
- I-5 Northbound Ramp/NW La Center Road; and
- NW Paradise Park Road/NW La Center Road


## PROPOSAL

Given the improvements proposed for the interchange, including reconfiguration of the ramp terminals and realignment of the frontage roads, the collision analysis will focus on the proposed condition and expected change in crash frequency. The methods and assumptions used to document the proposed condition are listed below.

## Methods

- Information related to the anticipated change in crash frequency with the installation of a roundabout will be provided from the Highway Safety Manual (HSM, Reference 1) and NCHRP Report 672: Roundabouts: An Informational Guide, Second Edition (Reference 3), specifically Exhibit 5-9.
- The research presented in the final report Safety Prediction Methodology and Analysis Tool for Freeways and Interchanges (Project 17-45, Reference 4) will be used to assess the change in expected crash frequency with the proposed roundabout improvements at the ramp terminals.
- This research has been approved by the American Association of State Highway and Transportation Officials (AASHTO) and will be incorporated in the next edition of the HSM.
- This research was used to develop the Enhanced Interchange Safety Analysis Tool (ISATe), which can be used to evaluate freeway and interchange safety. It will be used for the assessment at the ramp terminals.
- Expected crash frequency will be presented at the study intersections for the no-build and build scenarios in 2017 (day of opening) and 2037 (design year), accounting for the installation of roundabout traffic control at the ramp terminals.
- The anticipated safety effect of the frontage road realignment and improved access spacing will be discussed qualitatively given that no crash modification factor (CMF) currently exists for such an improvement (i.e., increased intersection spacing). The ISATe tool does include an input for "distance to the next public street intersection on the outside crossroad leg," which may help account for the effect from the realignment.
- The anticipated safety effect of the freeway ramp reconstruction (e.g., improving to current standards) will be discussed qualitatively. NCHRP 17-45 and the ISATe tool will be used to assess the impact of adding a second lane on the northbound off-ramp. It also provides information on the relationship between ramp speeds and crash frequency.
- The lane configurations, alignment, and traffic volumes developed as part of the operations assessment will be utilized for the safety analysis.


## Assumptions

- Average Annual Daily Traffic is assumed to grow at the same rate as the turning movement counts used in the operations analysis, for purposes of performing the Project 17-45 analysis. This equates to a $2 \%$ annual linear growth on I-5 and the ramps and $3 \%$ annual linear growth on NW 319 ${ }^{\text {th }}$ Street and NW La Center Road.
- The interchange is considered rural for the existing and 2017 analysis and urban for the 2037 analysis.


## NEXT STEPS

Please review the Collision Analysis methods and assumption memorandum and let us know if you have any questions or comments. Any feedback will be used to inform the development of the Collision Analysis as part of Policy Point 3 for the NW La Center Road/I-5 Interchange Improvement Project.

## ATTACHMENTS

A. WSDOT Crash Data Fields
B. Roadway Identification Map

## REFERENCES

1. Washington Department of Transportation, Design Manual, July 2014.
2. American Association of State Highway and Transportation Officials. Highway Safety Manual, $1^{\text {st }}$ Edition. 2010.
3. Rodegerdts, L., et al. NCHRP Report 672: Roundabouts: An Informational Guide, Second Edition. Washington, D.C., Transportation Research Board, National Research Council. 2010.
4. Bonneson, J., et al. Safety Prediction Methodology and Analysis Tool for Freeways and Interchanges. Washington, D.C., Transportation Research Board of the National Academies. Project No. 17-45. May 2012.

## ATTACHMENT A: WSDOT CRASH DATA FIELDS

The crash data from WSDOT is provided in excel form and includes the following data fields:

- State Route Only History Indicator
- JURISDICTION
- CITY
- PRIMARY TRAFFICWAY
- BLOCK NUMBER
- MILE POST
- INTERSECTING TRAFFICWAY
- CO ONLY INTERSECTING COUNTY ROAD MILEPOST
- DIST FROM REF POINT
- MI or FT
- COMP DIR FROM REF POINT
- REFERENCE POINT NAME
- REPORT NUMBER
- DATE
- TIME
- MOST SEVERE INJURY TYPE
- \# INJ
- \#FAT
- \#VEH
- \#PEDS
- \#PEDAL
- JUNCTION RELATIONSHIP
- WEATHER
- ROADWAY SURFACE CONDITIONS
- LIGHTING CONDITIONS
- FIRST COLLISION TYPE / OBJECT STRUCK
- VEHICLE 1 TYPE
- VEH 1 ACTION
- MV DRIVER CONT CIRC 1 (UNIT 1)
- MV DRIVER CONT CIRC 2 (UNIT 1)
- MV DRIVER CONT CIRC 3 (UNIT 1)
- VEH 1 COMP DIR FROM
- VEH 1 COMP DIR TO
- VEHICLE 2 TYPE
- VEH 2 ACTION
- MV DRIVER CONT CIRC 1 (UNIT 2)
- MV DRIVER CONT CIRC 2 (UNIT 2)
- MV DRIVER CONT CIRC 3 (UNIT 2)
- VEH 2 COMP DIR FROM
- VEH 2 COMP DIR TO
- PEDESTRIAN ACTION (UNIT 2)
- PEDESTRIAN CONT CIRC 1 (UNIT 2)
- PEDESTRIAN CONT CIRC 2 (UNIT 2)
- PEDCYCLIST ACTION (UNIT 1)
- PEDCYCLIST CONT CIRC 1 (UNIT 1)
- PEDCYCLIST CONT CIRC 2 (UNIT 1)
- PEDCYCLIST ACTION (UNIT 2)
- PEDCYCLIST CONT CIRC 1 (UNIT 2)
- PEDCYCLIST CONT CIRC 2 (UNIT 2)
- IMPACT LOCATION (City, County \& Misc Trafficways - 2010 forward)


## ATTACHMENT B: ROADWAY IDENTIFICATION DIAGRAM

(see next page)


| Not To Scale |
| :--- |
| 02/13/2013 KLK |

Appendix DD Crash Data (2009-2013)





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## Appendix EE Predictive Crash Assessment Worksheets

Crash Frequency Assessment at Ramp Terminals with Improvements

| Intersection | Observed Crashes(2009-2013) | Observed Crash Rate (/year) | Expected Crash Frequency (/year) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{aligned} & 2017 \text { No } \\ & \text { Build } \end{aligned}$ | $\begin{aligned} & 2017 \text { Build } \\ & \text { (ISATe) } \end{aligned}$ | 2017 Build (w roundabout CMF) | $\begin{aligned} & 2037 \text { No } \\ & \text { Build } \end{aligned}$ | $\begin{array}{\|l} 2017 \text { Build } \\ \text { (ISATe) } \end{array}$ | 2017 Build (w roundabout CMF) |
| NW La Center Rd/ I-5 SB Ramps | 0 | 0 | 0.7 | 0.702 | 0.39 | 0.979 | 1.074 | 0.60 |
| NW La Center Rd/ I-5 NB Ramps | 13 | 2.6 | 3.1 | 2.868 | 1.61 | 5.546 | 5.112 | 2.86 |
| Total | 13 | 2.6 | 3.8 | 3.57 | 2.00 | 6.525 | 6.186 | 3.46 |

Build (ISATe) presents results from ISATe tool, accounting for change in distance to the frontage road intersections Build (w roundabout CMF) applies CMF from NCHRP 972 to assess impact of roundabout control at intersection

Roundabouts expected to reduce crashes by 44\%
CMF 0.56 (NCHRP 972)


| Input Worksheet for Crossroad Ramp Terminals |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Clear | Echo Input Values | Check Input Values |  | Terminal 1 |  | Terminal 2 |  |
|  | Echo Input Values (View results in Column T) |  |  | Crash Period | Study Period | Crash Period | Study Period |
|  |  |  | 2018 |  |  |  |  |
|  |  |  | 2019 |  |  |  |  |
|  |  |  | 2020 |  |  |  |  |
|  |  |  | 2021 |  |  |  |  |
|  |  |  | 2022 |  |  |  |  |
|  |  |  | 2023 |  |  |  |  |
|  |  |  | 2024 |  |  |  |  |
|  |  |  | 2025 |  |  |  |  |
|  |  |  | 2026 |  |  |  |  |
|  |  |  | 2027 |  |  |  |  |
|  |  |  | 2028 |  |  |  |  |
|  |  |  | 2029 |  |  |  |  |
|  |  |  | 2030 |  |  |  |  |
|  |  |  | 2031 |  |  |  |  |
|  |  |  | 2032 |  |  |  |  |
| Outside Crossroad Leg Data |  |  | 2009 |  |  |  |  |
| Average daily traffic (AADT out) by year, veh/d: (enter data only for those years for which it is available, leave other years blank) |  |  | 2010 |  |  |  |  |
|  |  |  | 2011 |  |  |  |  |
|  |  |  | 2012 |  |  |  |  |
|  |  |  | 2013 |  |  |  |  |
|  |  |  | 2014 |  |  |  |  |
|  |  |  | 2015 |  |  |  |  |
|  |  |  | 2016 |  |  |  |  |
|  |  |  | 2017 |  |  |  |  |
|  |  |  | 2018 |  |  |  |  |
|  |  |  | 2019 |  |  |  |  |
|  |  |  | 2020 |  |  |  |  |
|  |  |  | 2021 |  |  |  |  |
|  |  |  | 2022 |  |  |  |  |
|  |  |  | 2023 |  |  |  |  |
|  |  |  | 2024 |  |  |  |  |
|  |  |  | 2025 |  |  |  |  |
|  |  |  | 2026 |  |  |  |  |
|  |  |  | 2027 |  |  |  |  |
|  |  |  | 2028 |  |  |  |  |
|  |  |  | 2029 |  |  |  |  |
|  |  |  | 2030 |  |  |  |  |
|  |  |  | 2031 |  |  |  |  |
|  |  |  | 2032 |  |  |  |  |
| Exit Ramp Data |  |  | 2009 |  |  |  |  |
| Average daily traffic (AADT $T_{\text {ex }}$ ) by year, veh/d: (enter data only for those years for which it is available, leave other years blank) |  |  | 2010 |  |  |  |  |
|  |  |  | 2011 |  |  |  |  |
|  |  |  | 2012 |  |  |  |  |
|  |  |  | 2013 |  |  |  |  |
| For a B4 terminal configuration, enter the AADT for the diagonal exit ramp (not the loop exit ramp). |  |  | 2014 |  |  |  |  |
|  |  |  | 2015 |  |  |  |  |
|  |  |  | 2016 |  |  |  |  |
|  |  |  | 2017 |  |  |  |  |
|  |  |  | 2018 |  |  |  |  |
|  |  |  | 2019 |  |  |  |  |
|  |  |  | 2020 |  |  |  |  |



| Output Worksheet for Crossroad Ramp Terminals |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Signal $=$ signalized intersection modelUnsig $=$ unsignalized intersection model |  | Terminal 1 |  | Terminal 2 |  |
|  | Applicable Models | Crash Period | $\begin{aligned} & \text { Study } \\ & \text { Period } \end{aligned}$ | Crash Period | Study Period |
| Crash Severity Distribution (during Study Period) |  |  |  |  |  |
| Fatal crash frequency ( $\mathrm{N}^{\star}{ }_{\text {e, w, , at, } \mathrm{k}}$ ), crashes: |  |  | 0.002 |  | 0.014 |
| Incapacitating injury crash freq. ( $\mathrm{N}^{*}$ e,w,x,a,t, $)$, crashes: |  |  | 0.011 |  | 0.072 |
| Non-incapacitating inj. crash freq. ( $\mathrm{N}^{*} \mathrm{e,w,x,at,B)} \mathrm{}, \mathrm{crashes:}$ |  |  | 0.037 |  | 0.238 |
| Possible injury crash freq. ( $\mathrm{N}^{*}{ }_{e, w, x, \mathrm{a}, \mathrm{c}, \mathrm{C}}$, crashes: |  |  | 0.129 |  | 0.836 |
| Total fatal-and-injury crash freq. ( $\left.\mathrm{N}^{*}{ }_{\text {e, w, }, \text { atatif }}\right)$, crashes: |  |  | 0.179 |  | 1.160 |
|  |  |  | 0.449 |  | 1.908 |
| Total crash frequency ( $\mathrm{N}^{*}$ e,w,x,at,as) ), crashes: |  |  | 0.628 |  | 3.069 |



| Input Worksheet for Crossroad Ramp Terminals |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Clear | Echo Input Values | Check Input Values |  | Terminal 1 |  | Terminal 2 |  |
|  | (View results in Column T) |  |  | Crash Period | Study Period | Crash Period | Study Period |
|  |  |  | 2018 |  |  |  |  |
|  |  |  | 2019 |  |  |  |  |
|  |  |  | 2020 |  |  |  |  |
|  |  |  | 2021 |  |  |  |  |
|  |  |  | 2022 |  |  |  |  |
|  |  |  | 2023 |  |  |  |  |
|  |  |  | 2024 |  |  |  |  |
|  |  |  | 2025 |  |  |  |  |
|  |  |  | 2026 |  |  |  |  |
|  |  |  | 2027 |  |  |  |  |
|  |  |  | 2028 |  |  |  |  |
|  |  |  | 2029 |  |  |  |  |
|  |  |  | 2030 |  |  |  |  |
|  |  |  | 2031 |  |  |  |  |
|  |  |  | 2032 |  |  |  |  |
| Outside Crossroad Leg Data |  |  | 2009 |  |  |  |  |
| Average daily traffic (AADT out) by year, veh/d: (enter data only for those years for which it is available, leave other years blank) |  |  | 2010 |  |  |  |  |
|  |  |  | 2011 |  |  |  |  |
|  |  |  | 2012 |  |  |  |  |
|  |  |  | 2013 |  |  |  |  |
|  |  |  | 2014 |  |  |  |  |
|  |  |  | 2015 |  |  |  |  |
|  |  |  | 2016 |  |  |  |  |
|  |  |  | 2017 |  |  |  |  |
|  |  |  | 2018 |  |  |  |  |
|  |  |  | 2019 |  |  |  |  |
|  |  |  | 2020 |  |  |  |  |
|  |  |  | 2021 |  |  |  |  |
|  |  |  | 2022 |  |  |  |  |
|  |  |  | 2023 |  |  |  |  |
|  |  |  | 2024 |  |  |  |  |
|  |  |  | 2025 |  |  |  |  |
|  |  |  | 2026 |  |  |  |  |
|  |  |  | 2027 |  |  |  |  |
|  |  |  | 2028 |  |  |  |  |
|  |  |  | 2029 |  |  |  |  |
|  |  |  | 2030 |  |  |  |  |
|  |  |  | 2031 |  |  |  |  |
|  |  |  | 2032 |  |  |  |  |
| Exit Ramp Data |  |  | 2009 |  |  |  |  |
| Average daily traffic (AADT ${ }_{\text {ex }}$ ) by year, veh/d: (enter data only for those years for which it is available, leave other years blank) |  |  | 2010 |  |  |  |  |
|  |  |  | 2011 |  |  |  |  |
|  |  |  | 2012 |  |  |  |  |
|  |  |  | 2013 |  |  |  |  |
| For a B4 terminal configuration, enter the AADT for the diagonal exit ramp (not the loop exit ramp). |  |  | 2014 |  |  |  |  |
|  |  |  | 2015 |  |  |  |  |
|  |  |  | 2016 |  |  |  |  |
|  |  |  | 2017 |  |  |  |  |
|  |  |  | 2018 |  |  |  |  |
|  |  |  | 2019 |  |  |  |  |
|  |  |  | 2020 |  |  |  |  |



| Output Worksheet for Crossroad Ramp Terminals |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Signal = signalized intersection model |  | Terminal 1 |  | Terminal 2 |  |
| Unsig = unsignalized intersection model | Applicable Models | $\begin{aligned} & \text { Crash } \\ & \text { Period } \end{aligned}$ | $\begin{aligned} & \hline \text { Study } \\ & \text { Period } \end{aligned}$ | Crash <br> Period | Study <br> Period |
| Crash Severity Distribution (during Study Period) |  |  |  |  |  |
| Fatal crash frequency ( $\mathrm{N}^{*}$ e,w,x,at,K ), crashes: |  |  | 0.003 |  | 0.011 |
| Incapacitating injury crash freq. ( $\mathrm{N}^{*}$ e, w, , at, $)$, crashes: |  |  | 0.016 |  | 0.060 |
| Non-incapacitating inj. crash freq. ( $\mathrm{N}^{*} \mathrm{e,w,x,a,B}$ ), crashes: |  |  | 0.052 |  | 0.197 |
| Possible injury crash freq. ( $\left.\mathrm{N}^{*}{ }_{\mathrm{e}, \mathrm{w}, \mathrm{x}, \mathrm{t}, \mathrm{C}}\right)$, crashes: |  |  | 0.183 |  | 0.692 |
| Total fatal-and-injury crash freq. ( $\left.\mathrm{N}^{*}{ }_{\text {e, w, }, \text { atatif }}\right)$, crashes: |  |  | 0.254 |  | 0.960 |
| Property-damage-only crash freq. ( $\mathrm{N}_{\text {* }}^{\text {e, w, }, \text { atatodo }}$ ), crashes: |  |  | 0.449 |  | 1.908 |
| Total crash frequency ( $\mathrm{N}^{*}$ e, w, x,ata, $)^{\text {a }}$, crashes: |  |  | 0.702 |  | 2.868 |


| Output Worksheet for Crossroad Ramp Terminals |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Signal = signalized intersection model | Terminal 1 | Terminal 2 |  |  |  |
| Unsig = unsignalized intersection model | Applicable | Crash <br> Models | Study <br> Period | Crash <br> Period | Study <br> Period |
| Period |  |  |  |  |  |


| Input Worksheet for Crossroad Ramp Terminals |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Clear | Echo Input Values <br> (View results in Column T) | Check Input Values |  | Terminal 1 |  | Terminal 2 |  |
|  |  |  |  | Crash <br> Period | Study Period | Crash Period | Study Period |
| Basic Intersection Data |  |  |  |  |  |  |  |
| Ramp terminal configuration: |  |  |  | D4 | D4 | D4 | D4 |
| Ramp terminal description: |  |  |  | SB ramps at La Center |  | NB ramps at La Center |  |
| Ramp terminal traffic control type: |  |  |  | One stop | One stop | One stop | One stop |
| Is a non-ramp public street leg present at the terminal ( $\mathrm{l}_{\mathrm{ps}}$ )?: |  |  |  |  |  |  |  |
| Alignment Data |  |  |  |  |  |  |  |
| Exit ramp skew angle ( $\mathrm{l}_{\text {sk }}$ ), degrees: |  |  |  | 0 | 0 | 0 | 0 |
| Distance to the next public street intersection on the outside crossroad leg ( $L_{\text {str }}$ ), mi: |  |  |  | 0.021 | 0.021 | 0.024 | 0.024 |
| Distance to the adjacent ramp terminal ( $\mathrm{L}_{\text {rmp }}$ ), mi: |  |  |  | 0.104 | 0.104 | 0.104 | 0.104 |
| Traffic Control |  |  |  |  |  |  |  |
| Left-Turn Operational Mode |  |  |  |  |  |  |  |
| Crossroad | Inside approach | Protected-only mode ( $\mathrm{I}_{\mathrm{p}, \mathrm{l}, \mathrm{in}}$ )?: |  |  |  |  |  |
|  | Outside approach | Protected-only mode ( $\mathrm{l}_{\mathrm{p}, \mathrm{l}, \text { out }}$ )?: |  |  |  |  |  |
| Right-Turn Control Type |  |  |  |  |  |  |  |
| Ramp | Exit ramp approach | \|Right-turn control type: |  | Stop | Stop | Stop | Stop |
| Cross Section Data |  |  |  |  |  |  |  |
| Crossroad median width ( $\mathrm{W}_{\mathrm{m}}$ ), ft: |  |  |  | 0 | 0 | 0 | 0 |
| Number of Lanes |  |  |  |  |  |  |  |
| Crossroad | Both approaches | Lanes serving through vehicles ( $\mathrm{n}_{\text {th }}$ ): |  | 2 | 2 | 2 | 2 |
|  | Inside approach | Lanes serving through vehicles ( $\mathrm{n}_{\text {th, } \mathrm{n}}$ ): |  |  |  |  |  |
|  | Outside approach | Lanes serving through vehicles ( $\mathrm{n}_{\text {th,out }}$ ): |  |  |  |  |  |
| Ramp | Exit ramp approach | All lanes ( $\mathrm{n}_{\text {ex }}$ ): |  | 1 | 1 | 1 | 1 |
| Right-Turn Channelization see note: |  |  |  |  |  |  |  |
| Crossroad | Inside approach | Channelization present ( $\mathrm{l}_{\mathrm{ch,in}}$ )?: |  |  |  |  |  |
|  | Outside approach | Channelization present ( $\mathrm{I}_{\text {ch,out }}$ )?: |  |  |  |  |  |
| Ramp | Exit ramp approach | Channelization present | $\left(\mathrm{l}_{\mathrm{ch}, \mathrm{ex}}\right)$ ?: |  |  |  |  |
| Left-Turn Lane or Bay |  |  |  |  |  |  |  |
| Crossroad | Inside approach | Lane or bay present ( $\mathrm{l}_{\text {bay,lt,in }}$ )?: |  | No | No | No | No |
|  |  | Width of lane or bay ( $\mathrm{W}_{\mathrm{b}, \mathrm{in}}$ ), ft: |  |  |  |  |  |
|  | Outside approach | Lane or bay present ( $\mathrm{l}_{\text {bay, } \mathrm{lt} \text {,out) }}$ )?: |  |  |  |  |  |
|  |  | Width of lane or bay ( $\mathrm{W}_{\mathrm{b}, \mathrm{out}}$ ), ft: |  |  |  |  |  |
| Right-Turn Lane or Bay |  |  |  |  |  |  |  |
| Crossroad | Inside approach | Lane or bay present ( $\mathrm{l}_{\text {bay,rt,in }}$ )?: |  |  |  |  |  |
|  | Outside approach | Lane or bay present (l | y,rt,out)?: | No | No | No | No |
| Access Data |  |  |  |  |  |  |  |
| Number of driveways on the outside crossroad leg ( $\mathrm{n}_{\mathrm{dw}}$ ): |  |  |  |  |  |  |  |
| Number of public street approaches on the outside crossroad leg ( $\mathrm{n}_{\mathrm{ps}}$ ): |  |  |  | 2 | 2 | 2 | 2 |
| Traffic Data |  |  | Year |  |  |  |  |
| Inside Crossroad Leg Data |  |  | 2009 |  |  |  |  |
| Average daily traffic (AADT ${ }_{\text {in }}$ ) by year (enter data only for those years for it is available, leave other years bla |  | eh/d: ch | 2010 |  |  |  |  |
|  |  | 2011 |  |  |  |  |
|  |  | 2012 |  |  |  |  |
|  |  | 2013 |  |  |  |  |
|  |  | 2014 |  |  |  |  |
|  |  | 2015 |  |  |  |  |
|  |  | 2016 |  |  |  |  |
|  |  | 2017 |  |  |  |  |


| Output Worksheet for Crossroad Ramp Terminals |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Signal $=$ signalized intersection modelUnsig = unsignalized intersection model |  | Terminal 1 |  | Terminal 2 |  |
|  | Applicable Models | Crash Period | Study Period | Crash Period | Study Period |
| Crash Severity Distribution |  |  |  |  |  |
| Fatal crash frequency ( $\mathrm{N}^{*}$ e,w,w,at,k ), crashes: |  |  | 0.001 |  | 0.013 |
| Incapacitating injury crash freq. ( $\mathrm{N}^{*}$ e,w,x,a,t, $)$, crashes: |  |  | 0.007 |  | 0.066 |
| Non-incapacitating inj. crash freq. ( $\mathrm{N}^{*}$ e,w,x,a,t, ), crashes: |  |  | 0.043 |  | 0.427 |
| Possible injury crash freq. ( $\mathrm{N}^{*}{ }_{e, w, x, \mathrm{a}, \mathrm{c}, \mathrm{C}}$, crashes: |  |  | 0.187 |  | 1.870 |
| Total fatal-and-injury crash freq. ( $\mathrm{N}_{\text {e, }{ }_{\text {e, }, \text {, a, } \text {, } \mathrm{f} \text { ) }} \text {, crashes: }}$ |  |  | 0.238 |  | 2.375 |
|  |  |  | 0.741 |  | 3.171 |
| Total crash frequency ( $\mathrm{N}^{*}$ e,w,x,at,as$)$, crashes: |  |  | 0.979 |  | 5.546 |





| Output Worksheet for Crossroad Ramp Terminals |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Signal = signalized intersection model |  | Terminal 1 |  | Terminal 2 |  |
| Unsig = unsignalized intersection model | Applicable Models | Crash <br> Period | Study Period | Crash Period | Study <br> Period |
| Crash Severity Distribution (during Study Period) |  |  |  |  |  |
| Fatal crash frequency ( $\mathrm{N}^{*}{ }_{e, w, w, a t, \mathrm{~K}}$ ), crashes: |  |  | 0.002 |  | 0.010 |
| Incapacitating injury crash freq. ( $\mathrm{N}^{*}$ e,w,w,a,t,A$)$, crashes: |  |  | 0.009 |  | 0.054 |
| Non-incapacitating inj. crash freq. ( $\mathrm{N}_{\text {e, w, } \mathrm{\chi}, \mathrm{at,}, \mathrm{~B}}$ ), crashes: |  |  | 0.060 |  | 0.349 |
| Possible injury crash freq. ( $\mathrm{N}^{*}{ }_{e, w, x, \mathrm{at,c}, \mathrm{C}}$, crashes: |  |  | 0.262 |  | 1.528 |
| Total fatal-and-injury crash freq. ( $\mathrm{N}^{*}$ e,w,x,a,t,fi) ), crashes: |  |  | 0.333 |  | 1.941 |
| Property-damage-only crash freq. ( $\mathrm{N}^{*}$ e,w,x,at,pdo), , crashes: |  |  | 0.741 |  | 3.171 |
| Total crash frequency ( $\mathrm{N}^{*}{ }_{e, w, \chi, \mathrm{atas}}$ ), crashes: |  |  | 1.074 |  | 5.112 |


| Output Worksheet for Crossroad Ramp Terminals |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| Signal = signalized intersection model | Terminal 1 | Terminal 2 |  |  |  |
| Unsig $=$ unsignalized intersection model | Applicable <br> Models | Crash <br> Period | Study <br> Period | Crash <br> Period | Study <br> Period |

## Appendix FF Truck Speed Study

Date:
Start Time
End Time $\quad 1: 55$ PM
Surveyor: JR, Sara, Brian and Bill

Heavy Vehicle Spot Speed Survey

| Item | Time | Truck Description | Truck Class | Merge Point | 1000 Feet | 2000 Feet | 3000 Feet |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 10:45:22 | Blue Bud Light-T | 10 | 42 | 40 | 53 | 51 |
| 2 | 10:46:39 | Grey Blue-T | 10 | 37 | 42 | 53 | 57 |
| 3 | 10:47:43 | White Garbage | 9 | 48 | 39 | 64 | 61 |
| 4 | 10:48:55 | White White-T | 8 | 47 | 48 | 67 | 57 |
| 5 | 10:50:00 | Red Green-T | 10 | 38 | 52 | 51 | 54 |
| 6 | 10:51:42 | Wideload | 10 | 37 | 42 | 51 | 57 |
| 7 | 10:52:46 | Wideload | 10 | 42 | 53 | 55 | 57 |
| 8 | 10:53:41 | Red White-T | 10 | 43 | 47 | 58 | 61 |
| 9 | 10:56:17 | White White-T | 9 | 45 | 57 | 60 | 61 |
| 10 | 10:57:27 | White Red-T | 9 | 39 | 52 | 57 | 61 |
| 11 | 10:58:28 | Small White Truck | 9 | 41 | 56 | 57 | 54 |
| 12 | 11:00:06 | Red w/combine | 5 | 35 | 55 | 54 | 54 |
| 13 | 11:01:04 | Baby Blue W-T | 10 | 34 | 41 | 49 | 54 |
| 14 | 11:02:10 | White w/Red Stripe | 9 | 45 | 44 | 58 | 61 |
| 15 | 11:03:51 | Gas Truck | 9 | 45 | 58 | 58 | 61 |
| 16 | 11:04:39 | Car Carrier | 10 | 41 | 53 | 55 | 57 |
| 17 | 11:05:57 | White W/C | 9 | 44 | 45 | 60 | 57 |
| 18 | 11:07:20 | White Tubing-T | 10 | 38 | 39 | 49 | 51 |
| 19 | 11:08:14 | Red GT on T | 12 | 44 | 44 | 61 | 57 |
| 20 | 11:09:21 | White w/wood | 10 | 33 | 30 | 41 | 48 |
| 21 | 11:10:07 | Black Black-T | 13 | 32 | 49 | 61 | 57 |
| 22 | 11:11:30 | Gas Truck | 9 | 45 | 45 | 61 | 57 |
| 23 | 11:12:31 | Small Red Truck | 13 | 49 | 37 | 60 | 57 |
| 24 | 11:13:43 | Red White-T | 5 | 48 | 40 | 62 | 54 |
| 25 | 11:14:50 | Lime Green | 9 | 27 | 40 | 59 | 61 |
| 26 | 11:15:44 | White w/Yellow Sign on-T | 10 | 40 | 40 | 57 | 61 |
| 27 | 11:17:01 | White Log T | 9 | 33 | 35 | 47 | 46 |
| 28 | 11:18:46 | Red White-T | 9 | 32 | 43 | 55 | 61 |
| 29 | 11:19:47 | Purple Red | 10 | 38 | 53 | 59 | 57 |
| 30 | 11:20:45 | White Gas DBL-T | 13 | 36 | 38 | 47 | 51 |
| 31 | 11:22:08 | Gray Metal-T | 9 | 45 | 44 | 53 | 51 |
| 32 | 11:23:25 | Fedex | 6 | 49 | 46 | 59 | 57 |
| 33 | 11:24:48 | Red Metal Coils | 10 | 33 | 35 | 49 | 51 |
| 34 | 11:25:54 | White w/white skirt | 9 | 36 | 42 | 54 | 61 |
| 35 | 11:27:00 | White Red H | 9 | 44 | 46 | 57 | 61 |
| 36 | 11:28:07 | Green White Canopy | 13 | 38 | 40 | 52 | 54 |
| 37 | 11:28:58 | Purple w/Canopy | 9 | 44 | 53 | 53 | 57 |
| 38 | 11:29:53 | Light Brown White-T | 10 | 32 | 54 | 50 | 54 |
| 39 | 11:32:45 | Red White-T | 9 | 42 | 42 | 56 | 54 |
| 40 | 11:34:37 | Black Chemical Tanks | 13 | 37 | 29 | 48 | 48 |
| 41 | 11:36:39 | Small Ladder Truck | 6 | 48 | 47 | 51 | 57 |
| 42 | 11:38:30 | Small White Truck | 5 | 33 | 55 | 52 | 70 |
| 43 | 11:44:11 | Gray White-T | 10 | 32 | 44 | 50 | 54 |
| 44 | 11:44:55 | Small Red Truck | 5 | 55 | 43 | 62 | 61 |
| 45 | 11:45:50 | White GT | 9 | 40 | 42 | 54 | 54 |
| 46 | 11:47:08 | Light Blue White-T | 9 | 39 | 54 | 50 | 54 |
| 47 | 11:48:01 | Blue Empty T | 9 | 41 | 43 | 53 | 51 |

## Quality Counts <br> TRANSPORTATION DATA COLLECTION SERVICES

Date:
Start Time
End Time
Surveyor: JR, Sara, Brian and Bill

Heavy Vehicle Spot Speed Survey

|  |  |  | Average Speeds | 41 | 44 | 55 | 56 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Item | Time | Truck Description | Truck Class | Merge Point | 1000 Feet | 2000 Feet | 3000 Feet |
| 48 | 11:49:18 | Yellow Penske | 5 | 43 | 44 | 58 | 54 |
| 49 | 11:50:10 | Pickup Truck Equipment | 8 | 34 | 43 | 54 | 57 |
| 50 | 11:51:14 | Purple | 10 | 34 | 42 | 49 | 51 |
| 51 | 11:52:05 | White White-T | 9 | 41 | 35 | 56 | 54 |
| 52 | 11:53:05 | White White-T | 9 | 38 | 37 | 53 | 54 |
| 53 | 11:54:06 | Baby Blue | 13 | 37 | 59 | 53 | 51 |
| 54 | 11:55:09 | Black Red-T | 9 | 41 | 48 | 54 | 57 |
| 55 | 11:56:18 | White White-T | 9 | 40 | 48 | 53 | 57 |
| 56 | 11:57:32 | White \& Blue | 9 | 42 | 46 | 55 | 57 |
| 57 | 11:58:28 | Red White-T | 9 | 47 | 59 | 56 | 57 |
| 58 | 11:59:35 | Dark Gray White-T | 10 | 36 | 58 | 49 | 51 |
| 59 | 12:00:50 | Blue Wide Load | 10 | 36 | 42 | 49 | 51 |
| 60 | 12:01:37 | Blue Black-T | 9 | 40 | 50 | 55 | 54 |
| 61 | 12:02:24 | Rite Aid | 13 | 40 | 52 | 53 | 57 |
| 62 | 12:03:38 | Carson Oil | 6 | 43 | 45 | 55 | 51 |
| 63 | 12:05:08 | White White-T | 8 | 35 | 50 | 53 | 51 |
| 64 | 12:05:35 | White McKinney | 9 | 43 | 51 | 55 | 54 |
| 65 | 12:07:02 | Green Construction | 13 | 38 | 43 | 51 | 54 |
| 66 | 12:07:55 | White no T | 6 | 44 | 50 | 59 | 65 |
| 67 | 12:08:43 | White Tank-T | 9 | 42 | 40 | 57 | 61 |
| 68 | 12:09:39 | Gray | 9 | 44 | 45 | 57 | 61 |
| 69 | 12:10:51 | Gray Orange-T | 10 | 34 | 47 | 50 | 51 |
| 70 | 12:11:59 | Orange Orange-T | 9 | 36 | 48 | 55 | 57 |
| 71 | 12:13:13 | Red Logger | 9 | 36 | 47 | 52 | 51 |
| 72 | 12:14:14 | White Green | 10 | 35 | 36 | 52 | 54 |
| 73 | 12:15:21 | Thermo King White | 5 | 49 | 45 | 48 | 54 |
| 74 | 12:16:15 | White Rite Aid | 13 | 38 | 36 | 52 | 54 |
| 76 | 12:18:37 | Tan Oil | 8 | 42 | 37 | 53 | 57 |
| 77 | 12:19:31 | White Oil | 8 | 38 | 30 | 52 | 57 |
| 78 | 12:20:39 | Orange Logger | 10 | 40 | 45 | 53 | 61 |
| 79 | 12:21:42 | White Black-T | 10 | 42 | 42 | 51 | 57 |
| 80 | 12:22:44 | White Train Wheels | 9 | 30 | 29 | 55 | 57 |
| 82 | 12:25:16 | Purple White-T | 9 | 48 | 49 | 58 | 54 |
| 83 | 12:26:13 | Red White-T | 9 | 42 | 36 | 51 | 48 |
| 84 | 12:26:57 | Red Empty-T | 9 | 40 | 45 | 57 | 61 |
| 85 | 12:28:13 | White Tow Truck | 5 | 49 | 40 | 55 | 57 |
| 86 | 12:29:09 | White Gray-T | 10 | 36 | 44 | 53 | 48 |
| 88 | 12:31:15 | Red White-T | 9 | 33 | 39 | 60 | 61 |
| 89 | 12:32:26 | Rite Aid | 13 | 34 | 40 | 60 | 61 |
| 90 | 12:33:06 | Red White | 9 | 44 | 47 | 58 | 61 |
| 91 | 12:34:01 | Black White-T | 9 | 47 | 41 | 59 | 57 |
| 92 | 12:34:57 | Yellow Penske | 5 | 50 | 54 | 62 | 70 |
| 93 | 12:36:14 | Gray Red | 9 | 50 | 49 | 63 | 65 |
| 94 | 12:37:08 | Red White Stripe | 9 | 45 | 45 | 58 | 57 |
| 95 | 12:38:01 | White White-T | 9 | 34 | 32 | 56 | 61 |
| 96 | 12:38:48 | Red Dump 2xT | 10 | 46 | 47 | 58 | 48 |
| 97 | 12:42:45 | Black Septic-T | 6 | 31 | 60 | 61 | 57 |

## Quality Counts <br> TRANSPORTATION DATA COLLECTION SERVICES <br> Date: <br> Start Time: <br> End Time 1:55 PM <br> Surveyor: JR, Sara, Brian and Bill

Heavy Vehicle Spot Speed Survey

|  |  |  | Average Speeds | 41 | 44 | 55 | 56 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Item | Time | Truck Description | Truck Class | Merge Point | 1000 Feet | 2000 Feet | 3000 Feet |
| 98 | 12:43:36 | White White-T | 9 | 39 | 46 | 48 | 54 |
| 99 | 12:44:29 | Red Red-T | 9 | 41 | 40 | 55 | 54 |
| 100 | 12:45:20 | Yellow Colored-T | 9 | 41 | 32 | 55 | 54 |
| 101 | 12:47:47 | Yellow White-T | 8 | 39 | 35 | 53 | 61 |
| 102 | 12:49:22 | Blue Logger | 10 | 43 | 32 | 55 | 51 |
| 104 | 12:51:48 | Green White-T | 10 | 48 | 48 | 54 | 54 |
| 105 | 12:52:44 | Red White-T | 9 | 39 | 50 | 55 | 57 |
| 106 | 12:53:39 | White White-T | 10 | 44 | 44 | 56 | 57 |
| 107 | 12:56:20 | Black White-T | 9 | 30 | 28 | 51 | 54 |
| 108 | 12:57:48 | Black Orange | 10 | 34 | 27 | 49 | 54 |
| 109 | 12:59:06 | Blue White | 9 | 42 | 41 | 50 | 57 |
| 110 | 1:00:54 | White White-T | 9 | 43 | 36 | 59 | 57 |
| 111 | 1:02:17 | White Swift | 9 | 40 | 41 | 48 | 54 |
| 112 | 1:03:15 | Gray Construction | 13 | 38 | 31 | 50 | 54 |
| 113 | 1:04:32 | White White-T | 9 | 37 | 37 | 54 | 54 |
| 114 | 1:05:55 | Small Uhaul | 5 | 51 | 52 | 59 | 61 |
| 115 | 1:06:57 | Red Logger | 6 | 40 | 38 | 61 | 61 |
| 116 | 1:08:03 | White empty-T | 9 | 42 | 40 | 60 | 57 |
| 117 | 1:09:27 | Green McKinney | 9 | 43 | 45 | 59 | 54 |
| 118 | 1:10:35 | Black Logger | 9 | 37 | 36 | 56 | 57 |
| 119 | 1:11:20 | Small Red | 5 | 56 | 42 | 64 | 61 |
| 120 | 1:12:35 | Small White Mayflower | 5 | 48 | 52 | 58 | 57 |
| 121 | 1:14:21 | White GT White-T | 10 | 53 | 48 | 60 | 54 |
| 122 | 1:15:50 | White White-T | 9 | 37 | 40 | 53 | 57 |
| 123 | 1:16:53 | Red Logger | 10 | 36 | 31 | 50 | 61 |
| 124 | 1:18:29 | Red Logger empty | 9 | 47 | 53 | 59 | 61 |
| 125 | 1:20:54 | Blue White-T | 10 | 40 | 46 | 50 | 51 |
| 126 | 1:21:51 | ABF Truck | 9 | 44 | 50 | 55 | 57 |
| 127 | 1:22:58 | White White-T | 9 | 42 | 36 | 58 | 57 |
| 128 | 1:23:46 | White Sound Beverage | 10 | 35 | 44 | 49 | 57 |
| 130 | 1:26:28 | Tan Oil | 9 | 40 | 45 | 52 | 61 |
| 131 | 1:28:02 | Tan White-T | 9 | 38 | 41 | 53 | 65 |
| 132 | 1:29:05 | Gray Gray-T | 9 | 29 | 49 | 52 | 61 |
| 133 | 1:29:55 | Red Green-T | 10 | 35 | 51 | 50 | 54 |
| 134 | 1:30:52 | Purple Blue White-T | 9 | 43 | 38 | 55 | 54 |
| 135 | 1:32:29 | White White-T | 9 | 39 | 51 | 56 | 57 |
| 136 | 1:33:23 | White no-T | 6 | 43 | 46 | 52 | 65 |
| 137 | 1:34:14 | Blue no-T | 6 | 46 | 52 | 50 | 54 |
| 138 | 1:36:45 | Blue White-T | 9 | 46 | 43 | 56 | 61 |
| 139 | 1:37:40 | Red White-T | 9 | 46 | 41 | 59 | 61 |
| 140 | 1:38:43 | Small White Truck | 5 | 49 | 51 | 58 | 41 |
| 141 | 1:39:36 | White | 9 | 42 | 53 | 63 | 65 |
| 142 | 1:41:05 | Tan Scrap Metal | 10 | 38 | 42 | 51 | 51 |
| 143 | 1:41:54 | Car Carrier Large | 9 | 38 | 45 | 55 | 57 |
| 144 | 1:42:58 | Red White-T | 9 | 45 | 49 | 60 | 65 |
| 145 | 1:43:53 | Red White-T | 9 | 40 | 53 | 56 | 61 |
| 146 | 1:44:55 | White White-T | 9 | 42 | 51 | 59 | 61 |

Quality Counts
TRANSPORTATION DATA
COLLECTION SERVICES

| Date: | 10/21/2014 |
| :---: | ---: |
| Start Time: | 10:45 AM |
| End Time | 1:55 PM |
| Surveyor: JR, Sara, Brian and Bill |  |

Heavy Vehicle Spot Speed Survey

|  |  | Average Speeds | $\mathbf{4 1}$ | $\mathbf{4 4}$ | $\mathbf{5 4}$ | $\mathbf{5 6}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Item | Time | Truck Description | Truck Class | Merge Point | 1000 Feet | 2000 Feet | 3000 Feet |
| 147 | $1: 45: 39$ | Gray w/metal load | 10 | 45 | 52 | 68 | 5 |
| 148 | $1: 46: 39$ | GMC Black | 5 | 37 | 44 | 58 |  |
| 150 | $1: 48: 37$ | Whtie Car Carrier | 9 | 35 | 42 | 57 |  |
| 151 | $1: 49: 22$ | Red White-T | 9 | 44 | 48 | 59 | 57 |
| 152 | $1: 51: 25$ | Green Gray-T | 10 | 38 | 46 | 57 |  |
| 153 | $1: 52: 24$ | Blue Empty | 10 | 52 | 51 | 59 | 51 |
| 154 | $1: 53: 54$ | White Blue-T | 10 | 35 | 51 | 62 | 46 |
| 155 | $1: 54: 53$ | White Canvas | 10 | 35 | 44 | 48 | 54 |

All classes
Average
Minimum
Maximum
Median

149

| 44 | 55 | 56 |
| :--- | :--- | :--- |
| 27 | 41 | 41 |
| 60 | 68 | 70 |
| 44 | 55 | 57 |

## Appendix GG Design Criteria

## NW La Center Road/l-5 Interchange Improvement Project Design Criteria Interstate Interchange Areas

Matrix 2
Row 11

This checklist is to confirm interpretation of design criteria. Your project may require that additional/different/or fewer Design Elements be addressed.

| Design Class | Class I-1 (Exh. 1140-5) |
| :--- | :--- |
| Functional Class | INTERSTATE (I-5) |
| Design Year | 2016 |
| Design Speed | Ramp Range: 70 mph - 25mph (Exh. 1360-4, based on I-5 design speed of 80mph) <br> Cross Road: 45 mph |
| ADT |  |
| Truck Percentage |  |
| Right of Way Width |  |


| $\begin{gathered} \text { DESIGN } \\ \text { ELEMENT } \end{gathered}$ | Design Level (B/M/F | Criteria | REFERENCE \& COMMENTS |
| :---: | :---: | :---: | :---: |
| Ramps \& Collector Distributors |  |  |  |
| Horizontal Alignment | F | - |  |
| Stopping Sight Distance |  | 730ft | Exh. 1260-1 |
| Max. Superelevation |  | 10\% | 1250.04 (Exh. 1250-4a) |
|  |  |  |  |
|  |  |  |  |
| Vertical Alignment | F | - |  |
| Maximum Grade |  | 5\%/3\% | Exh. 1360-5 (5\% max., 3\% desirable) |
| Stopping Sight Distance |  | $\begin{aligned} & \hline 730 \mathrm{ft} / \\ & 155 \mathrm{ft} \\ & \hline \end{aligned}$ | Exh. 1260-1 (Vd=70mph/Vd=25mph) |
| Passing Sight Distance |  | N/A |  |
| Decision Sight Distance |  | N/A |  |
|  |  |  |  |
|  |  |  |  |
| Lane Width | F |  |  |
| Number of Lanes |  | 1/2/3 | Exh. 1360-6: NB - 2 at gore, 3 at intersection; SB - 1 at gore, 2 at intersection |
| Lane Width |  | $\begin{aligned} & \hline 15 \mathrm{ft} / 25 \mathrm{ft} \\ & \hline 12 \mathrm{ft} \\ & \hline \end{aligned}$ | Exh. 1360-6: single-lane ramp/two-lane ramp/aux lane |
| Turning Roadway Width |  | 25 ft | Exh. 1240-2a ( $\mathrm{R}=1,000$ ' to 2,999') |
|  |  |  |  |


| $\begin{gathered} \text { DESIGN } \\ \text { ELEMENT } \end{gathered}$ | Design Level (B/M/F) | Criteria | REFERENCE \& COMMENTS |
| :---: | :---: | :---: | :---: |
| Shoulder Width | F |  |  |
| Shoulder Width-Left |  | $2 \mathrm{ft} / 4 \mathrm{ft}$ | Exh. 1360-6: single-lane/ two-lane (plus 2' shy at barriers) |
| Shoulder Width-Right |  | 8ft/10ft | Exh. 1360-6: ramp/Exh. 1360-13c aux lane (plus 2' shy at barriers) |
|  |  |  |  |
| Lane Transition |  |  |  |
| Channelization Tapers | F |  |  |
|  |  | 70/1 | Exh. 1210-1 Min. angle w/out curve $=0^{\circ} 49^{\prime}$ at 70 mph |
| On/Off Connections | F |  |  |
| On Connection |  | Singlelane, tapered | Exh. 1360-13a |
| Off Connection |  | Twolane, tapered | Exh. 1360-14d |
| Cross Slope Lane | F |  |  |
|  |  | 2\% | Section 1230.04 |
| Cross Slope Shoulder | F |  |  |
|  |  | 2\% | Section 1230.04. |
| Fill/Ditch Slopes | F |  |  |
| Fill Slopes |  | 6H:1V | Exh. 1230-4a or 4b-6H:1V max (0'-10' height of fill, depth of ditch), 4H:1H max (10'-20') |
| Ditch In-slopes |  | 6H:1V | Exh. 1230-4a or $4 \mathrm{~b}-6 \mathrm{H}: 1 \mathrm{~V} \max \left(0^{\prime}-10^{\prime}\right.$ height of fill, depth of ditch), 4H:1H max (10'-20') |
|  |  |  | - ${ }^{\text {a }}$ |
| Limited Access | F |  |  |
|  |  |  | - |
| Clear Zone | F |  |  |
|  |  | Varies | Exh. 1600-2 |
| Signing | F |  |  |
|  |  | * | Provide Permanent signing in accordance with WSDOT Standard Plans, Section M - Roadway Delineation and WSDOT Design Manual Chapter 1020 |
| Delineation | F |  |  |
|  |  | * | Provide Permanent signing in accordance with WSDOT Standard Plans, Section M - Roadway Delineation nd WSDOT Design Manual Chapter 1030 |
| Illumination | F |  |  |
|  |  | $\begin{array}{\|l\|} \hline \text { Varies } \\ 0.6 \text { to } \\ 0.9 \\ \hline \end{array}$ | (footcandles) Exh. 1040-25 Section 1040.05 |
| ITS | F |  |  |
|  |  |  |  |


| $\begin{aligned} & \text { DESIGN } \\ & \text { ELEMENT } \end{aligned}$ | Design Level (B/M/F) | Criteria | REFERENCE \& COMMENTS |
| :---: | :---: | :---: | :---: |
| Basic Safety |  |  |  |
|  |  | N/A | Exh. 1100-3 (does not apply for FULL design) |
| Vertical Clearance | F |  |  |
| Bridge \# |  | 16.5 ft | Exh. 720-1 |
| Bike and Pedestrian |  |  |  |
|  | F |  |  |
|  |  |  | - |
|  |  |  |  |
|  |  |  |  |
| Ramp Terminals | F |  |  |
| Design Vehicle |  | WB-67 | Exh. 1310-12-WB-67 is desirable |
|  |  |  |  |
| Turn Radii | F |  |  |
| Intersection Radii - Left |  | 70 ft | Exh. 1310-14 (Assume $\mathrm{A}=90^{\circ}$ ) |
| Intersection Radii - Right |  | 70ft | Exh. 1310-14 (Assume $\mathrm{A}=90^{\circ}$ ) |
|  |  |  |  |
|  |  |  | - - |
| Intersection Angle | F |  | - |
|  |  | $\begin{aligned} & 60^{\circ}- \\ & 120^{\circ} \\ & \hline \end{aligned}$ | 1310.03(9) |
| Intersection Sight Distance | F |  |  |
|  |  |  | 1310.06 - Signalized intersections - provide sight distance for right-turning vehicles |
|  |  |  | - |
| Barriers |  |  | - |
| Terminals \& Transition Section | F |  |  |
|  |  |  |  |
| Standard Run | F |  |  |
|  |  |  |  |
| Bridge Rail | F |  |  |
|  |  |  |  |
|  |  |  |  |
| Cross Roads |  |  |  |
| Lane Width | F |  |  |
| Number of Lanes |  | 4 | (6 future) |
| Lane Width |  | 12ft | Exh. 1140-8 |
| Turning Roadway Width |  | 27 ft | (for R = 1,000ft) Exh. 1240-1a. AASHTO Exh. 3-15 (page 147) to get min. Radius |
|  |  |  |  |


| DESIGN <br> ELEMENT | Design <br> Level <br> (B/M/F) | Criteria | REFERENCE \& COMMENTS |
| :--- | :--- | :--- | :--- |


| DESIGN <br> ELEMENT | Design <br> Level <br> $(\mathbf{B} / \mathrm{M} / \mathrm{F})$ | Criteria | REFERENCE \& COMMENTS |
| :---: | :--- | :--- | :--- |
| Bridge Rail | F |  |  |
|  |  |  |  |
|  |  |  |  |


[^0]:    ${ }^{1}$ La Center Junction Subarea Plan, City of La Center, 2010
    ${ }^{2}$ Cowlitz Indian Tribe Casino Project Traffic Impact Study, Parsons Brinkerhoff, 2006

[^1]:    ${ }^{3}$ The City of La Center has identified one in-process development (KWRL School Bus Facility Traffic Impact Study, H. Lee \& Associates, May 26, 2010)

[^2]:    ${ }^{4}$ Gaming positions include the number of slot machines, seats at gaming tables, or other positions at various gaming mechanisms.

[^3]:    ${ }^{1}$ The weekday AM and weekend (Friday PM) peak hours are provided because they are the time periods with directional volumes controlling design decisions. The weekday PM peak hour is documented in the IJR for the preferred roundabout corridor alternative as currently scoped; however, this time period has lower critical movement volumes compared to the weekend peak hour (Friday PM peak) and thus was excluded from this evaluation.
    ${ }^{2}$ The Friday PM peak hour represents the development's weekend peak hour and will be referred to as "Weekend Peak Hour".

[^4]:    Minor Lane/Major Mvmt

[^5]:    Zone wide Queuing Penalty: 2

[^6]:    Minor Lane/Major Mvmt

[^7]:    Minor Lane/Major Mvmt

[^8]:    Zone wide Queuing Penalty: 19

[^9]:    Zone wide Queuing Penalty: 195

[^10]:    ${ }^{1}$ Memo titled Cowlitz Reservation Development Trip Generation Memo and dated November 12, 2012. A copy is provided in Attachment B.

[^11]:    ${ }^{2}$ IJR for I-5 / SR 501 Ridgefield, prepared by WSDOT and HDR and dated May 4, 2009

[^12]:    Note: Data shown is from WSDOT for Friday, September $17^{\text {th }}, 2010$ - Sunday, September $19^{\text {th }}, 2010$

[^13]:    ${ }^{1}$ Based on data from the WSDOT Travel and Collision Data Office

[^14]:    Minor Lane/Major Mvmt

[^15]:    Minor Lane/Major Mvmt

[^16]:    Minor Lane/Major Mvmt

[^17]:    Minor Lane/Major Mvmt

[^18]:    Minor Lane/Major Mvmt

[^19]:    Minor Lane/Major Mvmt

[^20]:    Minor Lane/Major Mvmt

[^21]:    Minor Lane/Major Mvmt

[^22]:    Minor Lane/Major Mvmt

[^23]:    Minor Lane/Major Mvmt

[^24]:    Minor Lane/Major Mvmt

[^25]:    Minor Lane/Major Mvmt

[^26]:    Minor Lane/Major Mvmt

[^27]:    Minor Lane/Major Mvmt

[^28]:    Processed: Friday, August 29, 2014 11:54:13 AM SIDRA INTERSECTION 6.0.22.4722

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    Project: H:\projfile\12393 - Cowlitz Reservation Development\Sidra\2014 Analysis\Interchange Roundabouts\102
    NW 319th St and NW 31st Avel2017 Analysis\NW 319 St and NW 31st Ave.sip6
    8001045, KITTELSON AND ASSOCIATES INC, PLUS / Floating

[^29]:    Minor Lane/Major Mvmt

[^30]:    Processed: Friday, August 29, 2014 12:20:45 PM SIDRA INTERSECTION 6.0.22.4722

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    NW 319th St and NW 31st Avel2017 AnalysisINW 319 St and NW 31st Ave 85_15.sip6
    8001045, KITTELSON AND ASSOCIATES INC, PLUS / Floating

[^31]:    Processed: Friday, August 29, 2014 12:20:48 PM SIDRA INTERSECTION 6.0.22.4722

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    NW 319th St and NW 31st Avel2017 AnalysisINW 319 St and NW 31st Ave 85_15.sip6
    8001045, KITTELSON AND ASSOCIATES INC, PLUS / Floating

[^32]:    Minor Lane/Major Mvmt

[^33]:    Minor Lane/Major Mvmt

[^34]:    Minor Lane/Major Mvmt

